

# LINEAR INTEGRATED CIRCUIT DATA BOOK 

THE INFORMATION CONTAINED IN THIS DOCUMENT HAS BEEN CAREFULLY COMPTLED: HOWEVER, ITT SHALL NOU B

 STANDALD TERMS AND CONDITIONS OF SALE HQ REPRESENTATION AS TO APPLICATION OR USE OR THAT THE GIRCUITS ARE EITHEB LICENSED ÓR FREE FROM PATENT INFRINGEMENT IS INTENDED QR IMBLIED. BAYTHEON REEERVE THE RIGHT TO CHANGE THE CIRGLITRYY ANB GFHER DATA AT ANY TIME WITHOUT NOTICE AND ASSUMES NO LIABILY FOR IMODVEATENT ERRORS.
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Ceramic Flat Packages. ..... 8-5
Plastic Dual In-Line Packages ..... 8-6
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Manufacturers' Cross Reference

| Exar | Raytheon Direct Replacement | Page |
| :---: | :---: | :---: |
| XR-2207CN | XR-2207CN |  |
| XR-2207CP | XR-2207CP |  |
| XR-2207M | XR-2207M | -7-11 |
| XR-2207N | XR-2207N |  |
| XR-2207P | DR-2207P |  |
| XR-2211CN | XR-2211CN |  |
| XR-2211CP | XR-2211CP |  |
| XR-2211M. | XR-2211M | -7-16 |
| XR-2211N | XR-2211N |  |
| XR-2211P | XR-2211P |  |
| XR-2567CN | XR-2567CN |  |
| XR-2567CP | XR-2567CP | -7-24 |
| XR-2563M . | XR-2567M |  |


| Fairchild | Raytheon Direct Replacement | Page | Harris | Raytheon Direct Replacement | Page |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mu \mathrm{A} 709 \mathrm{FM}$ | RM709CQ |  | HA1-4741-2 | HA1-4741-2 |  |
| $\mu \mathrm{A} 709 \mathrm{HM}$ | RM709T |  | HA1-4741-5 | HA1-4741-5 |  |
| $\mu \mathrm{A} 709 \mathrm{HC}$ | RC709T | 1-34 | HA1-4741-8 | HA1-4741-8 | 112 |
| $\mu \mathrm{A} 709 \mathrm{DM}$ | RM709DC |  | НАЗ-4741-5 | HA3-4741-5 |  |

Manufacturers' Cross Reference


Manufacturers' Cross Reference


[^0]* Dual replacement
**Wideband, low-noise version

Manufacturers' Cross Reference

| Texas Instruments | Raytheon Direct Replacement | Page |
| :---: | :---: | :---: |
| SN52101AL. | LM101AH | 1-2 |
| SN5107L. | LM107H | 1-7 |
| SN52108L. | LM108H LM108H | 1-8 |
| SN52558L | RM4558T | 1-100 |
| SN52709J SN52709L SN52709L. SN52709S SN52709AJ SN52709AL SN52709AL SN52709AS | RM709DC |  |
|  | RM709T |  |
|  | RM709T |  |
|  | RM7090 | -1-34 |
|  | RM709ADC |  |
|  | RM709AT |  |
|  | RM709AT |  |
|  | RM709AQ |  |
| SN52710J <br> SN52710L <br> SN52710S | RM710DC |  |
|  | RM710T | -5-8 |
|  | RM7100 |  |
| SN52733L | RM733T | -2-2 |
| SN52741F <br> SN5274IJ <br> SN52741L <br> SN52741P | RM7410 |  |
|  | RM7411DC |  |
|  | RM741T |  |
|  | RM741NB |  |
| $\begin{aligned} & \text { SN52747J } \\ & \text { SN54747L } \end{aligned}$ | RM747D <br> RM747T | 1-40 |
| $\begin{aligned} & \text { SN52748J } \\ & \text { SN52748L } \end{aligned}$ | RM748D RM748T | $42$ |
| $\begin{aligned} & \text { SN72301AL. } \\ & \text { SN72301AP. } \end{aligned}$ | LM301AH <br> LM301AN | $-1-2$ |
| SN72307L <br> SN72307P | $\begin{aligned} & \text { LM307H } \\ & \text { LM307N } \end{aligned}$ | $-1-4$ |
| SN72308L | LM308H |  |
| SN72308L | LM308H |  |
| SN72558L | RC1458T/ | -1-46 |
|  | RC4558T | -1-100 |
| SN72558P | RC1458NB/ | -1-46 |
|  | RC4558NB | -1-100 |
| SN72709J | RC709DC RC709T |  |
| SN72709L | RC709NB | -1-34 |
| SN72709AJ. | RC709AD |  |
| SN72710J | RC709AT |  |
|  | RC7100C |  |
| SN72710L | RC710T | 5-8 |
| SN72711J | ${ }_{\text {RC710DC }}$ |  |
| SN72711L | RC710T |  |
| SN72733L | RC733T | -2-2 |
| SN72741L. <br> SN72741L. <br> SN72741P. <br> SN72741N. | RC741DC |  |
|  | RC741T | -1-38 |
|  | RC741NB | -38 |
|  | RC741NB |  |
| SN72747J. <br> SN72747L. <br> SN72747N | RC747DC |  |
|  | RC747T | -1-40 |
|  | RC747DB |  |
| SN72748L | RC748T | -1-42 |


|  | SYMBOL | RM/RC747 |  |  | RM1537/RC1437 |  |  | RM1558/RC1458 |  |  | LH2101A/2301A |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Ratings <br> Supply Voltage Range | $V_{C C}$ | $\begin{gathered} \pm 3 \text { to } \\ \pm 22 / \pm 18^{*} \end{gathered}$ |  |  | $\begin{gathered} \pm 3 \text { to } \\ \pm 18 \end{gathered}$ |  |  | $\begin{gathered} \pm 3 \text { to } \\ \pm 22 / \pm 18^{*} \end{gathered}$ |  |  | $\begin{gathered} \pm 3 \text { to } \\ \pm 22 / \pm 18^{*} \end{gathered}$ |  |  | V |
| Differential Input Voltage | VID | $\pm 30$ |  |  | $\pm 5$ |  |  | $\pm 30$ |  |  | $\pm 30$ |  |  | V |
| Input Voltage |  | $\pm 15$ |  |  | $\pm 10$ |  |  | $\pm 15$ |  |  | $\pm 15$ |  |  | V |
| Power Dissipation | $\mathrm{P}_{\mathrm{D}}$ | 500 |  |  | 500 |  |  | 500 |  |  | 500 |  |  | mW |
| Electrical Characteristics | @ $25^{\circ} \mathrm{C}$ | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Test Conditions | $V_{\text {CC }}$ |  | $\pm 15$ |  |  | $\pm 15$ |  |  | $\pm 15$ |  |  | ** |  | V |
| Input Offset Voltage | V/ID |  | $\begin{aligned} & 1.0 \\ & 2.0^{*} \end{aligned}$ | $\begin{aligned} & 5.0 \\ & 6.0^{*} \end{aligned}$ |  | 1.0 | $\begin{aligned} & 5.0 \\ & 7.5^{*} \end{aligned}$ |  | $\begin{aligned} & 1.0 \\ & 2.0^{*} \end{aligned}$ | $\begin{aligned} & 5.0 \\ & 6.0^{*} \end{aligned}$ |  |  | $\begin{aligned} & 2.0 \\ & 7.5^{*} \end{aligned}$ | mV |
| Input Offset Current | 110 |  | 30 | 200 |  | 50 | 200/500* |  | 30 | 200 |  |  | 10/50* | nA |
| Input Bias Current | IIB |  | 200 | 500 |  | 0.2/0.4 | 0.5/1.5* |  | 200 | 500 |  |  | 75/250* | nA |
| Input Common Mode Voltage Range | VICR | $\pm 12$ | $\pm 13$ |  | $\pm 8$ | $\pm 10$ |  | $\pm 12$ | $\pm 13$ |  | $\pm 15 / \pm 12^{*}$ |  |  | V |
| Supply Current | ID |  | 3.3 | 5.6 |  | 5 | 7.5 |  | 3.3 | 5.6 |  |  | 2.5 | mA |
| Open Loop Voltage Gain | AVOL | 50 | 200 |  | 25/15* | 45 | 70 | 50 | 200 |  | 25/15* |  |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | VOR | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | $\pm 12$ |  |  | V |
| Common Mode Rejection Ratio | CMRR | 70 | 90 |  | 70/65* | 90 |  | 70 | 90 |  | 80/70* |  |  | dB |
| Power Supply Rejection Fatio | PSSR |  | 30 | 150 |  |  | $\begin{array}{r} 150 \\ 200^{*} \\ \hline \end{array}$ |  | 30 | 150 | $\begin{gathered} 80 / 70^{*} \\ d B \\ \hline \end{gathered}$ |  | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Unity Gain Bandwidth | BW |  | 0.8 |  |  |  |  |  | 0.8 |  |  |  |  | MHz |
| Slew Rate | SR |  | 0.5 |  |  |  |  |  | 0.5 |  |  |  |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Channel Separation |  |  | -98 |  |  | -90 |  |  | -98 |  |  |  |  | dB |
| Noise Voltage | $\mathrm{V}_{\mathrm{N}}$ |  |  |  |  |  |  |  |  |  |  |  |  | $\mathrm{nV} /(\mathrm{Hz})^{1 / 2}$ |
| Operating Temperature Range | $\mathrm{T}_{\text {A }}$ | $\begin{gathered} -55 \\ 0 \end{gathered}$ | $\begin{aligned} & \mathrm{RM} \\ & \mathrm{RC} \end{aligned}$ | $\begin{gathered} 125 \\ 70 \end{gathered}$ | $\begin{gathered} -55 \\ 0 \end{gathered}$ | $\begin{aligned} & \text { RM } \\ & \text { RC } \end{aligned}$ | $\begin{gathered} 125 \\ 70 \end{gathered}$ | $\begin{gathered} -55 \\ 0 \end{gathered}$ | $\begin{aligned} & \text { RM } \\ & \text { RC } \end{aligned}$ | $\begin{gathered} 125 \\ 70 \end{gathered}$ | $\begin{gathered} -55 \\ -25 \\ 0 \end{gathered}$ | $\begin{aligned} & 2101 A \\ & 2201 A \\ & 2301 A \end{aligned}$ | $\begin{aligned} & +125 \\ & +85 \\ & +70 \end{aligned}$ | ${ }^{\circ} \mathrm{C}$ |
| Package: $\quad \mathrm{He}$ | etic TO-5 | TF |  |  |  |  |  | TE |  |  |  |  |  |  |
|  | Hermetic Dip Plastic Dip | DC |  |  | DC |  |  | $D E$ |  |  | DC |  |  |  |
|  |  | DB |  |  | DB |  |  | NB |  |  |  |  |  |  |

${ }^{* *}$ Note: Specifications apply $\pm 5 \leqslant \mathrm{~V}_{\mathrm{CC}} \leqslant \pm 20 \mathrm{~V}$ and over temperature.
*Commercial temp range device.

|  | SYMBOL | RM/RC4558 |  |  | RM/RC4559 |  |  | RC4739 |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Ratings |  | $\pm 4$ to |  |  | $\pm 4$ to |  |  | $\pm 4$ to |  |  |  |
| Supply Voltage Range | VCC | $\pm 18$ |  |  | $\pm 18$ |  |  | $\pm 18$ |  |  | V |
| Differential Input Voltage | VID | $\pm 30$ |  |  | $\pm 30$ |  |  | $\pm 30$ |  |  | V |
| Input Voltage |  | $\pm 15$ |  |  | $\pm 15$ |  |  | $\pm 15$ |  |  | $\checkmark$ |
| Power Dissipation | PD | 500 |  |  | 500 |  |  | 500 |  |  | mW |
| Electrical Characteristics | @ $25^{\circ} \mathrm{C}$ | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Test Conditions | VCC |  | $\pm 15$ |  |  | $\pm 15$ |  |  | $\pm 15$ |  | V |
| Input Offset Voltage | VID |  | $\begin{aligned} & 1.0 \\ & 2.0^{*} \end{aligned}$ | $\begin{aligned} & 5.0 \\ & 6.0^{*} \end{aligned}$ |  | $\begin{aligned} & 1.0 \\ & 2.0^{*} \end{aligned}$ | $\begin{aligned} & 5.0 \\ & 6.0^{*} \end{aligned}$ |  | 2.0 | 6.0 | mV |
| Input Offset Current | 110 |  | 5.0 | 200 |  | 5.0 | 200 |  | 5.0 | 200 | nA |
| Input Bias Current | IIB |  | 40/200* | 500 |  | 40/200* | 500 |  | 40 | 500 | nA |
| Input Common Mode Voltage Range | VICR | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | V |
| Supply Current | ${ }^{1}$ |  | 3.5 | 5.6 |  | 3.5 | 5.6 |  | 3.5 | 5.6 | mA |
| Open Loop Voltage Gain | AVOL | 50/20* | 300 |  | 50/20* | 300 |  | 20 | 300 |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | $\mathrm{V}_{\text {OR }}$ | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | V |
| Common Mode Rejection Ratio | CMRR | 70 | 100 |  | 70 | 100 |  | 70 | 100 |  | dB |
| Power Supply Rejection Ratio | PSSR |  | 10 | 150 |  | 10 | 150 |  | 10 | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Unity Gain Bandwidth | BW | 2.5/2.0* | 3.0 |  | 3 | 4 |  |  | 3.0 |  | MHz |
| Slew Rate | SR |  | 0.5 |  | 1.5 | 2.0 |  |  | 1.0 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Channel Separation |  |  | -90 |  |  | -90 |  |  | -125 |  | dB |
| Noise Voltage | $\mathrm{V}_{\mathrm{N}}$ |  | 10 |  | $2.0 \dagger$ | $1.4 \dagger$ |  |  | $2.5 \dagger$ |  | $\mathrm{nV} /(\mathrm{Hz})^{1 / 2}$ |
| Operating Temperature Range | TA | $\begin{gathered} -55 \\ 0 \end{gathered}$ | $\begin{aligned} & \mathrm{RM} \\ & \mathrm{RC} \end{aligned}$ | $\begin{gathered} +125 \\ 70 \end{gathered}$ | $\begin{gathered} -55 \\ 0 \end{gathered}$ | $\begin{aligned} & \mathrm{RM} \\ & \mathrm{RC} \end{aligned}$ | $\begin{gathered} +125 \\ 70 \\ \hline \end{gathered}$ | 0 |  | 70 | ${ }^{\circ} \mathrm{C}$ |
| Package: | metic TO-5 <br> rmetic Dip <br> Plastic Dip |  | TE <br> DE <br> NB |  | TE <br> DE |  |  | DB |  |  |  |

*Commercial temp range device.
†Broad Band noise voltage -20 Hz to $20 \mathrm{kHz}(\mu \vee \mathrm{RMS})$.

## Dual Operational Amplifier Summary

|  | SYMBOL | RM4136/RC4 136 |  |  | LM124/LM224/LM324 |  |  | LM2902 |  |  | $\begin{gathered} \text { RM3503A/ } \\ \text { RV3403A/RC3403A } \end{gathered}$ |  |  | L.M2900/LM3900 |  |  | RV3301/RC3401 |  |  | UNIT <br> V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Ratings <br> Supply Voltage Range | V'CC | $\begin{gathered} \pm 4 \text { to } \\ \pm 22 / \pm 18^{*} \end{gathered}$ |  |  | $\begin{gathered} +3 \text { or } \pm 1.5 \text { to } \\ +32 \text { or } \pm 16 \\ \hline \end{gathered}$ |  |  | $\begin{gathered} +3 \text { or } \pm 1.5 \text { to } \\ +32 \text { or } \pm 16 \end{gathered}$ |  |  | $\begin{aligned} & +2.5 \text { or } \pm 1.25 \text { to } \\ & +36 \text { or } \pm 18 \end{aligned}$ |  |  | $\begin{aligned} & +4 \text { or } \pm 2 \text { to } \\ & +36 \text { or } \pm 18 \end{aligned}$ |  |  | $\begin{gathered} +4 \text { to } \\ +28 /+18^{*} \end{gathered}$ |  |  |  |
| Differential Input Voltage | VID | $\pm 30$ |  |  | 32 |  |  | 26 |  |  | 36 |  |  |  |  |  |  |  |  | V |
| Input Voltage |  | $\pm 15$ |  |  | 32 |  |  | 26 |  |  | 36 |  |  |  |  |  |  |  |  | V |
| Power Dissipation | ${ }^{P} \mathrm{D}$ | 800 |  |  | 900 |  |  | 570 |  |  | 650 |  |  | 570 |  |  | 625 |  |  | mW |
| Electrical Characteristics | @ $25^{\circ} \mathrm{C}$ | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Test Condition VCC: |  |  | $\pm 15$ |  |  | +5 |  |  | +5 |  |  | $\pm 15$ |  |  | +15 |  |  | $\pm 15$ |  | V |
| Input Offset Voltage | $\mathrm{V}_{\mathrm{IO}}$ |  | $\begin{aligned} & 0.5 \\ & 0.5 \\ & \hline \end{aligned}$ | $\begin{gathered} 4.0 \\ 6.0^{*} \end{gathered}$ |  | 2 | $\begin{gathered} 5 \\ 7^{*} \\ \hline \end{gathered}$ |  | 2 | 7 |  | 2 | $\begin{gathered} 4 \\ 5^{*} \end{gathered}$ |  |  |  |  |  |  | mV |
| Input Offset Current | 110 |  | 5 | $\begin{gathered} 150 \\ 200^{*} \\ \hline \end{gathered}$ |  | $\begin{array}{r}  \pm 3 \\ \pm 3 \\ \hline \end{array}$ | $\begin{gathered} \pm 30 \\ \pm 50^{*} \\ \hline \end{gathered}$ |  | 5 | 50 |  | $\pm 30$ | $\pm 50$ |  |  |  |  |  |  | $n A$ |
| Input Bias Current | 1 IB |  | 40 | $\begin{gathered} 400 \\ 500^{*} \end{gathered}$ |  |  | $\begin{array}{r} 150 \\ 250^{*} \\ \hline \end{array}$ |  | 45 | 500 |  | 150 | 200 |  | 30 | 200 |  | 50 | 300 | $n A$ |
| Input Common Mode Voltage Range | $V_{\text {ICR }}$ | $\pm 12$ | $\pm 14$ |  |  | 35 |  |  | 35 |  | -15 |  | +13 |  |  |  |  |  |  | V |
| Supply Current | 1 D |  | 7 | 11.3 |  | 0.8 | 2 |  | 0.8 | 2 |  | 3 | 4/5* |  | 6.2 | 10 |  | 6.9 | 10 | mA |
| Open Loop Voltage Gain | AVOL | $\begin{array}{r} 50 \\ 20^{*} \\ \hline \end{array}$ | 300 |  | $\begin{gathered} 50 \\ 25^{*} \\ \hline \end{gathered}$ | 100 |  |  | 100 |  | $\begin{gathered} 50 \\ 25^{*} \\ \hline \end{gathered}$ | 100 |  | 1.2 | 2.8 |  | 1 | 2 |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | VOR | $\pm 12$ | $\pm 14$ |  | 0 |  | $\mathrm{V}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | $\pm 13$ | $\pm 14$ |  | 13.5 | 14.2 |  | 13.5 | 14.2 |  | V |
| Common Mode Rejection Ratio | CMIRR | 70 | 100 |  | $\begin{array}{r} 70 \\ 65^{*} \\ \hline \end{array}$ | 85 |  | 50 | 70 |  | 80 | 90 |  |  |  |  |  |  |  | dB |
| Power Supply Rejection Ratio | PSRR |  | $\begin{gathered} 10 \\ \mu \vee / \vee \end{gathered}$ | $\begin{gathered} 150 \\ \mu \mathrm{~V} / \mathrm{V} \end{gathered}$ | 65 dB | 100 dB |  | 50 dB | 100 dB |  |  | $\begin{gathered} 20 \\ \mu \vee / \vee \end{gathered}$ | $\begin{gathered} 45 \\ \mu \vee / \vee \\ 100 \\ \mu \vee / V^{*} \end{gathered}$ |  | 70 dB |  |  | 55 dB |  |  |
| Unity Gain Bandwidth | BW |  | 3 |  |  |  |  |  |  |  |  | 2.0 |  |  | 2.5 |  |  | 5.0 |  | MHz |
| Slew Rate | SR |  | $\begin{gathered} 1.5 \\ 1.0^{*} \\ \hline \end{gathered}$ |  |  | 0.3 |  |  |  |  |  | 1.2 |  |  | 0.5 |  |  | 0.6 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Output Sink Current | Is ${ }_{\text {ink }}$ |  |  |  | 10 | 20 |  | 10 | 20 |  | 10 | 20 |  | 0.5 | 1.3 |  | 0.5 | 1.0 |  | mA |
| Output Source Current | Isource |  |  |  | 20 | 40 |  | 20 | 40 |  | 20 | 40 |  | 6 | 18 |  | 5.0 | 10 |  | mA |
| Channel Separation |  |  | -90 |  |  | -120 |  |  | -120 |  |  | -120 |  |  |  |  |  | -65 |  | dB |
| Operating Temperature Range |  | $\begin{array}{\|c} -55 \\ -40 \\ 0 \\ \hline \end{array}$ | $\begin{aligned} & \text { RM } \\ & \text { RC } \\ & \text { RV } \end{aligned}$ | $\begin{aligned} & +125 \\ & +70 \\ & +85 \end{aligned}$ | $\begin{gathered} -55 \\ -25 \\ 0 \\ \hline \end{gathered}$ | LM124 LM224 LM324 | $\begin{aligned} & +125 \\ & +85 \\ & +70 \\ & \hline \end{aligned}$ | -40 |  | +85 | $\begin{gathered} -55 \\ -40 \\ 0 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{RM} \\ & \mathrm{RV} \\ & \mathrm{RC} \\ & \hline \end{aligned}$ | $\begin{gathered} +125 \\ +85 \\ +70 \\ \hline \end{gathered}$ | $\begin{gathered} -40 \\ 0 \end{gathered}$ | $\begin{aligned} & 2900 \\ & 3900 \end{aligned}$ | $\begin{aligned} & +85 \\ & +70 \end{aligned}$ | $\begin{gathered} -40 \\ 0 \end{gathered}$ | $\begin{aligned} & 3301 \\ & 3401 \end{aligned}$ | $\begin{aligned} & +85 \\ & +75 \end{aligned}$ | ${ }^{\circ} \mathrm{C}$ |
| Package: 14 pin DipHermetic <br>  <br> Plastic |  | DC |  |  | DC |  |  |  |  |  | DC |  |  |  |  |  |  |  |  |  |
|  |  | DB |  |  | DB |  |  | DB |  |  | DB |  |  | DB |  |  | DB |  |  |  |

*Denote commercial temperature range device

|  | SYMBOL | $R M / R V / R C 4156^{(2)}$ |  |  | LM149/249/349 LM148/248/348 |  |  | HA4741-2/5 |  |  | RM/RV/RC4157 |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Ratings <br> Supply Voltage Range | $\mathrm{V}_{\mathrm{CC}}$ | $\pm 4$ to $\pm 20$ |  |  | $\pm 4$ to $\pm 22$ |  |  | $\pm 4$ to $\pm 20$ |  |  | $\pm 4$ to $\pm 20$ |  |  | V |
| Differential Input Voltage | $V_{10}$ | $\pm 30$ |  |  | $\pm 44 / \pm 36$ * |  |  | $\pm 30$ |  |  | $\pm 30$ |  |  | V |
| Input Voltage |  | $\pm 15$ |  |  | $\pm 22 / \pm 18 *$ |  |  | $\pm 15$ |  |  | $\pm 15$ |  |  | V |
| Power Dissipation | $P_{D}$ | 880 |  |  | 900 |  |  | 800 |  |  | 880 |  |  | mW |
| Electrical Characteristics | @ $25{ }^{\circ} \mathrm{C}$ | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Test Condition $\mathrm{V}_{\mathrm{CC}}$ : |  |  | $\pm 15$ |  |  | $\pm 15$ |  |  | $\pm 15$ |  |  | $\pm 15$ |  | V |
| Input Offset Voltage | $\mathrm{V}_{10}$ |  | $\begin{aligned} & 0.5 \\ & 1.0 \end{aligned}$ | $\begin{gathered} 3.0 \\ 5.0^{*} \end{gathered}$ |  | 1.0 | $\begin{gathered} 5.0 \\ 6.0^{*} \end{gathered}$ |  | $\begin{aligned} & 0.5 \\ & 1.0 \end{aligned}$ | $\begin{gathered} 3.0 \\ 5.0^{*} \end{gathered}$ |  | 0.5 1.0 | $\begin{gathered} 3.0 \\ 5.0^{*} \end{gathered}$ | mV |
| Input Offset Current | 110 |  | $\begin{aligned} & 15 \\ & 30 \end{aligned}$ | $\begin{gathered} 30 \\ 50^{*} \end{gathered}$ |  | 4 | $\begin{gathered} 25 \\ 50^{*} \\ \hline \end{gathered}$ |  | $\begin{aligned} & 15 \\ & 30 \end{aligned}$ | $\begin{gathered} 30 \\ 50^{*} \end{gathered}$ |  | $\begin{aligned} & 15 \\ & 30 \end{aligned}$ | $\begin{gathered} 30 \\ 50^{*} \\ \hline \end{gathered}$ | nA |
| Input Bias Current | $I_{\text {IB }}$ |  | 60 | $\begin{gathered} 200 \\ 300^{*} \end{gathered}$ |  | 30 | $\begin{gathered} 100 \\ 200^{*} \end{gathered}$ |  | 60 | $\begin{gathered} 200 \\ 300^{*} \end{gathered}$ |  | 60 | $\begin{gathered} 200 \\ 300^{*} \end{gathered}$ | nA |
| Input Common Mode Voltage Range | VICR | $\pm 12$ | $\pm 14$ |  | $\pm 12^{* *}$ |  |  | $\pm 12$ |  |  | $\pm 12$ |  |  | V |
| Supply Current | ID |  | 4.5/5 | 5/7* |  | 2.4 | 3.6 |  | 4.5/5 | 5/7* |  | 4.5/5 | 5/7* | mA |
| Open Loop Voltage Gain | AVOL | $\begin{array}{\|c\|} \hline 50 \\ 25^{*} \\ \hline \end{array}$ | 100 |  | $\begin{array}{r} 50 \\ 25^{*} \\ \hline \end{array}$ | 160 |  | $\begin{gathered} 50 \\ 25^{*} \\ \hline \end{gathered}$ | $\begin{array}{r} 100 \\ 50^{*} \\ \hline \end{array}$ |  | $\begin{gathered} 50 \\ 25^{*} \\ \hline \end{gathered}$ | 100 |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | $\mathrm{V}_{\mathrm{OR}}$ | $\pm 12$ | $\pm 14$ |  | $\pm 12^{* *}$ | $\pm 13$ |  |  |  |  | $\pm 12$ |  |  | V |
| Common Mode Rejection Ratio | CMRR | 80 |  |  | 70** | 90 |  | 80 |  |  | 80 |  |  | dB |
| Power Supply Rejection Ratio | PSRR | 80dB |  |  | $\begin{gathered} 77^{* *} \\ \mathrm{~dB} \end{gathered}$ | 96 |  | $\begin{gathered} 80^{* *} \\ d B \end{gathered}$ |  |  | $\begin{aligned} & 80 \\ & d B \end{aligned}$ |  |  |  |
| Unity Gain Bandwidth | BW | 2.8 | 3.5 |  |  | $\begin{gathered} 1.0 /(1) \\ 4.0+ \end{gathered}$ |  |  | 3.5 |  | $15^{(1)}$ |  |  | MHz |
| Slew Rate | SR | 1.3 | 1.6 |  |  | $\begin{aligned} & 0.5 / \\ & 2.0 \dagger \end{aligned}$ |  |  | 1.6 |  | 6.5 | 8 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Output Sink Current | I sink |  |  |  |  | - |  | 5 | 15 |  |  |  |  | mA |
| Output Source Current | $\mathrm{I}_{\text {source }}$ |  |  |  |  |  |  | 5 | 15 |  |  |  |  | mA |
| Channel Separation |  |  | -108 |  |  | -120 |  |  | -108 |  |  | -108 |  | dB |
| Operating Temperature Range |  | $\begin{array}{\|c\|} \hline-55 \\ -40 \\ 0 \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{RM} \\ & \mathrm{RV} \\ & \mathrm{RC} \\ & \hline \end{aligned}$ | $\begin{gathered} +125 \\ 85 \\ 70 \\ \hline \end{gathered}$ | $\begin{gathered} -55 \\ -25 \\ 0 \\ \hline \end{gathered}$ | $\begin{aligned} & 148 \\ & 248 \\ & 348 \\ & \hline \end{aligned}$ | $\begin{aligned} & +125 \\ & +85 \\ & +70 \\ & \hline \end{aligned}$ | $\begin{gathered} -55 \\ 0 \end{gathered}$ | $\begin{aligned} & -2 \\ & -5 \end{aligned}$ | $\begin{gathered} +125 \\ 70 \end{gathered}$ | $\begin{gathered} -55 \\ -25 \\ 0 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{RM} \\ & \mathrm{RV} \\ & \mathrm{RC} \\ & \hline \end{aligned}$ | $\begin{aligned} & +125 \\ & +85 \\ & +70 \\ & \hline \end{aligned}$ | ${ }^{\circ} \mathrm{C}$ |
| Package: 14 pin Dip | Hermetic | DC |  |  | DC |  |  | DC |  |  | DC |  |  |  |
|  | Plastic | DB |  |  | DB |  |  | DB |  |  | DB |  |  |  |

[^1]|  | SYMBOL | LM139A/LM139 |  |  | LM239A/LM239/LM339A/LM339 |  |  | LM2901 |  |  | RV3302 |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Ratings |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Supply Voltage Range | $V_{\text {CC }}$ | +4 to +36 |  |  | +4 to +36 |  |  | +4 to +36 |  |  | +4 to +28 or $\pm 14$ |  |  | V |
| Differential Input Voltage | VID | +36 |  |  | +36 |  |  | $+36$ |  |  | +28 |  |  | V |
| Input Voltage |  | +36 |  |  | +36 |  |  | +36 |  |  | +28 |  |  | V |
| Power Dissipation | PD | 800 |  |  | 800 |  |  | 570 |  |  | 625 |  |  | mW |
| Electrical Characteristics |  | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Test Condition | VCC |  | +5 |  |  | +5 |  |  | +5 |  |  | +5 |  | V |
| Input Offset Voltage | $\mathrm{V}_{10}$ |  | 2/1 | 5/2* |  | 2/1 | 5/2* |  | 2 | 7 |  | 3 | 20 | mV |
| Input Offset Current | 110 |  | 3 | 25 |  | 5 | 50 |  | 5 | 50 |  | 3 | 100 | $n A$ |
| Input Bias Current | IIB |  | 25 | 100 |  | 25 | 250 |  | 25 | 250 |  | 25 | 500 | nA |
| Input Common Mode Voltage Range | VICR | 0 |  | +3.5 | 0 |  | +3.5 | 0 |  | +3.5 | 0 |  | +3.5 | V |
| Supply Current | IOC |  | 0.8 | 2 |  | 0.8 | 2 |  | 0.8 | 2 |  | 0.7 | 1.5 | mA |
| Open Loop Voltage Gain | AVOL |  | 200 |  |  | 200 |  |  | 200 |  | 2 | 30 |  | $\mathrm{V} / \mathrm{mV}$ |
| Common Mode Rejection Ratio | CMRR |  |  |  |  |  |  |  |  |  |  | 60 |  | dB |
| Slew Rate | SR |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & -200 \\ & +50 \\ & \hline \end{aligned}$ |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Response Time | $\mathrm{T}_{\mathrm{r}}$ |  | 1.3 |  |  | 1.3 |  |  | 1.3 |  |  | 2.0 |  | $\mu \mathrm{s}$ |
| Output Sink Current | $\mathrm{I}_{\text {sink }}$ | 6 | 16 |  | 6 | 16 |  | 6 | 16 |  | 2 | 16 |  | mA |
| Saturation Voltage | $\mathrm{V}_{\text {sat }}$ |  | 0.2 | 0.4 |  | 0.2 | 0.4 |  | 0.2 | 0.4 |  | 0.25 | 0.5 | V |
| Output Leak Current | $\mathrm{I}_{\mathrm{OL}}$ |  | 0.1 |  |  | 0.1 |  |  | 0.1 |  |  |  | 1.0 | nA |
| Operating Temperature Range | TA | -55 |  | +125 | $\begin{gathered} -25 \\ 0 \end{gathered}$ | $\begin{aligned} & \text { 239A } \\ & 339 A \end{aligned}$ | $\begin{array}{r} +85 \\ +70 \end{array}$ | -40 |  | +85 | -40 |  | +85 | ${ }^{\circ} \mathrm{C}$ |
| Package: 14 Pin Dip | Hermetic Plastic | DC |  |  | DC |  |  |  |  |  | DC |  |  |  |
|  |  | DB |  |  | DB |  |  | DB |  |  | DB |  |  |  |

* A version


## RAYACT-883 PROGRAM

The Raytheon Acceptance Testing Program called Rayact-883 involves in-process inspections which assure compliance with MIL-STD-883 test methods and MIL-M-38510 Program Plan Requirements.
Table 1 defines the Standard Process Flow for Raytheon Semiconductor's Integrated Circuits. After completion of the in-process inspections and 100\% production screens, each lot is subjected to a quality conformance inspection as defined in Table 2. The screening and acceptance testing outlined in Tables 1 and 2 are provided at no extra cost.
In addition to the Standard Process Flow and acceptance testing, Qualification Tests in accordance with MIL-STD-883, Method 5005 are conducted every three months on each product line. Generic Summary Data of Groups A, B, C and D is available upon request.
The level of reliability you desire can be selected from Table 3. These tests are conducted in accordance with Method 5004 of MIL-STD-883.

## APPLICABLE DOCUMENTS:

Military: MIL-STD-883
MIL-M-38510
MIL-Q-9858
Raytheon Semiconductor: Quality/Reliability Assurance Manual

## PROCESS MONITORS

Quality control process monitors as shown on Table 1 are designed to verify our compliance with our internal written specifications.
Our monitor reports are used to identify problem areas and process trends.
From the analysis of these reports we are able to continually improve our processes.

## DIE SALES

Raytheon devices are available in chip form as well as a variety of packages.
Each die is electrically tested to the applicable wafer probe test specification. In addition the die are $100 \%$ visually inspected to meet the requirements of MIL-STD-883 Method 2010 condition B. Die are then checked to assure a $1 \%$ AQL by quality control. Refer to Raytheon's dice catalog for complete product and processing information.

## FAILURE ANALYSIS GROUP

The failure analysis group is capable of analyzing any material used in the Semiconductor industry. Equipment such as S.E.M., Auger Spectroscopy and Dispersive x-ray are used on a daily basis.
Full metallographic capability is also available for studying various structures.

## Table 1-Standard Process Flow Summary for Integrated Circuits

| COMMERCIAL |  | MILITARY HERMETIC | PROCESS FLOW |
| :---: | :---: | :---: | :---: |
| EPOXY | HERMETIC |  |  |
| $x$ | $x$ | $x$ | Purchase raw material |
| X | X | X | Quality control receiving inspection. Parts are inspected to applicable M\&SS and/ or drawing. |
| X | X | X | Mask making |
| X | X | X | QC mask lot acceptance. Each lot is inspected for mask defects. |
| X | X | $x$ | Wafer fabrication |
| X | X | X | QC process monitors including particle counts, DI water, gasses, SEM and diffusion |
| X | X | X | QC lot acceptance. Samples are selected from each lot. |
| X | X | X | 100\% electrical probe test per applicable spec |


| COMMERCIAL |  | MILITARY HERMETIC | PROCESS FLOW |
| :---: | :---: | :---: | :---: |
| EPOXY | HERMETIC |  |  |
| X | X | X | QC lot acceptance. Samples are selected from each lot |
| X | X | X | Wafer stores |
| X | X | X | Scribe and break and plate. |
| X | X | X | QC monitor |
|  |  | X | 100\% die visual MIL-STD-883 Method 2010 condition B |
| X | X |  | $100 \%$ die visual commercial spec |
| X | X | X | QC lot acceptance |
| X | X | X | Die attach. |
| ${ }^{4} \times$ | X | X | QC monitor |
|  | X | X | Ultrasonic aluminum bond. |
|  | X | X | QC monitor |
| X |  |  | Thermal compression gold bond. |
| X |  |  | QC monitor |
|  |  | X | Preseal inspection 100X MIL-STD-883 Method 2010 Con- dition B |

Table 1-Standard Process Flow Summary for Integrated Circuits (Cont.)

| COMMERCIAL |  | MILITARY HERMETIC | PROCESS <br> FLOW |
| :---: | :---: | :---: | :---: |
| EPOXY | HERMETIC |  |  |
|  |  | x | Preseal inspection 30X MIL-STD-883 Method 2010 Condition B |
| X | X |  | Preseal inspection 30X commercial specification |
| X | $\times$ | X | QC lot acceptance |
| X | X | X | Seal/mold and cure. |
| X | X | X | QC monitor |
|  | X | X | $\begin{array}{cr}\text { Stabilization } & \text { bake } \\ \text { MIL-STD-883 } & \text { Meth- }\end{array}$ od 1008 Condition C $150^{\circ} \mathrm{C}$ |
|  | X | X | Temperature cycle MIL-STD-883 Method 1010 Condition C -65 to $+150^{\circ} \mathrm{C}$, 10 cycles |
|  | X | X | OC monitor |
|  | X | X | Centrifuge* MIL-STD883 Method 2001 Condition C, Y1 only |


| COMMERCIAL |  | MILITARY HERMETIC | PROCESS FLOW |
| :---: | :---: | :---: | :---: |
| EPOXY | HERMETIC |  |  |
|  | X | X | QC monitor |
|  | X | X | Tin plate MIL-STD883 Method 2003 |
|  | X | X | QC monitor |
| X |  |  | Solder dip MIL-STD- <br> 883 Methoci 2003 |
| X |  |  | QC monitor |
|  |  | X | Hermeticity MIL-STD-883 Method 1014 Condition A or B and C |
|  |  | X | QC monitor |
| X | X | X | Visual mechanical MIL-STD-883 Method 2009 |
| X | X | X | QC monitor |
| X | X | X | DC and functional per applicable electrical test specification |
| X | X | X | QA lot acceptance |
| X | X | X | Unbranded inventory |

*Except TK(TO66) packages.

Table 2-Quality Conformance Inspection (Each Lot)

| INSPECTION |  | LTPD/MAX. ACC. NO. | COMMENTS |
| :---: | :---: | :---: | :---: |
| External |  | 7/2 | MIL-STD-883, Method 2009 |
| Hermeticity <br> Fine Leak <br> Gross Leak |  | 7/2 | Military Products <br> MIL-STD-883, Method 1014, Condition A or B MIL-STD-883, Method 1014, Condition C |
| Electrical <br> Static Parameters | $+25^{\circ} \mathrm{C}$ | 5/1 | Per Applicable Electrical Test Specification |
|  | $+125^{\circ} \mathrm{C}$ | 7/1 |  |
|  | $-55^{\circ} \mathrm{C}$ | 7/1 |  |
| Dynamic Parameters | $+25^{\circ} \mathrm{C}$ | 5/1 |  |
|  | +1250 ${ }^{\circ}$ | 7/1 |  |
|  | $-55^{\circ} \mathrm{C}$ | 7/1 |  |
| Packaye and Ship |  | Quality Assurance Monitor |  |

## NOTE:

Generic Qualification Data in accordance with MIL-STD-883, Method 5005, can be supplied if negotiated prior to procurement.

## Table 3-Optional Screening Reference MIL-STD-883 Method 5004*

| SCREEN | CLASS S (A) ${ }^{(14)}$ |  | CLASS B |  | CLASS C |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | METHOD | REQMT | METHOD | REQMT | METHOD | REQMT |
| 3.1.1 Internal visual (1) | 2010, test condition A | 100\% | 2010, test condition B | 100\% | 2010, test condition B | 100\% |
| 3.1.2 Stabilization bake (see 3.4.1, 3.4.2) no end point measurements required ${ }^{\text {(16) }}$ | $1008$ <br> 24 hrs , min, test condition C min | 100\% | 1008 <br> 24 hrs , min, test condition C min | 100\% | $1008$ <br> 24 hrs, min, test condition C min | 100\% |
| 3.1.3 Temperature cycling (2) | 1010, test condition C | 100\% | 1010, test condition C | 100\% | 1010, test condition C | 100\% |
| 3.1.4 Constant acceleration (see 3.2 and 3.4.2) ${ }^{(16)}$ | 2001, test condition E (min) $\mathrm{Y}_{1}$ orientation only | 100\% | 2001, test condition E (min) $\mathrm{Y}_{1}$ orientation only | 100\% | 2001, test condition E $(\min ) \mathrm{Y}_{1}$ orientation only | 100\% |
| 3.1.5 Visual inspec- $\text { tion }(3)$ |  | 100\% |  | 100\% |  | 100\% |
| 3.1.6 Seal (4) <br> (a) Fine <br> (b) Gross | 1014 | 100\% <br> (5) | 1014 | 100\% | 1014 | 100\% |
| 3.1.7 Particle impact noise detection (PIND) | 2020, test condition A or B | $\begin{gathered} 100 \% \\ (6) \end{gathered}$ |  | - |  | - |
| 3.1.8 Serialization |  | (7) |  | - |  | - |
| 3.1.9 Interim (pre-burn-in) electrical parameters (see 3.5.1) ${ }^{\text {(16) }}$ | Per applicable device specification | $\begin{gathered} 100 \% \\ (8) \end{gathered}$ | Per applicable device specification | (9) |  | - |
| $\begin{aligned} & \text { 3.1.10 Burn-in test } \\ & \text { (see 3.4.2) }^{(16)} \end{aligned}$ | $\begin{aligned} & 1015(10) \\ & 240 \mathrm{hrs} \text { at } 125^{\circ} \mathrm{C} \text { min } \end{aligned}$ | 100\% | $\begin{aligned} & 1015^{(15)} \\ & 160 \mathrm{hrs} \text { at } 125^{\circ} \mathrm{C} \mathrm{~min} \end{aligned}$ | 100\% |  | - |
| 3.1.11 Interim (post-burn-in) electrical ${ }^{\text {(16) }}$ parameters (see 3.5.1) | Per applicable device specification | $\begin{gathered} 100 \% \\ \text { (8) } \end{gathered}$ |  | - |  | - |
| 3.1.12 Reverse bias burn-in(11) (see 3.4.2) ${ }^{(16)}$ | 1015; test condition A or $\mathrm{C}, 72$ hrs at $150^{\circ} \mathrm{C}$ $\min (10)$ | 100\% |  | - |  | - |
| 3.1.13 Interim (post-burn-in) electrical ${ }^{(16)}$ parameters (see 3.5.1) | Per applicable device specification | $100 \%$ <br> (8) | Per applicable device specification | 100\% |  | - |

*See footnotes at end of table.

## Table 3-Optional Screening Reference MIL-STD-883 Method 5004 (Cont.)

| SCREEN | CLASS S (A) ${ }^{(14)}$ |  | CLASS B |  | CLASS C |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | METHOD | REQMT | METHOD | REQMT | METHOD | REQMT |
| 3.1.14 Seal <br> (a) Fine <br> (b) Gross | 1014 | 100\% |  | - |  | - |
| 3.1.15 Final electrical test (see 3.5.2) ${ }^{\text {(16) }}$ <br> (a) Static tests <br> (1) $25^{\circ} \mathrm{C}$ (sub- <br> group 1, table I, 5005) <br> (2) Maximum and minimum rated operating temp (subgroups 2, 3, table I, 5005) <br> (b) Dynamic tests and switching tests $25^{\circ} \mathrm{C}$ (subgroups 4 and 9 , table I, 5005) <br> (c) Functional test $25^{\circ} \mathrm{C}$ (subgroup 7, table I, 5005) | Per applicable device specification | 100\% <br> 100\% <br> 100\% <br> 100\% | Per applicable device specification | 100\% <br> 100\% <br> 100\% <br> 100\% | Per applicable device specification | 100\% <br> - |
| 3.1.16 Radiographic (12) | 2012 two views | 100\% |  | - |  | - |
| 3.1.17 Qualification or quality conformance inspection test sample selection |  | (13) |  | (13) |  | (13) |
| 3.1.18 External visual | 2009 | 100\% | 2009 | 100\% | 2009 | 100\% |

## NOTES:

(1) Unless otherwise specified, at the manufacturer's option, test samples for group B, bond strength (method 5005) may be selected randomly immediately following internal visual (method 5004) prior to sealing.
(2) For class $B$ and $C$ devices, this test may be replaced with thermal shock method 1011, test condition $A$, minimum.
(3) At the manufacturer's option, visual inspection for catastrophic failures may be conducted after each of the thermal/mechanical screens, after the sequence or after seal test. Catastrophic failures are defined as missing leads, broken packages or lids off.
(4) For classes B and C devices, the seal test may be performed in any sequence between 3.1.6 and 3.1.16, but it shall be performed after all shearing and forming operations on the terminals.
(5) Optional when 3.1.14 is performed.
(6) See MIL-M-38510 paragraph 4.6.3. The PIND test may be performed in any sequence after 3.1.4 and prior to 3.1.13.
(7) Class $S$ devices shall be serialized prior to interim electrical parameter measurements.
(8) Electrical parameters shall be read and recorded.
(9) When specified in the applicable device specification, 100 percent of the devices shall be tested for those parameters requiring delta calculations.
(10) For class $S$ devices, test condition $F$ of method 1015 and 3.4 .2 herein shall not apply.
(11) The reverse bias burn-in (see 3.1.12) is a requirement only when specified in the applicable device specification and is recommended only for certain MOS, linear or other microcircuits where surface sensitivity may be of concern. When reverse bias burn-in is not required, interim electrical parameter measurements of 3.1.11 ara omitted. The ordier of performing the burn-in (see 3.1.10) and the reverse bias burn-in may be inverted.
(12) The radiographic (see 3.1.16) screen may be performed in any sequence after 3.1.8.
(13) Samples shall be selected for testing in accordance with the specific device class and lot requirements of method 5005.
(14) Class A devices have been deleted from MIL-STD-883 and MIL-M-38510. Pending a decision on additional Class S requirements, class (A) has been included in this data book.
(15) May use 80 hours at $150^{\circ} \mathrm{C}$.
(16) Refer MIL-STD-883, Method 5004 for complete details.

## Table 4-Group Electrical Tests.(1) Reference MIL-STD-883

| SUBGROUP(2) | CLASSES S (A) AND B <br> LTPD | (3) |
| :--- | :---: | :---: |
| Subgroup 1 <br> Static tests at $25^{\circ} \mathrm{C}$ | 5 |  |
| $\frac{\text { Subgroup 2 }}{\text { Static tests at maximum rated operating temperature }}$ |  |  |

## NOTES:

(1) The specific parameters to be included for tests in each subgroup shall be as specified in the applicable procurement document. Where no parameters have been identified in a particular subgroup or test within a subgroup, no group A testing is required for that subgroup or test to satisfy group $A$ requirements.
(2) A single sample may be used for all subgroup testing. Where the required size exceeds the lot size, $100 \%$ inspection shall be allowed (see 30.2 .5 of Appendix B of MIL-M-38510).
(3) Class A devices have been deleted from MIL-STD-883 and MIL-M-38510. Pending a decision on additional Class S requirements, class (A) has been included in this data book.

## Quality and Reliability

## Table 5-Group B Tests for Classes B and C. <br> (1) Reference MIL-STD-883 Method 5005

| TEST | MIL-STD-883 |  | CLASSES B AND C LTPD |
| :---: | :---: | :---: | :---: |
|  | METHOD | CONDITION |  |
| Subgroup 1 |  |  |  |
| a. Physical dimensions(2) | 2016 |  | 2 devices (no failures) |
| b. Internal water-vapor content ${ }^{(3)}$ | 1018 | $1,000 \mathrm{ppm}$ maximum water content at $100^{\circ} \mathrm{C}$ | 3 devices (no failures) |
| Subgroup 2 |  |  |  |
| a. Resistance to solvents | 2015 |  | 3 devices (no failures) |
| b. Internal visual and mechanical | 2014 | Failure criteria from design and construction requirements of applicable procurement document | 1 devices (no failures) |
| c. Bond strength (4) <br> (1) Thermocompression <br> (2) Ultrasonic or wedge <br> (3) Flip-chip <br> (4) Beam lead | 2011 | (1) Test condition $C$ or $D$ <br> (2) Test condition $C$ or $D$ <br> (3) Test condition F <br> (4) Test condition H | 15 |
| Subgroup 3 |  |  |  |
| Solderability (5) | 2003 | Soldering temperature of $260 \pm 10^{\circ} \mathrm{C}$. | 15 |

## NOTES:

(1) Electrical reject devices from the same inspection lot may be used for all subgroups when end-point measurements are not required.
(2) Not required for qualification or quality conformance inspections where group $D$ inspection is being performed on samples from the same inspection lot.
(3) This test is required only if the package contains a desiccant.
(4) Test samples for bond strength may, at the manufacturer's option, unless otherwise specified, be randomly selected immediately following internal visual (precap) inspection specified in Method 5004, prior to sealing. Unless otherwise specified, the LTPD sample size for condition C or $D$ is the number of bond pulls selected from a minimum number of 10 devices, and for conditions $F$ or $H$ is the number of dice (not bonds) (see Method 2011).
(5) All devices submitted for solderability test must have been through the temperature/time exposure specified for burn-in. The LTPD for solderability test applies to the number of leads inspected except in no case shall less than 3 devices be used to provide the number of leads required.

Table 5a-Group B Tests for Class S (A) Devices. (1) Reference MIL-STD-883 Method 5005

| TEST | MIL-STD-883 |  | $\begin{gathered} \text { CLASS S A }{ }^{(10)} \\ \text { QUANTITY/(ACCEPT NO.) } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: |
|  | METHOD | CONDITION | LOT 1 | LOT 2 AND SUBSEQUENT |
| Subgroup 1 <br> (a) Physical dimensions (2) <br> (b) Internal water-vapor content ${ }^{(3)}$ | $\begin{aligned} & 2016 \\ & 1018 \end{aligned}$ | $1,000 \mathrm{ppm}$ maximum water content at $100^{\circ} \mathrm{C}$ | $\begin{aligned} & 2(0) \\ & 3(0) \end{aligned}$ | $\begin{aligned} & 2(0) \\ & 3(0) \end{aligned}$ |
| Subgroup 2(4) <br> (a) Resistance to solvents <br> (b) Internal visual and mechanical <br> (c) Bond strength <br> (1) Thermocompression <br> (2) Ultrasonic <br> (3) Flip-chip <br> (4) Beam lead <br> (d) Die shear test | 2015 <br> 2013 <br> and <br> 2014 <br> 2011 <br> 2019 | Failure criteria from design and construction requirements of applicable procurement document <br> (1) Test condition $C$ or $D$ <br> (2) Test condition $C$ or $D$ <br> (3) Test condition F <br> (4) Test condition H <br> Per table I of Method 2019 for the applicable die size | $\begin{gathered} 3(0) \\ 2(0) \\ 2(0)^{(8)} \\ 3(0) \end{gathered}$ | $\begin{gathered} 3(0) \\ 2(0) \\ 2(0)^{(8)} \\ 3(0) \end{gathered}$ |
| Subgroup 3 <br> Solderability (5) | 2003 | Soldering temperature of $260 \pm 10^{\circ} \mathrm{C}$ | LTPD = 15 | LTPD = 15 |
| Subgroup 4 Lead integrity Seal (a) Fine <br> (b) Gross | $\begin{aligned} & 2004 \\ & 1014 \end{aligned}$ | Test condition $\mathrm{B}_{2}$, lead fatigue As applicable | 2(0) | 2(0) |

See footnotes at end of table.

## Table 5a-Group B Tests for Class S (A) Devices. (1) Reference MIL-STD-883 Method 5005 (Cont.)

| TEST | MIL-STD-883 |  | $\begin{gathered} \text { CLASS S A }{ }^{(10)} \\ \text { QUANTITY/(ACCEPT NO.) } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: |
|  | METHOD | CONDITION | LOT 1 | LOT 2 AND SUBSEQUENT |
| Subgroup 5(6)(7) <br> (a) Gate 1 <br> (1) Electrical parameters <br> (2) Steady state life (accelerated) <br> (3) Electrical parameters <br> (b) Gate 2 <br> (1) Steady state life (accelerated) <br> (2) Seal <br> a. Fine <br> b. Gross <br> (3) Electrical parameters | $\begin{aligned} & 1005 \\ & 1005 \\ & 1014 \end{aligned}$ | Group A, subgroup 1, 2, 3: Read and record <br> Group A, subgroups 4-11: Attributes <br> Condition $\mathrm{F}, 250^{\circ} \mathrm{C}, 120$ continuous hours minimum <br> Group A, subgroups 1, 2, 3: Read and record <br> Condition F, $250^{\circ} \mathrm{C}, 240$ hours minimum including actual gate 1 life test duration As applicable <br> Group A, subgroups 1, 2, 3: Read and record Group A, subgroups 4-11: Attributes | $40(8)$ $40(16)^{(9)}$ | $\begin{gathered} 10(2) \\ 10(4)(9) \end{gathered}$ |
| Subgroup 6(4) <br> (a) Electrical parameters <br> (b) Temperature cycling <br> (c) Constant acceleration <br> (d) Seal <br> (1) Fine <br> (2) Gross <br> (e) Electrical parameters | $\begin{aligned} & 1010 \\ & 2001 \\ & 1014 \end{aligned}$ | Group A, subgroups 1, 2, 3: Read and record Condition C 100 cycles $/ \mathrm{min}$ Test condition $\mathrm{E}: \mathrm{Y}_{1}$ orientation only <br> Group A, subgroups 1, 2, 3: Read and record | $\begin{gathered} 12(0) \\ \text { or } \\ 20(1) \end{gathered}$ | $5(0)$ <br> or $8(1)$ |

## NOTES:

(1) Electrical reject devices from the same inspection may be used for all subgroups when end-point measurements are not required.
(2) Not required for qualification or quality conformance inspections where group $D$ inspection is being performed on samples from the same inspection lot.
(3) This test is required only if the package contains a desiccant.
(4) For class $S$ lot quality conformance testing, all samples for subgroup $B 2$ must have been through the complete sequence of subgroup $B 6$ tests.
(5) All devices must have been through the temperature/time exposure in burn-in. The LTPD applies to the number of leads inspected except in no case shall less than three devices be used to provide the number of leads required.
(6) The alternate removal-of-bias provisions of 3.3 .1 and 3.2 . 1 of Methods 1005 and 1015 respectively shall not apply for test temperatures above $125^{\circ} \mathrm{C}$.
(7) At the manufacturer's option, an alternate life test may be performed in accordance with 3.8.2.
(8) All bonds on both devices shall be pulled or, for condition F or H , all dice shall be tested.
(9) Sample quantity for acceptance purposes is the incoming sample for gate 1 and the accept number applies to the total failures from both gate 1 and gate 2.
(10) Class A devices have been deleted from MIL-STD-883 and MIL-M-38510. Pending a decision on additional Class S requirements, class (A) has been included in this data book.

Table 6-Group C (Die-Related Tests) (for Classes B and C Only). Reference MIL-STD-883 Method 5005

| TEST | MIL-STD-883 |  | LTPD |
| :---: | :---: | :---: | :---: |
|  | METHOD | CONDITION |  |
| Subgroup 1 <br> Steady state life test ${ }^{(1)}$ <br> End-point electrical parameters | 1005 | Test condition to be specified ( 1,000 hours at $125^{\circ} \mathrm{C}$ ) As specified in the applicable device specification | 5 |
| Subgroup 2 <br> Temperature cycling <br> Constant acceleration <br> Seal <br> (a) Fine <br> (b) Gross <br> Visual examination <br> End-point electrical parameters | 1010 <br> 2001 <br> 1014 <br> (2) | Test condition C <br> Test condition E min (for large packages, see 3) <br> $\mathrm{Y}_{1}$ orientation only <br> As applicable <br> As specified in the applicable device specification | 15 |

## NOTES:

(1) See 40.4 of Appendix B of MIL-M-38510.
(2) Visual examination shall be in accordance with Method 1010 or 1011.

Table 7-Group D (Package Related Tests) (for All classes).
Reference MIL-STD-883 Method 5005

| TEST | MIL-STD-883 |  | LTPD |
| :---: | :---: | :---: | :---: |
|  | METHOD | CONDITION |  |
| Subgroup 1 <br> (a) Physical dimensions <br> (b) Internal water-vapor content | $\begin{aligned} & 2016 \\ & 1018 \end{aligned}$ | $5,000 \mathrm{ppm}$ maximum water content at $100^{\circ} \mathrm{C}$ | 15 <br> 3 devices (no failures) |
| Subgroup 2(1) <br> Lead integrity Seal <br> (a) Fine <br> (b) Gross | $\begin{aligned} & 2004 \\ & 1014 \end{aligned}$ | Test condition B2 (lead fatigue) As applicable | 15 |
| Subgroup 3(2) <br> Thermal shock <br> Temperature cycling Moisture resistance Seal <br> (a) Fine <br> (b) Gross <br> Visual examination End-point electrical parameters (4) | $\begin{aligned} & 1011 \\ & 1010 \\ & 1004 \\ & 1014 \end{aligned}$ | Test condition $B$ as a minimum, 15 cycles minimum <br> Test condition C, 100 cycles minimum <br> As applicable <br> Per visual criteria of Method 1004 <br> As specified in the applicable device specification | 15 |
| Subgroup 4(2) <br> Mechanical shock Vibration variable frequency Constant acceleration Seal <br> (a) Fine <br> (b) Gross <br> Visual examination End-point electrical parameters | $\begin{aligned} & 2002 \\ & 2007 \\ & 2001 \\ & 1014 \end{aligned}$ | Test condition B <br> Test condition A <br> Test condition E (see 3 ), $\mathrm{Y}_{1}$ orientation only <br> As applicable <br> As specified in the applicable device specification | 15 |
| Subgroup 5(1) <br> Salt atmosphere <br> Seal <br> (a) Fine <br> (b) Gross <br> Visual examination | $\begin{aligned} & 1009 \\ & 1014 \end{aligned}$ | Test condition A As applicable <br> Per visual criteria of Method 1009 | 15 |

## NOTES:

(1) Electrical reject devices from that same inspection lot may be used for samples.
(2) Devices used in subgroup 3, "Thermal and Moisture Resistance" may be used in subgroup 4, "Mechanical."
(3) Visual examination shall be in accordance with Method 1010 or 1011.
(4) At the mariufacturer's option, end-point electrical parameters may be performed after moisture resistance and prior to seal test.
NOTICE

Tables 3, 4, 5, 6 and 7 are referenced from MIL-STD-883. These are for reference only. All required test, screening procedures, classes or subgroup levels, whether in addition to or apart from any military standards must be specified on the purchase order and agreed upon in writing by Ravtheon Co.

## Introduction

Raytheon's A+ program is designed to provide the Industrial and Commercial marketplace with product reliability. © Reliability consistent with application requirements. ■ Reliability that avoids an overbuy situation where the user pays for screening beyond the scope of his needs.

Raytheon offers three screening flows under the A+ program. Each having a separate reliability factor and cost saving. When deciding which A+ flow best suits your needs, you should consider the cost savings realized through elimination of outside lab services and the need to tighten incoming inspection. Users who do not presently have their integrated circuits screened should consider the cost of component replacement during system test and in the field. Substantial cost savings can now be realized by specifying Raytheon's A+ program.

The designations $A+1$ and $A+2$ are used for epoxy $B$ packaged devices only. $A+3$ is reserved for ceramic devices. The appropriate screening level may be specified by simply adding the proper A+ suffix to the Raytheon part number, i.e., - - RC4136DB with A+2 screening would be designated RC4136DB2.

Customers who use the epoxy package may wish to obtain a copy of the Epoxy Encapsulated Linear I.C. Quality Review, available from your local Raytheon sales office.

## Basic Reliability Measures

Raytheon has instituted an internal program to assure that products bearing the Raytheon logo are unsurpassed in reliability when used in the industrial environment. Several tests, including some normally reserved for military products, are applied to our industrial products on a continuing basis in support of this effort. A brief summary of these tests is given below.

## 1. Monitored Burn-In (all packages)

24 hours at $+125^{\circ} \mathrm{C}$ with zero failures allowed. This RVT (reliability verification test), a Raytheon exclusive, is performed on 20 samples from each manufacturing lot.

## 2. Standard Burn-In (all packages)

168 hours at $+125^{\circ} \mathrm{C}, 1 \%$ PDA. This RVT is performed on 45 samples from each EIA data code.

## 3. Operating Life (all packages)

1000 hours at $+125^{\circ} \mathrm{C}$, LTPD $=5$. This RVT is performed on all new products and periodically on existing product types as an indicator of long-term reliability.

## 4. Steam Pressure (epoxy packages only)

24 hours at $+125^{\circ} \mathrm{C}$ in steam vapor. This RVT is performed on 25 samples from each EIA data code as to assure package and device integrity.

## 5. $85 / 85$ (epoxy packages only)

168 hours with bias at $+85^{\circ} \mathrm{C}$ and $85 \%$ relative humidity. This RVT is performed on 25 samples from each EIA data code also as an indicator of package and device integrity.

## 6. Temperature Cycle (epoxy packages only)

100 cycles per method $1010.1,0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$. This RVT is performed on 25 samples from each EIA date code to mechanically stress the wire bond, die bond and package material.

## 7. Military Flow (ceramic packages and metal-cans)

Only dice lots which pass MIL-STD-883 condition B visual tests are used in these packages and the 883 class B flow is used up to point of electrical test. This provides military type product reliability at commercial prices.

## A+ Programs Increase Reliability

Raytheon's A+ programs were designed to provide an even greater reliability assurance than standard process testing. Starting with devices which are processed with the basic reliability measures, various combinations of temperature cycle, burn-in, Hot Rail testing and tightened AQL lot acceptance are available as shown in the flow chart. The objectives of these $100 \%$ screens are:

## 1. Temperature Cycle (epoxy packages only)

$0^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$ per method 1011 , condition A . This is the first screening for the $A+1$ and $A+2$ flows. ( $A+3$ ceramic and metal-can devices received temperature cycles as part of standard product flow.) The purpose of this screening is to stress wire bonds and die bonds mechanically to prove the integrity of the devices.

## 2. Burn-In (all packages)

168 hours at $+125^{\circ} \mathrm{C}$ or equivalent up to $200^{\circ} \mathrm{C}$. This screening is performed in $A+2$ and $A+3$ flows.

[^2]

* Must be expressed as a range since a normally controlled environment (constant power and temperature) cannot be assured.


## OP AMPS

Average Input Offset Current $\mathbf{t}^{\circ}$ Coefficient-Change in input offset current divided by change in ambient temperature producing it.
Average Input Offset Voltage $t^{\circ}$ Coefficient-Change in input offset voltage divided by change in ambient temperature producing it.
Common-Mode Input Resistance-Resistance looking into both inputs tied together.
Common-Mode Rejection Ratio (CMRR)-Ratio of change of input offset voltage to input common-mode voltage change producing it.
Full Power Bandwidth-Maximum frequency at which full sinewave output might be obtained.
Input Bias Current-Average of the two input currents at zero output voltage. In some cases, input current for either input independently.
Input Capacitance-Capacitance looking into either input terminal with other grounded.
Input Current-Current into an input terminal.
Input Noise Voltage-Square root of mean square narrow-band noise voltage referred to input.
Input Offset Current-Difference in currents into two input terminals with output at zero volts.
Input Offset Voltage-Voltage which must be applied between input terminals to obtain zero output voltage. Input offset voltage may also be defined for case where two equal resistances are inserted in series with input leads.

Input Resistance-Resistance looking into either input terminal with other grounded.
Input Voltage Range-Range of voltages on input terminals for which amplifier operates within specifications. In some cases, input offset specifications apply over input voltage range.

Large-Signal Voltage Gain-Ratio of maximum output voltage swing to change in input voltage required to drive output to this voltage.
Output Resistance-Resistance seen looking into output terminal with output at null. This parameter is defined only under small signal conditions at frequencies above a few hundred cycles to eliminate influence of drift and thermal feedback.
Settling Time-Time between initiation of input step function and time when output voltage has settled to within specified error band of final output voltage.
Output Short-Circuit Current-Maximum output current available from amplifier with output shorted to ground or to either supply.
Output Voltage Swing-Peak output swing, referred to zero, that can be obtained.
Power Consumption-DC power required to operate amplifier with output at zero and with no load current.

Power Supply Rejection Ratio-Ratio of change in input offset voltage to change in supply voltages producing it.
Rise Time-Time required for an output voltage step to change from $10 \%$ to $90 \%$ of its final value.
Slew Rate-Maximum rate of change of output voltage under large signal condition.

Supply Current-Current required from power supply to operate amplifier with no load and output at zero.

Temperature Stability Of Voltage Gain-Maximum variation of voltage gain over specified temperature range.
Harmonic Distortion-Percentrage of harmonic distortion being defined as 100 times ratio of RMS sum of harmonics to fundamental.
$\%$ harmonic distortion $=$

$$
\frac{\left(v_{2}^{2}+v_{3}^{3}+v_{4}^{2}+\ldots\right)^{1 / 2}(100 \%)}{v_{1}}
$$

where $V_{1}$ is RMS amplitude of fundamental and $V_{2}, V_{3}, V_{4}$, . . . are RMS amplitudes of individual harmonics.
Transient Response-Closed-loop step-function response of amplifier under small-signal conditions.

Unity Gain Bandwidth-Frequency range from DC to frequency where amplifier open-loop gain rolls off to one.
Voltage Gain-Ratio of output voltage to input voltage under stated conditions for source resistance ( $\mathrm{R}_{\mathrm{S}}$ ) and load resistance ( $\mathrm{R}_{\mathrm{L}}$ ).
Bandwidth-Frequency at which voltage gain is reduced to $1 / \sqrt{ } 2$ times the low frequency value.
Output Impedance-Ratio of output voltage to output current under stated conditions for source resistance ( $\mathrm{R}_{\mathrm{S}}$ ) and load resistance ( $\mathrm{R}_{\mathrm{L}}$ ).

Input Impedance-Ratio of input voltage to input current under stated conditions for source resistance ( $\mathrm{R}_{\mathrm{S}}$ ) and load resistance ( $\mathrm{R}_{\mathrm{L}}$ ).

## REGULATORS

Dropout Voltage-Input-output voltage differential at which circuit ceases to regulate against further reductions in input voltage.
Input-Output Voltage Differential-Range of voltage difference between supply voltage and regulated output voltage over which regulator will operate.
Line Regulator-Percentage change in output voltage for a specified change in input voltage.
Load Regulator-Percentage change in output voltage for specified change in load current.
Maximum Power Dissipation-Maximum total device dissipation for which regulator will operate within specifications.
Output Noise Voltage-RMS output noise voltage with constant load and no input ripple.

Output Voltage Range-Range of output voltage over which regulator will operate.
Quiescent Current-Part of input current to regulator that is not delivered to load.
Reference Voltage-Output of reference amplifier measured with respect to negative supply.
Ripple Rejection-Ratio of peak-to-peak input ripple voltage to peak-to-peak output ripple voltage.
Sense Voltage-Voltage between current sense and current limit terminals necessary to cause current limiting.
Short-Circuit Current Limit-Output current of regulator with output shorted to negative supply.
Standby Current Drain-Supply current drawn by regulator with no output load and no reference voltage load.
Temperature Stability-Percentage change in output voltage for thermal variation from room temperature to either temperature extreme.
Long Term Stability-Output voltage stability under accelerated life-test conditions at $125^{\circ} \mathrm{C}$ with maximum rated voltages and power dissipation for 1000 hours.
Output Voltage Scale Factor-Output voltage obtained for unit value of resistance between adjustment terminal and ground.
Input Voltage Range-Range of DC input voltages over which regulator will operate within specifications.
Current-Limit Sense Voltage-Voltage across current limit terminals required to cause regulator to current-limit with short-circuited output. This voltage is used to determine value of external current-limit resistor when external booster transistors are used.

## COMPARATORS/SENSE AMPLIFIERS

Common-Mode Firing Voltage-CM input voltage that exceeds dynamic range of inputs with strobe enabled resulting in output switching states.
Common-Mode Recovery Time-Time from turn off of CM signal to analog input threshold of earliest sense line pulse signal that can be processed normally. Processed normally refers to bi-polar signals greater than or less than input threshold with corresponding proper output.
Equivalent Input Common-Mode Noise Voltage-Change in input offset voltage due to common-mode input noise.
Logic Input High Voltage-Minimum voltage allowed at bit control gate to hold bit off.
Logic Input Low Voltage-Maximum voltage allowed at bit control gate to hold bit on.
Output Sink Current-Maximum negative current that can be delivered by comparator.

Peak Output Current-Maximum current that may flow into output load without causing damage to comparator.
Propagation Delay-Interval between application of an input voltage step and its arrival at either output, measured at $50 \%$ of final value.
Response Time-Interval between application of input step function and time when output crosses logic threshold voltage. Input step drives comparator from some initial, saturated input voltage to input level just barely in excess of that required to bring output from saturation to logic threshold voltage overdrive.
Strobe Current-Maximum current drawn by strobe terminals when it is at zero logic level.
Strobe Delay-Time delay measured from strobe to output threshold with signal present exceeding input threshold.
Strobe Release Time-Time required for output to rise to logic threshold voltage after strobe terminal has been driven from zero to one logic level. Appropriate input conditions are assumed.
Strobed Output Level - DC output voltage, independent of input voltage, with voltage on strobe terminal equal to or less than minimum specified amount.
Switching Speed-Time required to turn on least significant bit.
Threshold Uncertainty-With all sense amps sharing same input threshold less uncertainty as " 0 ." This includes unit to unit, power supply and temperature variations.

Threshold Voltage-Typical referred to input voltage which determines whether input is " 1 " or " 0 ." Signal whose magnitude is greater than threshold level is sensed as logic " 1 " and signal whose magnitude is less as " 0 ."
Zero Scale Output Current-Output current for all bits turned off.
Supply Current-Current required from positive or negative supply to operate comparator with no output load. Power will vary with input voltage, but is specified as maximum for entire range of input voltage conditions.
Voltage Gain-Ratio of change in output voltage to change in voltage between input terminals producing it.
Differential Input Offset Current-Absolute difference in two input bias currents of one differential input.
Differential Input Overload Recovery Time-Time necessary for device to recover from 2 V differential pulse ( $\mathrm{t}_{\mathrm{f}}=\mathrm{t}_{\mathrm{r}}=20 \mathrm{~ns}$ ) prior to strobe enable signal.
Offset Voltage-Difference between absolute values of threshold voltage in positive- and negative-going directions.
Input Bias Current-Average of two input currents.
Input Offset Current-Absolute value of difference between two input currents for which output will be driven higher or lower than specified voltages.

## Glossary of Terms

Input Offset Voltage-Absolute value of voltage between input terminals required to make output voltage greater or less than specified voltages.
Input Voltage Range-Range of voltage on input terminals (common-mode) over which offset specifications apply.
Positive Output Level-High output voltage level with given load and input drive equal to or greater than specified value.
Power Consumption-Power required to operate comparator with no output load. Power will vary with signal level, but is specified as maximum for entire range of input signal conditions.
Output Leakage Current-Current into output terminal with output voltage within given range and input drive equal to or greater than given value.
Output Resistance-Resistance seen looking into output terminal with DC output level at logic threshold voltage.

Strobed Output Level - DC output voltage, independent of input conditions, with voltage on strobe terminal equal to or less than specified low state.
Strobe ON Voltage-Maximum voltage on either strobe terminal required to force output to specified high state independent of input voltage.
Differential Input Threshold Voltage-DC input voltage which forces logic output to logic threshold voltage ( $\sim 1.5 \mathrm{~V}$ ) level.
Input Bias Current-DC current which flows into each input pin with differential input of OV.
Negative Output Level-Negative DC output voltage with comparator saturated by differential input equal to or greater than specified voltage.
Strobe OFF Voltage-Minimum voltage on strobe terminal that will guarantee that it does not interfere with operation of comparator.

## SECTION 1

## Operational Amplifiers

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## GENERAL DESCRIPTION

The LM101A/LM201A and LM301A are general purpose, high performance operational amplifiers fabricated monolithically on a silicon chip by the planar epitaxial process. The units may be fully compensated with the addition of a 30 pF capacitor stabilizing the circuit for all feedback configurations including capacitive loads.

The device may be operated as a comparator with a differential input as high as $\pm 30 \mathrm{~V}$. Used as a comparator the output can be clamped at any desired level to make it compatible with logic circuits.
The LM101A operational amplifier will operate over the full military temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The commercial version, the LM301A operates over a temperature range from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$..
The LM201A is the same as the LM101A except its performance is guaranteed from $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Offset Voltage 3mV Maximum Over Temperature
- Input Current 100nA Maximum Over Temperature
- Offset Current 20nA Maximum Over Temperature
- Offsets Guaranteed Over Entire Common-Mode Range and Supply Voltage Range
- Frequency Compensation 30pF
- Supply Voltage $\pm 5 \mathrm{~V}$ to $\pm 20 \mathrm{~V}$


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION

| CQ Flatpak |
| :---: |
| (Top View) |

Metal Can Package
(Top View)

NOTE: THE LM101A/301A IS AVAILABLE ON SPECIAL ORDER IN THE DC (14-PIN) CERAMIC DIP PACKAGE.

ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\text { 101A, 201A: } \pm 22 \mathrm{~V}$ | Operating Temperature Range LM101A | C |
| :---: | :---: | :---: | :---: |
| Power Dissipation (Note 1) | 500 mW | LM201A | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ | LM301A | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | $\pm 15 \mathrm{~V}$ | Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Output Short-Circuit Duration (Note 3) | Indefinite | Lead Temperature (Soldering, 60s) | $300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS LM101A, LM201A: $\pm 5 \mathrm{~V} \leqslant \mathrm{~V}_{S} \leqslant \pm 20 \mathrm{~V}$; LM $301 \mathrm{~A}: \pm 5 \leqslant \mathrm{~V}_{S} \leqslant \pm 15 \mathrm{~V}$ (Note 4)

| PARAMETER | CONDITIONS | LM101A, LM201A |  |  | LM301A |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25{ }^{\circ} \mathrm{C}, \mathrm{RS} \leqslant 50 \mathrm{k} \Omega$ |  | 0.7 | 2.0 |  | 2.0 | 7.5 | mV |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 1.5 | 10 |  | 3 | 50 | nA |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 30 | 75 |  | 70 | 250 | nA |
| Input Resistance | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 1.5 | 4 |  | 0.5 | 2 |  | $\mathrm{M} \Omega$ |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 20 \mathrm{~V}$ |  | 1.8 | 3.0 |  | 1.8 | 3.0 | mA |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{~V},= \pm 15 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{OUT}}= \pm 10 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \end{aligned}$ | 50 | 160 |  | 25 | 160 |  | $\mathrm{V} / \mathrm{mV}$ |
| Input Offset Voltage | RS $\leqslant 50 \mathrm{k} \Omega$ |  |  | 3.0 |  |  | 10 | mV |
| Average Temperature Coefficient of Input Offset Voltage |  |  | 3.0 | 15 |  | 6.0 | 30 | $\mu \mathrm{V} / \mathrm{OC}$ |
| Input Offset Current |  |  |  | 20 |  |  | 70 | nA |
| Average Temperature Coefficient of Input Offset Current | $\begin{aligned} & 25^{\circ} \mathrm{C} \leqslant T_{A} \leqslant 125^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \leqslant T_{A} \leqslant 70^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C} \leqslant T_{A} \leqslant 25^{\circ} \mathrm{C} \\ & 0{ }^{\circ} \mathrm{C} \leqslant T_{A} \leqslant 25{ }^{\circ} \mathrm{C} \end{aligned}$ |  | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ | $\begin{aligned} & 0.1 \\ & 0.2 \end{aligned}$ |  | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.6 \end{aligned}$ | $n A / 0 \mathrm{C}$ <br> $n A /{ }^{\circ} \mathrm{C}$ <br> $n A /{ }^{\circ} \mathrm{C}$ <br> nA/oc |
| Input Bias Current |  |  |  | 100 |  |  | 300 | nA |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=+125^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 20 \mathrm{~V}$ |  | 1.2 | 2.5 |  |  |  | mA |
| Large Signal Voltage Gain | $\begin{aligned} & V_{S}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}= \pm 10 \mathrm{~V} \\ & R_{L} \geqslant 2 \mathrm{k} \Omega \end{aligned}$ | 25 |  |  | 15 |  |  | V/mV |
| Output Voltage Swing | $\begin{aligned} & V_{S}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \\ & \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \end{aligned}$ | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \text { v } \\ & \text { v } \end{aligned}$ |
| Input Voltage Range | LM101A: $\mathrm{V}_{\mathrm{S}}= \pm 20 \mathrm{~V}$; <br> LM301A: $V_{S}= \pm 15 \mathrm{~V}$ | $\pm 15$ |  |  | $\pm 12$ |  |  | V |
| Common Mode Rejection Ratio | RS $\leqslant 50 \mathrm{k} \Omega$ | 80 | 96 |  | 70 | 90 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k} \Omega$ | 80 | 96 |  | 70 | 96 |  | dB |

## NOTES:

1. For operating at elevated temperatures, the device must be derated based on $+150^{\circ} \mathrm{C}$ for $\mathrm{LM} 101 \mathrm{~A},+100^{\circ} \mathrm{C}$ for LM 201 A and LM 301 A, maximum junction temperature and a thermal resistance of $150^{\circ} \mathrm{C} / \mathrm{W}$ junction to ambient or $45^{\circ} \mathrm{C} / \mathrm{W}$ junction to case.
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Continuous short-circuit is allowed for case temperatures to $+125^{\circ} \mathrm{C}$ and ambient temperatures to $+75^{\circ} \mathrm{C}$ for LM 101 A, case temperatures to $+70^{\circ} \mathrm{C}$ and ambient temperatures to $+55^{\circ} \mathrm{C}$ for LM301A.
4. Specifications apply for temperature ranges: LM101A: $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$; LM201A: $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$; $\mathrm{LM} 301 \mathrm{~A}: 0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ unless otherwise specified.

## GENERAL DESCRIPTION

The LM107, LM207, and LM307 high-gain, general purpose operational amplifiers are monolithically constructed and internally compensated. The addition of a 30pF MOS capacitor guarantees unconditional stability eliminating the need for external frequency compensation. Input currents are a factor of ten lower than an industry standard device such as the 709, LM101, and 741.

This series offers all the best features of the LM101. In addition, the devices provide better accuracy and lower noise in high impedance circuitry.
The LM107 operates over a temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The LM307 operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.
The LM207 is the same as the LM107 except its performance is guaranteed from $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Offset Voltage 3mV Maximum Over Temperature
- Input Current 100nA Maximum Over Temperature
- Offset Current 20nA Maximum Over Temperature
- Offsets Guaranteed Over Entire Common-Mode Range and Supply Voltage Range
- Internal Frequency Compensation
- Supply Voltage $\pm 5 \mathrm{~V}$ to $\pm 20 \mathrm{~V}$


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS



ELECTRICAL CHARACTERISTICS LM107A, LM $207 A: \pm 5 \mathrm{~V} \leqslant \mathrm{~V}_{\mathrm{S}} \leqslant \pm 20 \mathrm{~V}$; LM $307 \mathrm{~A}: \pm 5 \leqslant \mathrm{~V}_{\mathrm{S}} \leqslant \pm 15 \mathrm{~V}$ (Note 4)

| PARAMETER | CONDITIONS | LM107/207 |  |  | LM307 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{TA}^{\prime}=25{ }^{\circ} \mathrm{C}, \mathrm{RS} \leqslant 50 \mathrm{k} \Omega$ |  | 0.7 | 2.0 |  | 2.0 | 7.5 | mV |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 1.5 | 10 |  | 3 | 50 | $n \mathrm{~A}$ |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 30 | 75 |  | 70 | 250 | $n \mathrm{~A}$ |
| Input Resistance | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 1.5 | 4 |  | 0.5 | 2 |  | $\mathrm{M} \Omega$ |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 20 \mathrm{~V}$ |  | 1.8 | 3.0 |  | 1.8 | 3.0 | mA |
| Large Signal Voltage Gain | $\begin{aligned} & T_{A}=25^{\circ} \mathrm{C}, \mathrm{~V}_{S}= \pm 15 \mathrm{~V} \\ & \mathrm{~V}_{\text {OUT }}= \pm 10 \mathrm{~V}, R_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \end{aligned}$ | 50 | 160 |  | 25 | 160 |  | V/mV |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k} \Omega$ |  |  | 3.0 |  |  | 10 | mV |
| Average Temperature Coefficient of Input Offset Voltage |  |  | 3.0 | 15 |  | 6.0 | 30 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Offset Current |  |  |  | 20 |  |  | 70 | $n \mathrm{~A}$ |
| Average Temperature Coefficient of Input Offset Current | $\begin{aligned} & 25^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 125^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \leqslant \mathrm{TA}_{A} \leqslant 70^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 25^{\circ} \mathrm{C} \\ & 0^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 25^{\circ} \mathrm{C} \end{aligned}$ |  | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ | $\begin{aligned} & 0.1 \\ & 0.2 \end{aligned}$ |  | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.6 \end{aligned}$ | $n \mathrm{~A} /{ }^{\circ} \mathrm{C}$ <br> nA/ ${ }^{\circ} \mathrm{C}$ <br> $n A /{ }^{\circ} \mathrm{C}$ <br> $n A /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current |  |  |  | 100 |  |  | 300 | $n \mathrm{~A}$ |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=+125^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 20 \mathrm{~V}$ |  | 1.2 | 2.5 |  |  |  | mA |
| Large Signal Voltage Gain | $\begin{aligned} & V_{S}= \pm 15 \mathrm{~V}, V_{\text {OUT }}= \pm 10 \mathrm{~V} \\ & R_{L} \geqslant 2 \mathrm{k} \Omega \end{aligned}$ | 25 |  |  | 15 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | $\begin{aligned} & V_{S}= \pm 15 \mathrm{~V}, R_{\mathrm{L}}=10 \mathrm{k} \Omega \\ & R_{\mathrm{L}}=2 \mathrm{k} \Omega \end{aligned}$ | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Input Voltage Range | $\mathrm{V}_{\mathrm{S}}= \pm 20 \mathrm{~V}$ | $\pm 15$ |  |  | $\pm 12$ |  |  | V |
| Common Mode Rejection Ratio | $\mathrm{RS} \leqslant 10 \mathrm{k} \Omega$ | 80 | 96 |  | 70 | 90 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 80 | 96 |  | 70 | 96 |  | dB |

## NOTES:

 junction temperature and a thermal resistance of $150^{\circ} \mathrm{C} / \mathrm{W}$ junction to ambient or $45^{\circ} \mathrm{C} / \mathrm{W}$ junction to case.
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
. Continuous short-circuit is allowed for case temperatures to $+125^{\circ} \mathrm{C}$ and ambient temperatures to $+75^{\circ} \mathrm{C}$ for LM 107 , case temperatures to $+70^{\circ} \mathrm{C}$ and ambient temperatures to $+55^{\circ} \mathrm{C}$ for LM307.
 specified.

## GENERAL DESCRIPTION

The LM108A/LM108, LM208A/LM208 and LM308A/LM308 are Super Beta operational amplifiers fabricated on single silicon chips using the planar epitaxial process.
The LM108A/LM108 offer specifications an order of magnitude better than FET amplifiers over a temperature range $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.
The LM208A/LM208 are identical to the LM108A/LM108 except their performance is guaranteed from $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$.
The LM308A/LM308 provide lower input offset voltage of 0.5 mV maximum, and drift characteristics of $5.0 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ maximum. These devices can be compensated by the conventional technique used with the LM101/LM101A series.

## DESIGN FEATURES

- Offset Voltage Over Temperature Range 0.5 mV Maximum
- Input Current Over Temperature Range 3.OnA Maximum
- Offset Current Over Temperature Range 400pA Maximum
- Supply Current Only $400 \mu \mathrm{~A}$
- Guaranteed Drift Characteristics $5.0 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Maximum
- Supply Voltage $\pm 2 \mathrm{~V}$ to $\pm 20 \mathrm{~V}$


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



ABSOLUTE MAXIMUM RATINGS

| Supply Voltage $\ldots \ldots \ldots .$LM108A/LM108: $\pm 20 \mathrm{~V}$ <br> LM208A/LM208: $\pm 20 \mathrm{~V}$ <br> LM308A/LM308: $\pm 18 \mathrm{~V}$ | Operating Temperature Range LM108A/LM108 . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| :---: | :---: |
| Power Dissipation (Note 1) . . . . . . . . . . . . . . . . 500mW | LM208A/LM208 . . . . . . . . . . . . . . $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Differential Input Current (Note 3) . . . . . . . . . $\pm 10 \mathrm{~mA}$ | LM308A/LM308 . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ 的 $+70^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) . . . . . . . . . . . . . . . . . . . $\pm 15 \mathrm{~V}$ | Storage Temperature Range . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Output Short-Circuit Duration . . . . . . . . . . . Indefinite | Lead Temperature (Soldering, 60s) . . . . . . . . . . $300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS (Notes 4 and 5)

| PARAMETER | CONDITIONS | LM108A/LM208A |  |  | LM308A |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 0.3 | 0.5 |  | 0.3 | 0.5 | mV |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{~V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \\ & \mathrm{~V}_{\text {out }}= \pm 10 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega \end{aligned}$ | 80 | 300 |  | 80 | 300 |  | $\mathrm{V} / \mathrm{mV}$ |
| Input Offset Voltage |  |  |  | 1.0 |  |  | 0.73 | mV |
| Average Temperature Coefficient of Input Offset Voltage |  |  | 1.0 | 5.0 |  | 1.0 | 5.0 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\text {out }}= \pm 10 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega \end{aligned}$ | 40 |  |  | 60 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| Common Mode Rejection Ratio |  | 96 | 110 |  | 96 | 110 |  | dB |
| Supply Voltage Rejection Ratio |  | 96 | 110 |  | 96 | 110 |  | dB |
| PARAMETER | CONDITIONS | LM108/LM208 |  |  | LM308 |  |  | UNITS |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 0.7 | 2.0 |  | 2.0 | 7.5 | mV |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 0.05 | 0.2 |  | 0.2 | 1.0 | nA |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 0.8 | 2.0 |  | 1.5 | 7.0 | nA |
| Input Resistance | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 30 | 70 |  | 10 | 40 |  | $\mathrm{M} \Omega$ |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 0.3 | 0.6 |  | 0.3 | 0.8 | mA |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{T}_{A}=25^{\circ} \mathrm{C}, \mathrm{~V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \\ & \mathrm{~V}_{\text {out }}= \pm 10 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega \end{aligned}$ | 50 | 300 |  | 25 | 300 |  | $\mathrm{V} / \mathrm{mV}$ |
| Input Offset Voltage |  |  |  | 3.0 |  |  | 10 | mV |
| Average Temperature Coefficient of Input Offset Voltage |  |  | 3.0 | 15 |  | 6.0 | 30 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Offset Current |  |  |  | 0.4 |  |  | 1.5 | nA |
| Average Temperature Coeffiecient of Offset Current |  |  | 0.5 | 2.5 |  | 2.0 | 10 | $\mathrm{pA} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current |  |  |  | 3.0 |  |  | 10 | nA |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=+125^{\circ} \mathrm{C}$ |  | 0.15 | 0.4 |  |  |  | mA |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\text {out }}=+10 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega \end{aligned}$ | 25 |  |  | 15 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | $\pm 13$ | $\pm 14$ |  | $\pm 13$ | $\pm 14$ |  | V |
| Input Voltage Range | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ | $\pm 13.5$ |  |  | 14 |  |  | V |
| Common Mode Rejection Ratio |  | 85 | 100 |  | 80 | 100 |  | dB |
| Supply Voltage Rejection Ratio |  | 80 | 96 |  | 80 | 96 |  | dB |

## NOTES:

1. For operating at elevated temperatures, the device must be derated based on $+150^{\circ} \mathrm{C}$ for $\mathrm{LM} 108,+100^{\circ} \mathrm{C}$ for LM 308 maximum junction temperature and a thermal resistance of $150^{\circ} \mathrm{C} / \mathrm{W}$ junction to ambient or $45^{\circ} \mathrm{C} / \mathrm{W}$ junction to case.
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. The inputs are shunted with back-to-back diodes for overvoltage protection. Therefore, excessive current will flow if a differential input voltage in excess of 1 V is applied between the inputs unless some limiting resistance is used.
4. These specifications apply for $\pm 5 \mathrm{~V}<\mathrm{V}_{S}< \pm 20 \mathrm{~V}$ and $-55^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}, \mathrm{LM} 108 \mathrm{~A} / \mathrm{LM} 108 ; \pm 5 \mathrm{~V}<\mathrm{V}_{\mathrm{S}}< \pm 20 \mathrm{~V}$ and $-25^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+85^{\circ} \mathrm{C}$, LM208A/LM208.
5. These specifications apply for $\pm 5 \mathrm{~V}<\mathrm{V}_{S}< \pm 15 \mathrm{~V}$ and $0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+70^{\circ} \mathrm{C}, \mathrm{LM} 308 \mathrm{~A} / \mathrm{LM} 308$.

## GENERAL DESCRIPTION

The LM118, LM218, and LM318 are precision operational amplifiers which offer fast slewing and wide bandwidth. They feature internal frequency compensation and ten times the speed of general purpose amplifiers.
External feedforward compensation may be used for an additional increase in speed. For inverting applications this will increase the slew rate to more than $150 \mathrm{~V} / \mu \mathrm{s}$ and almost double the bandwidth. (Feedforward is not used for non-inverting or differential applications.)
Their high speed and fast settling time make them ideal devices for A/D converters, oscillators, active filters, sample-and-hold circuits, as well as general purpose amplifiers.
The LM118 military version operates over a temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The LM218 is the same as the LM118 except its performance is guaranteed from $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. The LM318 operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- 15 MHz Small Signal Bandwidth
- Guaranteed 50V/ $\mu \mathrm{s}$ Slew Rate
- Operates from $\pm 5 \mathrm{~V}$ to $\pm 20 \mathrm{~V}$ Supply
- Internal Frequency Compensation
- Input and Output Overload Protected
- Pin Compatible With General Purpose Op Amps


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS



ELECTRICAL CHARACTERISTICS (Note 4)

| PARAMETER | CONDITIONS | LM118/LM218 | LM318 | UNITS |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input Offset Voltage | $\mathrm{TA}^{\prime}=25^{\circ} \mathrm{C}$ | 4 | 10 | mV | Max. |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 50 | 200 | nA | Max. |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 250 | 500 | $n \mathrm{~A}$ | Max. |
| Input Resistance | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 1 | 0.5 | $\mathrm{M} \Omega$ | Min. |
| Supply Current | $\mathrm{TA}=25^{\circ} \mathrm{C}$ | 8 | 10 | mA | Max. |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{T}_{A}=25{ }^{\circ} \mathrm{C}, \mathrm{~V}_{S}= \pm 15 \mathrm{~V}, \\ & \mathrm{~V}_{\text {OUT }}= \pm 10 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \end{aligned}$ | 50 | 25 | $\mathrm{V} / \mathrm{mV}$ | Min. |
| Input Offset Voltage |  | 6 | 15 | mV | Max. |
| Small Signal Bandwidth | $\mathrm{T}_{\mathrm{A}}=25{ }^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ | 15 | 15 | MHz | Typ. |
| Slew Rate | $\begin{aligned} & T_{A}=250^{\circ} \mathrm{C}, \mathrm{VS}= \pm 15 \mathrm{~V}, \mathrm{AV}=1 \\ & \mathrm{RS}=10 \mathrm{k} \Omega \end{aligned}$ | 50 | 50 | $\mathrm{V} / \mu \mathrm{s}$ | Min. |
| Input Offset Current |  | 100 | 300 | nA | Max. |
| Input Bias Current |  | 500 | 750 | nA | Max. |
| Supply Current | $T_{A}=T_{M A X}$ | 7 |  | mA | Max. |
| Large Signal Voltage Gain | $\begin{aligned} & V_{S}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}= \pm 10 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \end{aligned}$ | 25 | 20 | $\mathrm{V} / \mathrm{mV}$ | Min. |
| Output Voltage Swing | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega$ | $\pm 12$ | $\pm 12$ | V | Min. |
| Input Voltage Range | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ | $\pm 11.5$ | $\pm 11.5$ | V | Min. |
| Common Mode Rejection Ratio |  | 80 | 70 | dB | Min. |
| Supply Voltage Rejection Ratio |  | 70 | 65 | dB | Min. |

## NOTES:

1. The maximum junction temperature of the LM118 is $+150^{\circ} \mathrm{C}, \mathrm{LM} 218$ is $+100^{\circ} \mathrm{C}$ and $+85^{\circ} \mathrm{C}$ for the LM318. For operating at elevated temperatures, devices in the TO-5 package must be derated based on a thermal resistance of $150^{\circ} \mathrm{C} / \mathrm{W}$, junction to ambient, or $45^{\circ} \mathrm{C} / \mathrm{W}$, junction to case.
2. The inputs are shunted with shunt diodes for overvoltage protection. Therefore, excessive current will flow if a differential input voltage in excess of 1 V is applied between the inputs unless some limiting resistance is used.
3. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
4. These specifications apply for $\pm 5 \mathrm{~V} \leqslant V_{S} \leqslant \pm 20 \mathrm{~V}$ and $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for the LM118; $\pm 5 \mathrm{~V} \leqslant V_{S} \leqslant \pm 20 \mathrm{~V}$ and $-20^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$ for the LM $218 ; \pm 5 \mathrm{~V} \leqslant \mathrm{~V}_{S} \leqslant \pm 20 \mathrm{~V}$ and $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+70^{\circ} \mathrm{C}$ for the LM318. Also, power supplies must be bypassed with $0.1 \mu \mathrm{~F}$ ceramic disc capacitors.

## TYPICAL APPLICATIONS

| Offset Balancing | Fast Voltage Follower $\quad$Compensation for Minimum <br> Setting${ }^{\text {Time }}$ | Fast Sample and Hold | Feedforward Compensation for Greater Inverting Slew Rate ${ }^{+}$ |
| :---: | :---: | :---: | :---: |
|  |  |  |  |

## GENERAL DESCRIPTION

Each of the devices in this series consists of four independent, high-gain, operational amplifiers that are designed for singlesupply operation. Operation from split power supplies is also possible and the low power supply drain is independent of the magnitude of the power supply voltage.
Used with a dual supply, the circuit will operate over a wide range of supply voltages. However, a large amount of crossover distortion may occur with loads to ground. An external cur-rent-sinking resistor to $-\mathrm{V}_{\mathrm{CC}}$ will reduce crossover distortion. There is no crossover distortion problem in single supply operation if the load is direct-coupled to ground.

## DESIGN FEATURES

- Large DC Voltage Gain 100 dB
- Compatible with All Forms of Logic
- Temperature Compensated
- Wide Bandwidth at Unity Gain Frequency 1 MHz
- Large Output Voltage Swing: $0 V_{D C}$ to $\mathrm{V}^{+}-1.5 \mathrm{~V}_{\mathrm{DC}}$
- Input Common Mode Voltage Range Includes Ground

SCHEMATIC DIAGRAM


CONNECTION INFORMATION


Supply Voltage, $\mathrm{V}^{+}$
Differential Input Voltage Input Voltage
Power Dissipation (Note 1) Molded DIP Cavity DIP
Flat Pack
Output Short-Circuit to GND (One Amplifier) (Note 2)
$V^{+} \leqslant 15 V_{D C}$ and $T_{A}=25^{\circ} \mathrm{C}$

LM124/LM224/LM324 LM124A/LM224A/LM324A
$32 V_{D C}$ or $16 V_{D C}$ $32 V_{D C}$
$-0.3 V_{D C}$ to $+32 V_{D C}$

## 570 mW

900 mW
800 mW
Continuous

## LM2902

$26 V_{D C}$ or $\pm 13 V_{D C}$ $26 V_{D C}$
$-0.3 V_{D C}$ to $+32 V_{D C}$
570 mW

Continuous

Input Current $\left(\mathrm{V}_{\text {IN }}<-0.3 \mathrm{~V}_{\mathrm{OL}}\right)$ (Note 3) Operating Temperature Range
LM324/LM324A
LM224/LM224A
LM124/LM124A
Storage Temperature Range
Lead Temperature (Soldering, 10 seconds)

LM124/LM224/LM324 LM124A/LM224A/LM324A

## 50 mA

$0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
$-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
$-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
$-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
$300^{\circ} \mathrm{C}$
$-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
$-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ $300^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS $\left(\mathrm{V}^{+}=+5.0 \mathrm{~V}_{\mathrm{DC}}\right.$, Note 4$)$

| PARAMETER | CONDITIONS | LM124A |  |  | LM224A |  |  | LM324A |  |  | LM124/LM224 |  |  | LM324 |  |  | LM2902 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, (Note 5) |  | 1 | 2 |  | 1 | 3 |  | 2 | 3 |  | $\therefore 2$ | $\pm 5$ |  | $\pm 2$ | : 7 |  | $\therefore 2$ | $\pm 7$ | $m V_{\text {DC }}$ |
| Input Bias Current (Note 6) | $\operatorname{IIN(+)}$ or $\operatorname{IIN}(-), \mathrm{T}_{A}=25^{\circ} \mathrm{C}$ |  | 20 | 50 |  | 40 | 80 |  | 45 | 100 |  | 45 | 150 |  | 45 | 250 |  | 45 | 250 | $n{ }^{\text {D }}$ C |
| Input Offset Current | $\mathrm{I}^{\prime} \mathrm{N}(+)-{ }^{1} \mathrm{IN}(-), \mathrm{T}_{A}=25^{\circ} \mathrm{C}$ |  | 2 | 10 |  | 2 | 15 |  | 5 | 30 |  | $\pm 3$ | +30 |  | - 5 | $\pm 50$ |  | $\pm 5$ | $\pm 50$ | ${ }^{n A} D^{\prime}$ |
| Input Common-Mode Voltage Range (Note 7) | $\mathrm{V}^{+}=30 \mathrm{VDC}, \mathrm{T}_{A}=25^{\circ} \mathrm{C}$ | 0 |  | $\mathrm{v}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | 0 |  | $\mathrm{v}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | $V_{D C}$ |
| Supply Current | $\begin{aligned} & R_{L}=\infty, V_{C C}=30 \mathrm{~V},\left(\mathrm{LM} 2902 \mathrm{~V}_{C C}=26 \mathrm{~V}\right) \\ & R_{\mathrm{L}}=\infty \text { On All Op Amps } \end{aligned}$ <br> Over Full Temperature Range $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | $\begin{aligned} & 1.5 \\ & 0.7 \end{aligned}$ | $\begin{gathered} 3 \\ 1.2 \end{gathered}$ |  | $\begin{aligned} & 1.5 \\ & 0.7 \end{aligned}$ | $\begin{gathered} 3 \\ 1.2 \end{gathered}$ |  | $\begin{aligned} & 1.5 \\ & 0.7 \end{aligned}$ | $\begin{gathered} 3 \\ 1.2 \end{gathered}$ |  | $\begin{aligned} & 1.5 \\ & 0.7 \end{aligned}$ | $\begin{gathered} 3 \\ 1.2 \end{gathered}$ |  | $\begin{aligned} & 1.5 \\ & 0.7 \end{aligned}$ | $\begin{gathered} 3 \\ 1.2 \end{gathered}$ |  | $\begin{aligned} & 1.5 \\ & 0.7 \end{aligned}$ | $\begin{gathered} 3 \\ 1.2 \\ 3 \end{gathered}$ | $m^{m} D_{C}$ <br> mADC <br> mADC |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{V}^{+}=15 \mathrm{~V}_{\mathrm{DC}} \text { (F.or Large } \mathrm{V}_{\mathrm{O}} \text { Swing) } \\ & \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{aligned}$ | 50 | 100 |  | 50 | 100 |  | 25 | 100 |  | 50 | 100 |  | 25 | 100 |  |  | 100 |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | $R_{L}=2 \mathrm{k} \Omega, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\left(\mathrm{LM} 2902 \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega\right)$ |  |  |  |  |  |  |  |  |  | 0 |  | $v^{+}-1.5$ | 0 |  | $\mathrm{v}^{+}-1.5$ | 0 |  | $\mathrm{v}^{+}-1.5$ | $\vee_{\text {DC }}$ |
| Common-Mode Rejection Ratio | DC, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 70 | 85 |  | 70 | 85 |  | 65 | 85 |  | 70 | 85 |  | 65 | 70 |  | 50 | 70 |  | dB |
| Power Supply Rejection Ratio | DC, $T_{A}=25^{\circ} \mathrm{C}$ | 65 | 100 |  | 65 | 100 |  | 65 | 100 |  | 65 | 100 |  | 65 | 100 |  | 50 | 100 |  | dB |
| Amplifier-to-Amplifier Coupling (Note 8) | $\mathrm{f}=1 \mathrm{kHz} \text { to } 20 \mathrm{kHz}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ <br> (Input Referred) |  | -120 |  |  | -120 |  |  | -120 |  |  | -120 |  |  | -120 |  |  | -120 |  | $d^{\text {B }}$ |
| Output Current Source | $\begin{aligned} & V_{I N^{+}}=1 \mathrm{~V}_{D C}, V_{I N^{-}}=0 \mathrm{~V}_{D C} . \\ & \mathrm{V}^{+}=15 \mathrm{~V}_{\mathrm{DC}}, \mathrm{~T}_{A}=25^{\circ} \mathrm{C} \end{aligned}$ | 20 | 40 |  | 20 | 40 |  | 20 | 40 |  | 20 | 40 |  | 20 | 40 |  | 20 | 40 |  | mADC |
| Output Current Sink | $\begin{aligned} & V_{I N}=1 \mathrm{~V}_{\mathrm{DC}}, \mathrm{~V}_{\mathrm{IN}^{+}}=0 \mathrm{~V}_{\mathrm{DC}} . \\ & \mathrm{V}^{+}=15 \mathrm{VDC}, \mathrm{~T}_{A}=25^{\circ} \mathrm{C} \end{aligned}$ | 10 | 20 |  | 10 | 20 |  | 10 | 20 |  | 10 | 20 |  | 10 | 20 |  | 10 | 20 |  | ${ }^{m A D C}$ |
|  | $\begin{aligned} & V_{I N^{-}}=1 V_{D C}, V_{I N^{+}}=0 V_{D C} \\ & T_{A}=25^{\circ} \mathrm{C}, V_{O}=200 m V_{D C} \end{aligned}$ | 12 | 50 |  | 12 | 50 |  | 12 | 50 |  | 12 | 50 |  | 12 | 50 |  |  |  |  | ${ }^{\mu A} \mathrm{DC}$ |
| Short Circuit to Ground | $\mathrm{T}_{A}=25^{\circ} \mathrm{C}$, (Note 2) |  | 40 | 60 |  | 40 | 60 |  | 40 | 60 |  | 40 | 60 |  | 40 | 60 |  | 40 | 60 | mADC |

## ELECTRICAL CHARACTERISTICS（CONT）

| PARAMETER | CONDITIONS | LM124A |  |  | LM224A |  |  | LM324A |  |  | LM124／LM224 |  |  | LM324 |  |  | LM2902 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | （Note 5） |  |  | 4 |  |  | 4 |  |  | 5 |  |  | $\pm 7$ |  |  | $\pm 9$ |  |  | $\pm 10$ | mV DC |
| Input Offset Voltage Drift | $\mathrm{R}_{\mathrm{S}}=0 \Omega$ |  | 7 | 20 |  | 7 | 20 |  | 7 | 30 |  | 7 |  |  | 7 |  |  | 7 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Offset Current | $\operatorname{lin}(+)-\operatorname{Iin}(-)$ |  |  | 30 |  |  | 30 |  |  | 75 |  |  | $\pm 100$ |  |  | $\pm 150$ |  | 45 | $\pm 200$ | $n A_{\text {D }}$ |
| Input Offset Current Drift |  |  | 10 | 200 |  | 10 | 200 |  | 10 | 300 |  | 10 |  |  | 10 |  |  | 10 |  | $\mathrm{pA}_{\text {DC }}{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | $\operatorname{liN(+)}$ or I，N（－） |  | 40 | 100 |  | 40 | 100 |  | 40 | 200 |  | 40 | 300 |  | 40 | 500 |  | 40 | 500 | nA ${ }^{\text {dC }}$ |
| Input Common－Mode Voltage Range（Note 7） | $\mathrm{V}^{+}=30 \mathrm{VDC}$ | 0 |  | $\mathrm{V}^{+}-2$ | 0 |  | $\mathrm{V}^{+}-2$ | 0 |  | $\mathrm{V}^{+}-2$ | 0 |  | $\mathrm{v}^{+}-2$ | 0 |  | $\mathrm{v}^{+}-2$ | 0 |  | $\mathrm{v}^{+}-2$ | $V_{D C}$ |
| Large Signal Voltage Gain | $\mathrm{V}^{+}=+15 \mathrm{~V}_{\mathrm{DC}}$（For Large $\mathrm{V}_{\mathrm{O}}$ Swing） $R_{L} \geqslant 2 \mathrm{k} \Omega$ | 25 |  |  | 25 |  |  | 15 |  |  | 25 |  |  | 15 |  |  | 15 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing $\mathrm{VOH}_{\mathrm{OH}}$ $\mathrm{v}_{\mathrm{OL}}$ | $\begin{aligned} & \mathrm{V}^{+}=+30 \mathrm{~V}_{\mathrm{DC}}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \\ & \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega \\ & \mathrm{~V}^{+}=5 \mathrm{~V}_{\mathrm{D}}, \mathrm{R}_{\mathrm{L}} \leqslant 10 \mathrm{ks} 2 \end{aligned}$ | $\begin{aligned} & 26 \\ & 27 \end{aligned}$ | $\begin{gathered} 28 \\ 5 \end{gathered}$ | 20 | $\begin{aligned} & 26 \\ & 27 \end{aligned}$ | $\begin{gathered} 28 \\ 5 \end{gathered}$ | 20 | $\begin{aligned} & 26 \\ & 27 \end{aligned}$ | $\begin{gathered} 28 \\ 5 \end{gathered}$ | 20 | $\begin{aligned} & 26 \\ & 27 \end{aligned}$ | $\begin{gathered} 28 \\ 5 \end{gathered}$ | 20 | $\begin{aligned} & 26 \\ & 27 \end{aligned}$ | $\begin{gathered} 28 \\ 5 \end{gathered}$ | 20 | $\begin{aligned} & 22 \\ & 23 \end{aligned}$ | $\begin{gathered} 24 \\ 5 \end{gathered}$ | 100 | $V_{D C}$ <br> $V_{D C}$ <br> $m V_{D C}$ |
| Output Current Source Sink | $\begin{aligned} & V_{I N^{+}}=+1 \mathrm{~V}_{\mathrm{DC}}, V_{I N^{-}}=0 \mathrm{~V}_{\mathrm{DC}}, \mathrm{~V}^{+}=15 \mathrm{~V}_{\mathrm{DC}} \\ & \mathrm{VIN}^{-}=+1 \\ & \mathrm{VDC}, \mathrm{~V}_{1 \mathrm{~N}^{+}}=0 \mathrm{~V}_{\mathrm{DC}}, \mathrm{~V}^{+}=15 \mathrm{~V}_{\mathrm{DC}} \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & 15 \\ & \hline \end{aligned}$ |  | $\begin{gathered} 10 \\ 5 \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ 8 \\ \hline \end{gathered}$ |  | $\begin{gathered} 10 \\ 5 \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ 8 \\ \hline \end{gathered}$ |  | $\begin{gathered} 10 \\ 5 \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ 8 \\ \hline \end{gathered}$ |  | $\begin{gathered} 10 \\ 5 \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ 8 \\ \hline \end{gathered}$ |  | $\begin{gathered} 10 \\ 5 \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ 8 \\ \hline \end{gathered}$ |  | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \\ & \hline \end{aligned}$ |
| Differential Input Voltage | （Note 7） |  |  |  |  |  | $\mathrm{v}^{+}$ |  |  | $\mathrm{v}^{+}$ |  |  | $\mathrm{v}^{+}$ |  |  | $\mathrm{v}^{+}$ |  |  | $\mathrm{v}^{+}$ | $V_{D C}$ |

## NOTES：

 board，operating in a still air ambient．The LM224／LM224A and LM124／LM124A can be derated based on a $+150^{\circ} \mathrm{C}$ maximum junction temperature．The dissipation is the total of all four amplifiers－use external resistors，where possible，to allow the amplifier to saturate or to reduce the power which is dissipated in the integrated circuit
 continuous short－circuits can exceed the power dissipation ratings and cause eventual destruction．Destructive dissipation can result from simultaneous shorts on all amplifiers．


4．These specifications apply for $V^{+}=+5 \mathrm{VDC}$ and $-55^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+125^{\circ} \mathrm{C}$ ，unless otherwise stated．With the LM224／LM224A，all temperature specifications are limited to $-25^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+85^{\circ} \mathrm{C}$ ，the $\mathrm{LM} 324 / \mathrm{C}$ cations are limited to $0^{\circ} \mathrm{C} \leqslant T_{A} \leqslant-70^{\circ} \mathrm{C}$ ，and the LM2902 specifications are limited to $-40^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+85^{\circ} \mathrm{C}$ ．
5．$V_{O} 1.4 \vee_{D C}$ ． $\mathrm{RS}_{\mathrm{S}}=0 \Omega 2$ with $\mathrm{V}^{+}$from $5 \mathrm{~V}_{\mathrm{DC}}$ to $30 \mathrm{~V}_{\mathrm{DC}}$ ；and over the full common－mode range（ $0 \mathrm{~V}_{\mathrm{DC}}$ to $\mathrm{V}^{+}-1.5 \mathrm{~V}_{\mathrm{DC}}$ ）
6．The direction of the input current is out of the IC due to the PNP input stage．This current is essentially constant，independent of the state of the output so no loading change exists on the input lines
 without damage（ +26 V $_{\text {DC }}$ for LMz＇902）．
8．Due to proximity of external components，insure that coupling is not originating via stray capacitance between these external parts．This typically can be detected as this type of capacitive increases at higher frequencies．

## Quad Single-Supply

 Operational Amplifiers
## TYPICAL PERFORMANCE CHARACTERISTICS



## DESCRIPTION

The LM148 series is a true quad 741 . It consists of four independent, high gain, internally compensated, low power operational amplifiers which have been designed to provide functional characteristics identical to those of the familiar 741 operational amplifier. In addition, the total supply current for all four amplifiers is comparable to the supply current of a single 741 type op amp. Other features include input offset currents and input bias current which are much less than those of a standard 741. Also, excellent isolation between amplifiers has been achieved by independently biasing each amplifier and using layout techniques which minimize thermal coupling. The LM149 series has the same features as the LM148 plus a gain bandwidth product of 4 MHz at a gain of 5 or greater.
The LM148 can be used anywhere multiple 741 or 1558
type amplifiers are being used and in applications where amplifier matching or high packing density is required.

## FEATURES

- 741 op amp operating characteristics
- Low supply current drain ( $0.6 \mathrm{~mA} /$ Amplifier)
- Class $A B$ output stage - no crossover distortion
- Pin compatible with the LM124
- Low input offset voltage ( 1 mV )
- Low input offset current ( 4 nA )
- Low input bias current ( 30 nA )
- Gain bandwidth product: LM148 (unity gain) ( 1.0 MHz )

$$
\text { LM149 }\left(A_{V} \geqslant 5\right)(4 M H z)
$$

- High degree of isolation between amplifiers ( 120 dB )
- Overload protection for inputs and outputs


## SCHEMATIC DIAGRAM (1/4 Shown)



CONNECTION INFORMATION

| CJ Flatpak (Top View) | DC and DB Dual In-Line Packages (Top View) | $\begin{gathered} \text { PIN } \\ 1 \\ 2 \\ 3 \end{gathered}$ | FUNCTION OUTPUT A$-V_{\text {IN }} A$$+V_{\text {IN }} A$ | HIGH RELIABILITY OPTIONS |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Part Number | Screening |
|  |  |  |  | LM148J03 | MIL-STD-883 Class B |
| $\square$ | [1 ${ }^{16}$ | $\begin{aligned} & 4 \\ & 5 \end{aligned}$ | $\begin{aligned} & V+ \\ & +V_{\text {IN }} B \end{aligned}$ | LM248J03** | Raytheon $\mathrm{A}+3$ screening including |
|  | $2{ }^{2}$ 全 413 | 6 | $\begin{aligned} & +V_{I N} \\ & \text {-VIN } \end{aligned}$ | LM348J03 | Burn-in and tightened AOL |
| 二ers | $3{ }^{3}$ | 7 | OUTPUT B | LM248N02* ${ }^{\text {a }}$ | Raytheon $A+2$ screening including |
| $\square \square^{6}$ | [4. 11 | 8 | OUTPUT C | LM348N02 | temp cycles, Burn-in, "Hot Rail" |
| Order Part Nos. | [5] | 10 | -VIN $+V_{\text {IN }}$ |  | testing and tightened AOL |
| LM148F, LM149F, |  | 11 | $\mathrm{V}_{-} \mathrm{VIN}^{\text {d }}$ | LM248N01* ${ }^{\text {LM348N01 }}$ \} | Raytheon $\mathrm{A}+1$ screening including |
| LM148J, LM248J, LM348J, LM248N, LM348N | 8 | 12 | $+V_{\text {IN }} D$ $-V_{\text {IN }} D$ | LM348N01 | temp cycles, "Hot Rail" testing and tightened AOL |
| LM149J, LM249J, LM349J, LM149N, LM349N |  | 14 | OUTPUT D | *Complete d section of th | ails are shown in the quality catalog. |

## ABSOLUTE MAXIMUM RATINGS

LM148/LM149
Supply Voltage
Differential Input Voltage
Input Voltage
Output Short Circuit Duration (Note 1)
Power Dissipation ( $\mathrm{P}_{\mathrm{d}}$ at $25^{\circ} \mathrm{C}$ ) and
Thermal Resistance ( $\theta_{\mathrm{j}} \mathrm{A}$ ) (Note 2)

| Molded DIP (N) | $\mathrm{P}_{\mathrm{d}}$ |
| :--- | :--- |
|  | $\theta_{\mathrm{j} A}$ |
| Cavity DIP (D) (J) | $\mathrm{P}_{\mathrm{d}}$ |
|  | $\theta_{\mathrm{jA}}$ |
| Flat Pack (CJ) | $\mathrm{P}_{\mathrm{d}}$ |
|  | $\theta_{\mathrm{jA}}$ |

Maximum Junction Temperature ( $\mathrm{T}_{\mathrm{j} M A X}$ )
Operating Temperature Range
Storage Temperature Range
Lead Temperature (Soldering 60 seconds)

| $\pm 22 \mathrm{~V}$ |
| :--- |
| $\pm 44 \mathrm{~V}$ |
| $\pm 22 \mathrm{~V}$ |
| Continuous |
|  |
|  |
| - |
|  |
|  |
| 900 mW |
| $100^{\circ} \mathrm{C} / \mathrm{W}$ |
| 675 mW |
| $185^{\circ} \mathrm{C} / \mathrm{W}$ |
| $150^{\circ} \mathrm{C}$ |
| $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ |
| $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| $300^{\circ} \mathrm{C}$ |

LM248/LM249

Continuous

|  | - | 500 mW |
| ---: | :--- | :--- |
|  | - | $150^{\circ} \mathrm{C} / \mathrm{W}$ |
| 900 mW |  | 900 mW |
| $100^{\circ} \mathrm{C} / \mathrm{W}$ |  | $100^{\circ} \mathrm{C} / \mathrm{W}$ |

$110^{\circ} \mathrm{C}$
$-25^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$
$-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
$300^{\circ} \mathrm{C}$

LM348/LM349
$\pm 18 \mathrm{~V}$
$\pm 36 \mathrm{~V}$
$\pm 18 \mathrm{~V}$
Continuous

ELECTRICAL CHARACTERISTICS
(See Note 3)


Note 1: Any of the amplifier outputs can be shorted to ground indefinitely; however, more than one should not be simultaneously shorted as the maximum junction temperature will be exceeded.
Note 2: The maximum power dissipation for these devices must be derated at elevated temperatures and is dictated by $T_{j M A X}, \theta_{j A}$, and the ambient temperature, $T_{A}$. The maximum available power dissipation at any temperature is $P_{d}=\left(T_{j M A X}-T_{A}\right) / \theta_{j A}$ or the $25^{\circ} \mathrm{C} P_{d M A X}$, whichever is less.

Note 3: These specifications apply for $V_{S}= \pm 15 \mathrm{~V}$ and over the absolute maximum operating temperature range ( $T_{L} \leqslant T_{A} \leqslant T_{H}$ ) unless otherwise noted.

## APPLICATION GUIDES

The 148 series are low power quad operational amplifiers that exhibit performance comparable to the popular 741. Substitution can therefore be made with no change in circuit behavior.

The 149 series is similar to the 148 except it is decompensated to yield a wider gain-bandwidth product. Consequently, it must be operated at a minimum closed loop gain of 5 .

The input characteristics of these devices allow differential voltages which exceed the supplies. Output phase will be correct as long as one of the inputs are within the operating common mode range. If both exceed the negative limit, the output will latch positive. Current limiting resistors should be used on the inputs in case voltages become excessive.

When capacitive loading becomes much greater than 100 pf, a resistor should be placed between the output and feedback connection in order to reduce phase shift.

The $148 / 149$ series is short circuit protected to either ground or the supplies continuously when only one of the four amplifiers are shorted. If multiple shorts occur simultaneously, the unit can be destroyed due to excessive power dissipation.
To assure stability, feedback resistors should be placed close to the input to maximize the feedback pole frequency (function of input to ground capacitance) and to minimize pickup. A good rule of thumb is that the feedback pole frequency should be 6 times the operating 3 dB frequency. If less, a lead capacitor should be placed between the output and input.

## TYPICAL APPLICATIONS

TYPICAL PERFORMANCE DATA


## TYPICAL PERFORMANCE DATA (CONT)



Inverting Large Signal Pulse
Response (LM148)


Large Signal Pulse
Response (LM149)


Slew Rate vs
Temperature


Input Noise Voltage and Noise Current


Inverting Large Signal Pulse
Response (LM149)


Bode Plot LM149


Negative Common-Mode Input Voltage Limit


Positive Common-Mode Input Voltage Limit


Small Signal Pulse
Response (LM149)

## Low Power Quad 741 <br> Operational Amplifiers

TYPICAL APPLICATIONS-LM148

Low Drift Peak Detector with Bias Current Compensation


Universal State-Space Filter


Use Band Pass output to tune for $Q$
$\frac{V(s)}{V_{I N(s)}}=\frac{N(s)}{D(s)}, D(s)=s^{2}+\frac{S \omega_{0}}{Q}+\omega_{0}{ }^{2}$
$N_{H P(s)}=s^{2} H_{O H P}, N_{B P}(s)=\frac{-S \omega_{O} H_{O B P}}{Q} \quad N_{L P}=\omega_{o}{ }^{2} H_{O L P}$
$f_{o}=\frac{1}{2 \pi} \sqrt{\frac{R 6}{R 5}} \sqrt{\frac{1}{t 1 t 2}}, t_{i}=R_{i} C_{i}, Q=\left(\frac{1+R 4|R 3+R 4| R 0}{1+R 6 \mid R 5}\right) \quad\left(\frac{R 6}{R 5} \frac{t_{1}}{t_{2}}\right) \quad 1 / 2$
$f_{N O T C H}=\frac{1}{2 \pi}\left(\frac{R_{H}}{R_{L} t_{1} t_{2}}\right)^{1 / 2}, H_{O H P}=\frac{1+R 6 \mid R 5}{1+R 3|R 0+R 3| R 4}, H_{O B P}=\frac{1+R 4|R 3+R 4| R 0}{1+R 3|R 0+R 3| R 4}$
$H_{O L P}=\frac{1+R 5 I R 6}{1+R 3 I R O+R 3 I R 4}$

## TYPICAL APPLICATIONS LM148 (CONT)



Use general equations, and tune each section separately
$\mathrm{Q}_{1 \text { st }}$ SECTION $=0.541, \mathrm{Q}_{2 \text { ndSECTION }}=1.306$
The response should have $0 d B$ peaking

## A 3 Amplifier Bi-Quad Notch Filter


$Q=\sqrt{\frac{R 8}{R 7}} \times \frac{R 1 C 1}{\sqrt{R 3 C 2 R 2 C 1}}, f_{0}=\frac{1}{2 \pi} \sqrt{\frac{R 8}{R 7}} \times \frac{1}{\sqrt{R 2 R 3 C 1 C 2}}, f_{N O T C H}=\frac{1}{2 \pi} \sqrt{\frac{R 6}{R 3 R 5 R 7 C 1 C 2}}$
Necessary condition for notch: $\frac{i}{R 6}=\frac{\overline{R i}}{R 4 R 7}$
$E x: f_{N O T C H}=3 \mathrm{kHz}, \mathrm{Q}=5, R 1=270 \mathrm{k}, \mathrm{R} 2=\mathrm{R} 3=20 \mathrm{k}, \mathrm{R} 4=27 \mathrm{k}, \mathrm{R} 5=20 \mathrm{k}, \mathrm{R} 6=\mathrm{R} 8=10 \mathrm{k}, \mathrm{R} 7=100 \mathrm{k}, \mathrm{C} 1=\mathrm{C} 2=0.001 \mu \mathrm{~F}$ Better noise performance than the state-space approach

## Low Power Quad 741 <br> Operational Amplifiers

TYPICAL APPLICATIONS LM148 (CONT)

${ }^{\mathrm{f}} \mathrm{C}=1 \mathrm{kHz}, \mathrm{f} S=2 \mathrm{kHz}, \mathrm{f}_{\mathrm{P}}=0.543, \mathrm{f}_{\mathrm{Z}}=2.14, \mathrm{Q}=0.841, \mathrm{f}^{\prime} \mathrm{P}=0.987, \mathrm{f}^{\prime} \mathrm{Z}=4.92, \mathrm{Q}^{\prime}=4.403$, normalized to ripple BW
$f_{P}=\frac{1}{2 \pi} \sqrt{\frac{R 6}{R 5}} \times \frac{1}{t}, f_{Z}=\frac{1}{2 \pi} \sqrt{\frac{R_{H}}{R_{L}}} \times \frac{1}{t}, Q=\left(\frac{1+R 4|R 3+R 4| R 0}{1+R 6 \mid R 5}\right) \times \sqrt{\frac{R 6}{R 5}}, Q^{\prime}=\sqrt{\frac{R^{\prime} 6}{R^{\prime} 5} \frac{1+R^{\prime} 4 \mid R^{\prime} 0}{1+R^{\prime} 6\left|R^{\prime} 5+R^{\prime} 6\right| R_{P}}}$
$R_{P}=\frac{R_{H} R_{L}}{R_{H}+R_{L}}$
Use the BP outputs to tune $\mathrm{Q}, \mathrm{Q}^{\prime}$, tune the 2 sections separately
$R 1=R 2=92.6 \mathrm{k}, \mathrm{R} 3=R 4=R 5=100 \mathrm{k}, \mathrm{R} 6=10 \mathrm{k}, R 0=107.8 \mathrm{k}, R_{\mathrm{L}}=100 \mathrm{k}, \mathrm{R}_{\mathrm{H}}=155.1 \mathrm{k}$,
$R^{\prime} 1=R^{\prime} 2=50.9 k, R^{\prime} 4=R^{\prime} 5=100 k, R^{\prime} 6=10 k, R^{\prime} 0=5.78 k, R_{L}^{\prime}=100 \mathrm{k}, R^{\prime} H=248.12 k, R^{\prime} f=100 \mathrm{k}$. All capacitors are $0.001 \mu F$.

## TYPICAL APPLICATIONS-LM149




Low Power Quad 741 Operational Amplifiers

## TYPICAL SIMULATION



## GENERAL DESCRIPTION

The LF155A, 156A and 157A family is composed of JFET input operational amplifiers which by using advanced processing techniques, contain both bipolar transistors and closely matched JFET's on the same chip. The resulting amplifiers feature low input offset voltage and offset voltage drift, low input bias and offset current, and low noise. These devices also feature wide bandwidth, high slew rate and fast settling time making them extremely versatile in such applications as $A / D$ and $D / A$ conversion, sample and hold circuits; analog function circuits, active filters and instrumentation circuits.

## DESIGN FEATURES

- Low input offset voltage - 1 mV
- Low input offset current - 3 pA
- Low input bias current - 30 pA
- Low input noise voltage $-12 \mathrm{nV} / \sqrt{\mathrm{Hz}}$ 156A,157A

$$
20 \mathrm{nV} / \sqrt{\mathrm{Hz}} \quad 155 \mathrm{~A}
$$

- Low input noise current $-0.01 \mathrm{pA} \sqrt{\mathrm{Hz}}$
- High DC voltage gain - 200,000 V/V


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



ABSOLUTE MAXIMUM RATINGS

|  | LF155A/6A/7A | LF355A/6A/7A | LF155/6/7 | LF255/6/7 | LF355/6/7 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Supply Voltage | $\pm 22 \mathrm{~V}$ | $\pm 22 \mathrm{~V}$ | $\pm 22 \mathrm{~V}$ | $\pm 22 \mathrm{~V}$ | $\pm 18 \mathrm{~V}$ |
| Power Dissipation (Note 1) T0-99 (H package) | 670 mW | 500 mW | 670 mW | 570 mW | 500 mW |
| Operating Temperature Range | -55 to $+125^{\circ} \mathrm{C}$ | 0 to $+70^{\circ} \mathrm{C}$ | -55 to $+125^{\circ} \mathrm{C}$ | -25 to $+85^{\circ} \mathrm{C}$ | 0 to $+70^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{j}}(\mathrm{MAX})$ | $150^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ | $150^{\circ} \mathrm{C}$ | $110^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 40 \mathrm{~V}$ | $\pm 40 \mathrm{~V}$ | $\pm 40 \mathrm{~V}$ | $\pm 40 \mathrm{~V}$ | $\pm 30 \mathrm{~V}$ |
| Input Voltage Range (Note 2) | $\pm 20 \mathrm{~V}$ | $\pm 20 \mathrm{~V}$ | $\pm 20 \mathrm{~V}$ | $\pm 20 \mathrm{~V}$ | $\pm 16 \mathrm{~V}$ |
| Output Short Circuit Duration | Continuous | Continuous | Continuous | Continuous | Continuous |
| Storage Temperature Range | -65 to $+150^{\circ} \mathrm{C}$ | -65 to $+150^{\circ} \mathrm{C}$ | -65 to $+150^{\circ} \mathrm{C}$ | -65 to $+150^{\circ} \mathrm{C}$ | -65 to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 seconds) | $300^{\circ} \mathrm{C}$ | $300^{\circ} \mathrm{C}$ | $300^{\circ} \mathrm{C}$ | $300^{\circ} \mathrm{C}$ | $300^{\circ} \mathrm{C}$ |

Note: LF157A, 357A, 157, 257, 357 are decompensated for use in circuits with $A V \geqslant 5$ only.
DC ELECTRICAL CHARACTERISTICS $V_{C C} \pm 15 \vee T_{A}+25^{\circ} \mathrm{C}$ unless otherwise specified

| PARAMETER | CONDITIONS | LF155A/156A/157A |  |  | LF355A/356A/357A |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{S} \leqslant 10 \mathrm{~K} \Omega$ |  | 1.0 | 2.0 |  | 1.0 | 2.0 | mV |
| Input Offset Current |  |  | 3 | 10 |  | 3 | 10 | pA |
| Input Bias Current |  |  | 30 | 50 |  | 30 | 50 | pA |
| Input Resistance |  |  | $10^{6}$ |  |  | $10^{6}$ |  | M $\Omega$ |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 50K | 200K |  | 50K | 200K |  | V/V |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for LF155A/156A/157A; $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C}$ for LF355A/356A/357A . |  |  |  |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{R}_{S} \leqslant 10 \mathrm{~K} \Omega$ |  |  | 2.5 |  |  | 2.3 | mV |
| Input Offset Current |  |  |  | 10 |  |  | 1.0 | nA |
| Input Bias Current |  |  |  | 25 |  |  | 5 | nA |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 25K |  |  | 25K |  |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{~K} \Omega$ | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | V |
| Average Offset Voltage Drift |  |  | 3 | 5 |  | 3 | 5 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega \Delta \mathrm{~V} \pm 5 \mathrm{~V}$ | 85 | 100 |  | 85 | 100 |  | dB |
| Power Supply Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega \Delta \mathrm{~V} \pm 5 \mathrm{~V}$ | 85 | 100 |  | 85 | 100 |  | dB |
| Input Voltage Range |  | $\pm 11$ | $\begin{aligned} & \hline+15.1 \\ & -12 \\ & \hline \end{aligned}$ |  | $\pm 11$ | $\begin{aligned} & \hline+15.1 \\ & -12 \\ & \hline \end{aligned}$ |  | V |

AC ELECTRICAL CHARACTERISTICS $V_{C C} \pm 15 V_{A}+25^{\circ} \mathrm{C}$ unless otherwise specified

| PARAMETER | CONDITIONS | LF155A/355A |  |  | LF156A/356A |  |  | LF157A/357A |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Gain Bandwidth Product |  |  | 2.5 |  | 4.0 | 4.5 |  | 15 | 20 |  | M Hz |
| Settling Time | To 0.01\% |  | 4 |  |  | 1.5 |  |  | 1.5 |  | $\mu \mathrm{s}$ |
| Slew Rate | LF155A/156A: $A V=1$ <br> LF157A: AV = 5 | 3 | 5 |  | 10 | 12 |  | 40 | 50 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Input Capacitance |  |  | 3 |  |  | 3 |  |  | 3 |  | pF |
| Input Noise Current | $F=100 \mathrm{~Hz}$ |  | 0.01 |  |  | 0.01 |  |  | 0.01 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
|  | $\mathrm{F}=1 \mathrm{kHz}$ |  | 0.01 |  |  | 0.01 |  |  | 0.01 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
| Input Noise Voltage ( $\mathrm{R}_{\mathrm{S}}=100 \Omega$ ) | $\mathrm{F}=100 \mathrm{~Hz}$ |  | 25 |  |  | 15 |  |  | 15 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
|  | $\mathrm{F}=1 \mathrm{kHz}$ |  | 20 |  |  | 12 |  |  | 12 |  | $n \mathrm{~V} / \sqrt{\mathrm{Hz}}$ |

DC ELECTRICAL CHARACTERISTICS $V_{S}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

| PARAMETER | LF155A/355A LF155/255 |  | LF355 |  | LF156A/356A LF156/256 |  | LF356 |  | LF157A/357A LF157/257 |  | LF357 |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | TYP | MAX | TYP | MAX | TYP | MAX | TYP | MAX | TYP. | MAX | TYP | MAX |  |
| Supply Current | 2 | 4 | 2 | 4 | 5 | 7 | 5 | 10 | 5 | 7 | 5 | 10 | mA |

DC ELECTRICAL CHARACTERISTICS $V_{C C} \pm 15 \mathrm{~V} \mathrm{~T}_{\mathrm{A}}+25^{\circ} \mathrm{C}$ unless otherwise specified

| PARAMETER | -CONDITIONS | LF155/156/157 |  |  | LF255/256/257 |  |  | LF355/356/357 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{S} \leqslant 10 \mathrm{~K} \Omega$ |  | 3 | 5 |  | 3 | 5 |  | 3 | 10 | mV |
| Input Offset Current |  |  | 3 | 20 |  | 3 | 20 |  | 3 | 50 | pA |
| Input Bias Current |  |  | 30 | 100 |  | 30 | 100 |  | 30 | 200 | pA |
| Input Resistance |  |  | $10^{6}$ |  |  | $10^{6}$ |  |  | $10^{6}$ |  | $\mathrm{M} \Omega$ |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 50 K | 200K |  | 50K | 200 K |  | 25K | 200K |  | V/V |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for LF155/156/157; $-25^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$ for LF255/256/257; $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}}$ $\leqslant+70^{\circ} \mathrm{C}$ for LF355/356/357. |  |  |  |  |  |  |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{RS}_{S} \leqslant 10 \mathrm{~K} \Omega$ |  |  | 7 |  |  | 6.5 |  |  | 13 | mV |
| Input Offset Current |  |  |  | 20 |  |  | 1 |  |  | 2 | nA |
| Input Bias Current |  |  |  | 50 |  |  | 5 |  |  | 8 | nA |
| ' arge Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 25K |  |  | 25K |  |  | 15K |  |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{~K} \Omega$ | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | V |
| Average Offset Voltage Drift |  |  | 5 |  |  | 5 |  |  | 5 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Common Mode Rejection Ratio | $\mathrm{R}_{S} \leqslant 10 \mathrm{~K} \Omega \Delta \mathrm{~V} \pm 5 \mathrm{~V}$ | 85 | 100 |  | 85 | 100 |  | 80 | 100 |  | dB |
| Power Supply Rejection Ratio | $\mathrm{R}_{S} \leqslant 10 \mathrm{~K} \Omega \Delta \mathrm{~V} \pm 5 \mathrm{~V}$ | 85 | 100 |  | 85 | 100 |  | 80 | 100 |  | dB |
| Input Voltage Range |  | $\pm 11$ | $\begin{array}{\|l\|} \hline+15.1 \\ -12 \\ \hline \end{array}$ |  | $\pm 11$ | $\begin{aligned} & +15.1 \\ & -12 \\ & \hline \end{aligned}$ |  | $\pm 11$ | $\begin{aligned} & +15.1 \\ & -12 \\ & \hline \end{aligned}$ |  | V |

AC ELECTRICAL CHARACTERISTICS $V_{C C} \pm 15 \vee T_{A}+25^{\circ} \mathrm{C}$ unless otherwise specified

| PARAMETER | CONDITIONS | LF155/255/355 TYP | LF156/256 MIN | LF156/256/356 TYP | LF157/257 <br> MIN | LF157/257/357 TYP | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Gain Bandwidth Product |  | 2.5 |  | 5.0 |  | 20 | MHz |
| Settling Time | To 0.01\% | 4 |  | 1.5 |  | 1.5 | $\mu \mathrm{s}$ |
| Slew Rate | LF155/156: AV=1 LF157: AV=5 | 5 | 7.5 | 12 | 30 | 50 | $\mathrm{V} / \mu \mathrm{s}$ |
| Input Capacitance |  | 3 |  | 3 |  | 3 | pF |
| Input Noise Current | $\mathrm{F}=100 \mathrm{~Hz}$ | 0.01 |  | 0.01 |  | 0.01 | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
|  | $\mathrm{F}=1 \mathrm{kHz}$ | 0.01 |  | 0.01 |  | 0.01 |  |
| Input Noise Voltage ( $R_{S}=100 \Omega$ ) | $F=1.00 \mathrm{~Hz}$ | 25 |  | 15 |  | 15 | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
|  | $\mathrm{F}=1 \mathrm{kHz}$ | 20 |  | 12 |  | 12 |  |

Note 1: The TO-99 package must be derated based on a thermal resistance of $150^{\circ} \mathrm{C} / \mathrm{W}$ junction to ambient or $45^{\circ} \mathrm{C} / \mathrm{W}$ junction to case. Note 2: Unless otherwise specified the absolute maximum negative input voltage is equal to the negative power supply voltage.
Note 3: These specifications apply for $\pm 15 \mathrm{~V} \leqslant V_{S} \leqslant \pm 20 \mathrm{~V},-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ and $\mathrm{T}_{H I G H}=-125^{\circ} \mathrm{C}$ unless otherwise stated for the LF155A/6A/7A and the LF155/6/7. For LF255/6/7, these specifications apply for $\pm 15 \mathrm{~V} \leqslant \mathrm{~V}_{S} \leqslant \pm 20 \mathrm{~V},-25^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}}+85^{\circ} \mathrm{C}$ and $\mathrm{T}_{\mathrm{H}}$ GH $=+85^{\circ} \mathrm{C}$ unless otherwise stated. For LF355A/6A/7A, these specifications apply for $\pm 15 \mathrm{~V} \leqslant \mathrm{VS}_{\mathrm{S}} \leqslant \pm 20 \mathrm{~V}, 0^{\circ} \mathrm{C} \leqslant \mathrm{TA} \leqslant+70^{\circ} \mathrm{C}$ and $\mathrm{TH} \mathrm{H} G \mathrm{H}$ $=+70^{\circ} \mathrm{C}$, and for the LF355/6/7 these specifications apply for $V_{S}= \pm 15 \mathrm{~V}$ and $0^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+70^{\circ} \mathrm{C} . V_{O S}$, $I_{B}$ and IOS are measured at $V C M=0$. Note 4: The Temperature Coefficient of the adjusted input offset voltage changes only a small amount ( $0.5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ typically) for each mV of adjustment from its original unadjusted value. Common mode rejection and open loop voltage gain are also unaffected by offset adjustment. Note 5: The input bias currents are junction leakage currents which approximately double for every $10^{\circ} \mathrm{C}$ increase in the junction temperature, $\mathrm{T}_{\mathrm{J}}$. Due to limited production test time, the input bias currents measured are correlated to junction temperature. In normat operation the junction temperature rises above the ambient temperature as a result of internal power dissipation, $\mathrm{P}_{\mathrm{d}} . \mathrm{T}_{\mathrm{j}}=\mathrm{T}_{\mathrm{A}}+\mathrm{O}_{\mathrm{j}} \mathrm{A} \mathrm{Pd}_{\mathrm{d}} \mathrm{where} \mathrm{O}_{\mathrm{j}} \mathrm{A}$ is the thermal resistance from junction to ambient. Use of a heat sink is recommended if input bias current is to be kept to a minimum.
Note 6: Supply Voltage Rejection is measured for both supply magnitudes increasing or decreasing simultaneously, in accordance with common practice.
Note 7: Setting time is defined here, for a unity gain inverter connection using $2 \mathrm{k} \Omega$ resistors for the LF115/6. It is the time required for the error voltage (the voltage at the inverting input pin on the amplifier) to settle to within $0.01 \%$ of its final value from the time a 10 V step input is applied to the inverter. For the LF157, AV $=-5$, the feedback resistor from output to input is $2 \mathrm{k} \Omega$ and the output step is 10 V (see Setting Time Test Circuit).

## TYPICAL AC PERFORMANCE CHARACTERISTICS



## 155/155A 156/156A 157/157A

## TYPICAL AC PERFORMANCE CHARACTERISTICS (CONT)



TYPICAL DC PERFORMANCE CHARACTERISTICS


## INPUT PROTECTION

This family of op amps has an ion-implanted, P -ChannelJFET input stage. The reverse breakdown voltages are large; therefore there is no need for protective diode-clamps across the inputs. Also, large differential-input voltages can be accommodated without causing large increases in inputbias current. The maximum differential-input-voltage is independent of the supply voltages. These amplifiers have JFET inputs rather than MOSFET inputs, so special hand-
ling is not needed. The only word of caution: Do not let either input voltage exceed the negative supply voltage. If either input becomes more negative than the negative supply voltage, then excessive currents may flow through the input stage and destroy the unit.

## INPUT COMMON-MODE RANGE

An unusual feature of these amplifiers is that the common-mode-input-voltage range for linear operation extends to
the positive supply voltage. The common-mode input voltage can even exceed the positive supply voltage by approximately 100 mV . This ability to operate with common-mode voltages of up to, and slightly over, the positive supply voltage holds over the full power-supply range and rated operating temperature range. This capability is very useful in comparator applications where the positive supply voltage can be used as a reference voltage on one of the inputs.

On the negative side, the specified range must be adhered to for proper operation. Exceeding the negative common-mode limit on either input will cause a reversal of phase at the output and will force the amplifier output to the corresponding high or low state (positive or negative saturation). Exceeding the negative common-mode voltage limit on both inputs forces the amplifier output into positive saturation. The amplifier will not "latch" or become damaged by exceeding the negative common-mode limits as long as the peak input current is limited to 30 mA . But there is reversal of phase and this should be carefully considered in designing oscillator circuits, comparators, etc. where commonmode limits might be exceeded.

## BROADBANDING

The LF157 family is decompensated to obtain very high slew-rate and gain-bandwidth product. This sacrifices phasemargin and thereby limits the usage to selected applications, but the performance improvement in those particular applications is often substantial. External compensation can be used to optimize overall performance.

The LF157 series is a LF156 circuit decompensated by a factor of 5 , and is therefore 5 times faster than the LF.156. But to obtain the same degree of stability, the LF157 op amp must be operated at a minimum closed-loop gain of 5 (maximum feedback factor of 0.2). Stability is determined by the phase shift and magnitude of the loop gain. Instability occurs if the loop gain is greater than unity at a frequency where phase shift of $180^{\circ} \mathrm{C}$ can occur.

Wideband decompensated amplifiers can be used as low gains if frequency compensation is used. An example of a unity-gain circuit is shown in Figure 1.

At high frequencies, the $\mathrm{C}_{\mathrm{O}}$ impedance becomes low and resistor $\mathrm{R}_{\mathrm{O}}$ serves to reduce the feedback factor. This circuit has improved AC response with no sacrifice of DC parameters.

## INPUT OFFSET VOLTAGE

Conventional FET-input op amps often have an undesirable interaction between adjustment of input offset voltage and drift. With some designs, CMR is also degraded by adjusting input offset voltage. This family of monolithic FET-input op amps has very little interaction of offset adjustment with other parameters. Each mV of offset adjustment typically


Figure 1. LF157 Unity Gain Operation
causes less than $\pm 0.5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ change in drift. The low initial offset, low drift, and low degree of interaction between offset and drift, all combine to make this amplifier family an ideal choice for any high-gain circuit. For example, the LF356A has a maximum input offset voltage at $25^{\circ} \mathrm{C}$ of 2 mV and a maximum average temperature of $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$. Adjusting input offset on the LF356A will typically cause less than $\pm 1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ of additional drift.

A circuit for adjusting input offset voltage is shown in Figure 2. The range of adjustment will be sufficient to zero any of these amplifiers. For applications requiring very low drift, we recommend using the " $A$ " versions ( $\pm 2 \mathrm{mV}$ VOS Max).


Figure 2. Offset Voltage Adjust

## INPUT BIAS CURRENT

Low input bias current is the primary advantage of using FET-input op amps. The reduction in bias current is approximately 1000:1 when compared to standard 741type op amps. This significantly reduces offset and noise when using high-impedance summing networks or when driving the noninverting input with a high-impedance signal source.

# Monolithic JFET Input Operational Amplifiers 

Because the input bias currents are junction leakage currents, there will be a doubling of bias current for each $10^{\circ} \mathrm{C}$ increase in junction temperature. In normal operation, the junction temperature will rise above the ambient temperature by approximately $10^{\circ} \mathrm{C}$ to $20^{\circ} \mathrm{C}$ due to the internal power dissipation. In addition, input bias current varies somewhat with common-mode voltage and power supply voltages. The performance curves illustrate typical changes in bias current due to these effects. For applications where input bias currents must be minimized, these secondary effects should be considered.

## APPLICATIONS

## General-Purpose Instrumentation Amplifier

The three-op-amp instrumentation amplifier circuit shown in Figure 3 provides excellent performance when implemented with op amps from the LF156 family. The circuit will amplify millivolt-level differential signals with very good rejection of common-mode inputs. The FET-input stages of A1 and A2 provide high-input impedance and very low input-bias-currents. CMR vs frequency is usually good due to the excellent $A C$ response. The interaction between input offset adjustment and drift is unusually low, which is very important when using this circuit at high gain.

Circuit operation is straight-forward: The input amplifiers A1 and A2 buffer and amplify the differential-input-voltage $V_{d}$, and the common-mode voltage $V_{c m}$ is rejected by the output amplifier A3. To adjust offsets, ground both inputs $\left(V_{d} \rightarrow 0\right)$ and set the gain $A_{d}$ to some high value ( $A_{d}>100$ ). Adjust the offset of amplifier A1 for zero at amplifier A3 output ( $\mathrm{V}_{\mathrm{O}} \rightarrow 0$ ). Then open up the gain-setting path ( $\mathrm{R}_{\mathrm{g}} \rightarrow \infty$ ) and adjust amplifier A3 offset pot for zero at amplifier A3 output ( $\mathrm{V}_{\mathrm{O}} \rightarrow 0$ ). Now the gain can be varied over a wide range ( 1 to 1000 is reasonable) without changing the offset.

To adjust common-mode rejection, connect the two amplifier inputs together ( $\mathrm{V}_{\mathrm{d}}=0$ ) and drive them with an AC input. A low-frequency sine wave with an amplitude of about $\pm 10 \mathrm{~V}$ will give the best results. Drive the horizontal input of a scope with the AC signal and observe the output $V_{O}$ on the vertical channel. Vary the CMR adjust pot for minimum peak-to-peak error voltage at $\mathrm{V}_{\mathrm{O}}$. Differential phase shift between amplifiers A 1 and A 2 and amplifier nonlinearities will limit the CMR obtainable, but 100 dB to 120 dB at 60 Hz is practical. One advantage of using the 156 family is that the R2 impedance can be larger than usual due to the low input bias currents. Therefore, the CMR adjust pot value can be chosen to provide improved resolution. A value of $100 \mathrm{k} \Omega$ is a good choice for R2.


Figure 3. Instrumentation Amplifier

Gain can be varied by changing $R_{g}$, and the gain formula is:

$$
V_{o}=\left[1+\frac{2 R_{1}}{R_{g}}\right] V_{d}
$$

Minimum gain is unity and the maximum gain is limited by the op-amp open-loop gain. A gain range of 1 to 1000 is readily achieved with excellent performance.

## High Q, Bandpass Filter

The LF157 version is recommended for use in active filter circuits. The extra margin of AC response provides much higher performance than can be achieved using standard 741-type op amps.

A bandpass filter using LF157 op amps is shown in Figure 4. This circuit uses positive feedback to achieve high Q. A Qrange of 10 to 50 is practical for this circuit. The transfer function for this circuit is:
$\frac{V_{0}(s)}{V_{\text {in }}(s)}=\frac{\frac{1}{R_{1} C_{1}} K s}{s^{2}+\frac{1}{R_{1} C_{1}}\left(2-K \frac{R_{1}}{R_{2}}\right) s+\left(\frac{1}{R_{1} C_{1}}\right)^{2}\left(1+\frac{R_{1}}{R_{2}}+\frac{R_{1}}{R_{3}}\right)}$

Center frequency $f_{0}$ is determined primarily by the time constant $R_{1} C_{1}$ and the ratio of $R_{1}$ to $R_{3}$. Values are chosen such that $R_{1} \gg R_{3}$. A range of 5 to 10 is practical for the gain K.

Center frequency and Q are given by:

$$
\omega_{o}=\frac{1}{R_{1} C_{1}} \sqrt{1+\frac{R_{1}}{R_{2}}+\frac{R_{1}}{R_{3}}}
$$



Center frequency can be most easily set by adjusting $\mathrm{R}_{3}$. The $\mathbf{Q}$ can then be independently set by adjusting gain $K$. Both op amps are operated at loop gains above 5 in this circuit, so the LF157 can be used without encountering stability problems. As with any high-Q bandpass filter, reasonable care must be taken to lead dress, grounding, and power-supply bypassing, to avoid undesired oscillation and noise pick-up.


Monolithic JFET Input Operational Amplifiers

## SELECTION GUIDE

| Model No. | Temp. <br> Range | $V_{\text {os }}($ max $)$ |  | Avg. TC (max) | $\begin{gathered} \mathrm{I}_{\mathrm{OS}} \\ (\max ) \end{gathered}$ | $\underset{(\max )}{I_{b}}$ | Slew Rate | $\underset{(\max )}{I_{c c}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | at $25^{\circ} \mathrm{C}$ | Over T |  |  |  |  |  |

## LOW SUPPLY CURRENT

| LF155 | $-55 / 125$ | 5 mV | 7.0 mV |  | 20 pA | 100 pA | $5 \mathrm{~V} / \mu \mathrm{sec}$ | 4 mA |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LF155A | $-55 / 125$ | 2 mV | 2.5 mV | $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 10 pA | 50 pA | $3 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 4 mA |
| LF255 | $-25 / 85$ | 5 mV | 6.5 mV |  | 20 pA | 100 pA | $5 \mathrm{~V} / \mu \mathrm{sec}$ | 4 mA |
| LF355 | $0 / 70$ | 10 mV | 13.0 mV |  | 50 pA | 200 pA | $5 \mathrm{~V} / \mu \mathrm{sec}$ | 4 mA |
| LF355A | $0 / 70$ | 2 mV | 2.3 mV | $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 10 pA | 50 pA | $3 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 4 mA |

## WIDE BAND

| LF156 | $-55 / 125$ | 5 mV | 7.0 mV |  | 20 pA | 100 pA | $7.5 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 7 mA |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | ---: |
| LF156A | $-55 / 125$ | 2 mV | 2.5 mV | $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 10 pA | 50 pA | $10 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 7 mA |
| LF256 | $-25 / 85$ | 5 mV | 6.5 mV |  | 20 pA | 100 pA | $7.5 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 7 mA |
| LF356 | $0 / 70$ | 10 mV | 13.0 mV |  | 50 pA | 200 pA | $12 \mathrm{~V} / \mu \mathrm{sec}$ | 10 mA |
| LF356A | $0 / 70$ | 2 mV | 2.3 mV | $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 10 pA | 50 pA | $10 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 7 mA |

## WIDE BAND DECOMPENSATED ( $\left.A V_{\min }=5\right)$

| LF157 | $-55 / 125$ | 5 mV | 7.0 mV |  | 20 pA | 100 pA | $30 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 7 mA |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LF157A | $-55 / 125$ | 2 mV | 2.5 mV | $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 10 pA | 50 pA | $40 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 7 mA |
| LF257 | $-25 / 85$ | 5 mV | 6.5 mV |  | 20 pA | 100 pA | $30 \mathrm{~V} / \mu \mathrm{sec}(\mathrm{min})$ | 7 mA |
| LF357 | $0 / 70$ | 10 mV | 13.0 mV |  | 5 pA | 200 pA | $50 \mathrm{~V} / \mu \mathrm{sec}$ | 10 mA |
| LF357A | $0 / 70$ | 2 mV | 2.3 mV | $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 10 pA | 50 pA | $40 \mathrm{VV} / \mu \mathrm{sec}(\mathrm{min})$ | 7 mA |

## HIGH RELIABILITY OPTIONS

| Part Type | Added Screening | To Order: |
| :--- | :--- | :--- |
| $\begin{array}{l}\text { All LF15X } \\ \text { types }\end{array}$ | $\begin{array}{l}\text { With MIL-STD-883 } \\ \text { Class B processing }\end{array}$ | $\begin{array}{l}\text { Add suffix 3 } \\ \text { example: } \\ \text { LF156DE3 }\end{array}$ |
| $\begin{array}{l}\text { All LF35S DE } \\ \text { types } \\ \text { ceramic }\end{array}$ | $\begin{array}{l}\text { With A+3 processing } \\ \text { including burn-in } \\ \text { and tightened AQL* }\end{array}$ | $\begin{array}{l}\text { Add suffix 3 } \\ \text { example: } \\ \text { LF356DE3 }\end{array}$ |
| $\begin{array}{l}\text { All LF35S N } \\ \text { types } \\ \text { plastic }\end{array}$ | $\begin{array}{l}\text { With A+2 processing } \\ \text { including "Hot Rail" } \\ \text { testing, burn-in, } \\ \text { temp cycle and } \\ \text { tightened AQL* } \\ \text { With A+1 processing } \\ \text { including "Hot Rail" } \\ \text { testing, temp cycle } \\ \text { and tightened AQL* }\end{array}$ | $\begin{array}{l}\text { Add suffix 02 } \\ \text { example: } \\ \text { LF356N02 }\end{array}$ |
| Add suffix 01 |  |  |
| example: |  |  |
| LF356N01 |  |  |$]$

*Full description contained in the quality section of this catalog.

## GENERAL DESCRIPTION

The RM709 and RC709 are monolithic, high gain DC operational amplifiers fabricated on a single silicon chip by the planar process.

These devices are designed for use in operational amplifier signal processing, low level instrumentation, control systems and for the generation of special linear and non-linear transfer functions.
The RM709 operates over the full military temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The RC709 is the commercial device intended to operate over a temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Low Input Offset Voltage $\pm 1.0 \mathrm{mV}$ Maximum
- Low Temperature Drift of Input Offset Voltage $\pm 6 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ Maximum
- Low Temperature Drift of Input Offset Current $\left(+25^{\circ} \mathrm{C}\right.$ to $+125^{\circ} \mathrm{C}$ ) $0.3 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ Maximum $\left(-55^{\circ} \mathrm{C}\right.$ to $\left.+25^{\circ} \mathrm{C}\right) 1.0 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ Maximum
- Low Power Consumption 90 mW Maximum
- High Performance Open Loop Gain Characteristics 45k Typical


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\pm 18 \mathrm{~V}$ | Output Short-Circuit Duration ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ) $\ldots . . . \mathrm{S} \mathrm{5ec}$ |
| :---: | :---: | :---: |
| Differential Input Voltage | $\pm 5 \mathrm{~V}$ | Storage Temperature Range . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Input Voltage | $\pm 10 \mathrm{~V}$ | Operating Temperature Range |
| Power Dissipation (Note) |  | RM709/709A . . . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Dual In-line Package | 300 mW | RC709 . . . . . . . . . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| TO-5 Package | 300 mW | Lead Temperature (Soldering, 60s) . . . . . . . . $300^{\circ} \mathrm{C}$ |
| Flat Package | 250 mW |  |

ELECTRICAL CHARACTERISTICS $\left( \pm 9 \leqslant \mathrm{v}_{\mathrm{S}} \leqslant \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM709 |  |  | RC709 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Offset Voltage | $\mathrm{RS}_{S} \leqslant 10 \mathrm{k} \Omega$ |  | 1.0 | 3.0 |  | 2.0 | 7.5 | mV |
| Input Offset Current |  |  |  | 100 |  | 100 | 500 | nA |
| Input Bias Current |  |  | 180 | 300 |  | 300 | 1500 | nA |
| Input Resistance |  | 220 | 400 |  | 50 | 250 |  | $\mathrm{k} \Omega$ |
| Output Resistance |  |  | 150 |  |  | 150 |  | $\Omega$ |
| Supply Current | $V_{S}= \pm 15 \mathrm{~V}$ |  | 2.6 | 4.0 |  |  | 6.6 | mA |
| Power Consumption | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ |  |  | 120 |  | 80 | 200 | mW |
| Transient Response | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=20 \mathrm{mV}$ |  |  |  |  |  |  |  |
| Rise Time | $\begin{aligned} & C_{1}=5 n F, R_{1}=1.5 k \\ & C_{2}=200 \rho F, R_{2}=50 \Omega \end{aligned}$ |  | 0.3 | 1.0 |  | 0.3 | 1.0 | $\mu \mathrm{s}$ |
| Overshoot | $C_{L} \leqslant 100 \mathrm{pF}$ |  |  | 30 |  | 10 | 30 | \% |
| Slew Rate | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega, \mathrm{AV}=1$ | 0.15 | 0.4 |  |  | 0.4 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Large Signal Voltage Gain | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k}, \mathrm{V}_{\text {OUT }}= \pm 10 \mathrm{~V}$ |  |  |  | 15 | 45 |  | kV/V |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{RM} ; 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 70^{\circ} \mathrm{C}$ for RC. |  |  |  |  |  |  |  |  |
| Large Signal Voltage Gain | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k}, \mathrm{V}_{\text {OUT }}= \pm 10 \mathrm{~V}$ | 25 | 45 | 70 | 12 |  |  | kV/V |
| Input Offset Voltage | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 4.0 |  |  | 10 | mV |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=\max$ |  | 10 | 100 |  |  |  | nA |
|  | $\mathrm{T}_{A}=\min$ |  |  | 300 |  |  | 750 |  |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=\mathrm{min}$ |  | 400 | 1000 |  |  | 2000 | nA |
| Average Temperature of Coefficient of Input Offset Voltage | $\mathrm{R}_{S}=50 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ to $\mathrm{T}_{A}=\max$ |  | 1.8 | 10 |  |  |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  | $\mathrm{R}_{S}=50 \Omega, \mathrm{~T}_{A}=25^{\circ} \mathrm{C}$ to $\mathrm{T}_{A}=\mathrm{min}$ |  | 1.8 | 10 |  |  |  |  |
|  | $\mathrm{R}_{\mathrm{S}}=10 \mathrm{k}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ to $\mathrm{T}_{A}=\max$ |  | 2.0 |  |  |  |  |  |
|  | $\mathrm{R}_{S}=10 \mathrm{k}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ to $\mathrm{T}_{A}=\mathrm{min}$ |  | 6.0 |  |  |  |  |  |
| Average Temperature Coefficient of Input Offset Current | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ to max |  |  |  |  |  |  | $n \mathrm{~A} /{ }^{\circ} \mathrm{C}$ |
|  | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ to min |  |  |  |  |  |  |  |
| Input Voltage Range | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ | $\pm 8.0$ | $\pm 10$ |  | $\pm 8.0$ | $\pm 10$ |  | V |
| Output Voltage Swing | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega$ | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | V |
|  | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ | $\pm 13$ |  | $\pm 10$ | $\pm 13$ |  |  |
| Input Resistance | $\mathrm{T}_{A}=\mathrm{min}$ | 50 | 125 |  | 35 | 125 |  | $\mathrm{k} \Omega$ |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 70 | 90 |  | 65 | 90 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 150 |  | 25 | 200 | $\mu \mathrm{V} / \mathrm{V}$ |
| Supply Current | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=\max$ |  |  |  |  |  |  | mA |
|  | $V_{S}= \pm 15 \mathrm{~V}, T_{A}=\min$ |  |  |  |  |  |  |  |
| Power Consumpstion | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=\max$ |  |  |  |  |  |  | mW |
|  | $\mathrm{V}_{S}= \pm 15 \mathrm{~V}, \mathrm{~T}_{A}=\min$ |  |  |  |  |  |  |  |

## NOTE:

Derate linearly the maximum power dissipation of the dual in-line package at $8.6 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperature above $+115^{\circ} \mathrm{C}$, of the $\mathrm{TO}-5$ package at $5.6 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperature above $+95^{\circ} \mathrm{C}$ and of the flat package at $5.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperature above $+103^{\circ} \mathrm{C}$. For RC 709 , rating applies for case temperatures to $+70^{\circ} \mathrm{C}$.

## GENERAL DESCRIPTION

The RM725 and RC725 are high performance, high gain operational amplifiers on a silicon planar epitaxial processed chip.
The RM725 military version operates over full temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The commercial RC725 operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.
The RM725 and RC725 offer offset null capability, very high voltage gain and low power consumption over a wide power supply voltage range. They are used for all instrumentation applications requiring precise, low level signal amplification, low noise, low drift and accurate closed loop gain.

## DESIGN FEATURES

- Low Input Noise Current $0.15 \mathrm{pA} / \sqrt{ } \mathrm{Hz}$
- High Open Loop Gain 3,000,000
- Low Input Offset Current 2nA
- Low Input Voltage Drift $0.6 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$
- High Common-Mode Rejection 120dB
- High Input Voltage Range $\pm 14 \mathrm{~V}$
- Wide Power Supply Range $\pm 3 \mathrm{~V}$ to $\pm 22 \mathrm{~V}$
- Offset Null Capability


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION

| TE (TO-99) |
| :---: |
| Metal Can Package |
| (Top View) |

Order Part Nos.
RMO25T, RC725T

## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\pm 22 \mathrm{~V}$ | Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | 500 mW | Operating Temperature Range |  |
| Differential Input Voltage. | $\pm 5 \mathrm{~V}$ | RM725 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) . . | $\pm 22 \mathrm{~V}$ | RC725 | . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Voltage Between Offset Null and $\mathrm{V}^{+}$ | $\pm 0.5 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) | $300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS $\quad\left(\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM725 |  |  | RC725 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage (without external trim) | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 0.5 | 1.0 |  | 0.5 | 2.5 | mV |
| Input Offset Current |  |  | 2.0 | 20 |  | 2.0 | 35 | nA |
| Input Bias Current |  |  | 42 | 100 |  | 42 | 125 | nA |
| Input Noise Voltage | $\mathrm{f}_{\mathrm{O}}=10 \mathrm{~Hz}$ |  | 15 |  |  | 15 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
|  | $\mathrm{f}_{\mathrm{O}}=100 \mathrm{~Hz}$ |  | 9.0 |  |  | 9.0 |  |  |
|  | $\mathrm{f}_{\mathrm{O}}=1 \mathrm{kHz}$ |  | 8.0 |  |  | 8.0 |  |  |
| Input Noise Current | $\mathrm{f}_{\mathrm{O}}=10 \mathrm{~Hz}$ |  | 1.0 |  |  | 1.0 |  | $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |
|  | $\mathrm{f}_{\mathrm{O}}=100 \mathrm{~Hz}$ |  | 0.3 |  |  | 0.3 |  |  |
|  | $\mathrm{f}_{\mathrm{O}}=1 \mathrm{kHz}$ |  | 0.15 |  |  | 0.15 |  |  |
| Input Resistance |  |  | 1.5 |  |  | 1.5 |  | $\mathrm{M} \Omega$ |
| Input Voltage Range |  | $\pm 13.5$ | $\pm 14$ |  | $\pm 13.5$ | $\pm 14$ |  | V |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \\ & \mathrm{~V}_{\text {out }}= \pm 10 \mathrm{~V} \end{aligned}$ | 1,000,000 | 3,000,000 |  | 250,000 | 3,000,000 |  |  |
| Common Mode Rejection Ratio | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 110 | 120 |  | 94 | 120 |  | dB |
| Power Supply Rejection Ratio | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 2.0 | 10 |  | 2.0 | 35 | $\mu \mathrm{V} / \mathrm{V}$ |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega$ | $\pm 12$ | $\pm 13.5$ |  | $\pm 12$ | $\pm 13.5$ |  | V |
|  | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ | $\pm 13.5$ |  | $\pm 10$ | $\pm 13.5$ |  |  |
| Output Resistance |  |  | 150 |  |  | 150 |  | $\Omega$ |
| Power Consumption |  |  | 80 | 105 |  | 80 | 150 | mW |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for RM725; $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C}$ for RC725. |  |  |  |  |  |  |  |  |
| Input Offset Voltage (without external trim) | $\mathrm{RS} \leqslant 10 \mathrm{k} \Omega$ |  |  | 1.5 |  |  | 3.5 | mV |
| Average Input Offset Voltage Drift (without external trim) | $\mathrm{R}_{\mathrm{S}}=50 \Omega$ |  | 2.0 | 5.0 |  | 2.0 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Average Input Offset Voltage Drift (with external trim) | $\mathrm{R}_{\mathrm{S}}=50 \Omega$ |  | 0.6 |  |  | 0.6 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=125^{\circ} \mathrm{C} ; 70^{\circ} \mathrm{C}$ |  | 1.2 | 20 |  | 1.2 | 3.5 | nA |
|  | $\mathrm{T}^{\prime}=-55^{\circ} \mathrm{C} ; 0^{\circ} \mathrm{C}$ |  | 7.5 | 40 |  | 4.0 | 50 |  |
| Average Input Offset Current Drift |  |  | 35 | 150 |  | 10 |  | $\mathrm{pA} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=125^{\circ} \mathrm{C} ; 70^{\circ} \mathrm{C} \\ & \mathrm{~T}_{\mathrm{A}}=-55^{\circ} \mathrm{C} ; 0^{\circ} \mathrm{C} \end{aligned}$ |  | $\begin{aligned} & 20 \\ & 80 \end{aligned}$ | $\begin{aligned} & 100 \\ & 200 \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & 125 \\ & 250 \end{aligned}$ | nA |
| Large Signal Voltage Gain | $\mathrm{T}_{\mathrm{A}}=125^{\circ} \mathrm{C} ; 70^{\circ} \mathrm{C}$ | 1,000,000 |  |  | 125,000 |  |  |  |
|  | $\mathrm{T} \mathrm{A}=-55^{\circ} \mathrm{C} ; 0^{\circ} \mathrm{C}$ | 250,000 |  |  | 125,000 |  |  |  |
| Common Mode Rejection Ratio | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 100 |  |  |  | 115 |  | dB |
| Power Supply Rejection Ratio | RS $\leqslant 10 \mathrm{k} \Omega$ |  |  | 20 |  | 20 |  | $\mu \mathrm{V} / \mathrm{V}$ |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ |  |  | $\pm 10$ |  |  | V |

## NOTES:

1. Rating applies for case temperature to $+125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperature above $+75^{\circ} \mathrm{C}$.
2. For supply voltages less than $\pm 22 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.

## GENERAL DESCRIPTION

The RM741 and RC741 integrated circuits are high performance, high gain internally compensated monolithic operational amplifiers fabricated on a single silicon chip using the planar epitaxial process.
High common-mode voltage range and absence of latch-up tendencies make the RM741 and RC741 ideal for use as a voltage follower. High gain and wide ranges of operating voltages provide superior performance in integrator, summary amplifier and general feedback applications.
Both RM741 and RC741 are pin compatible with the RM709, LM101A and the LM107. The military version, RM741 operates over a temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The commercial version RC 741 operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Supply Voltage $\pm 22 \mathrm{~V}$ RM741, $\pm 18 \mathrm{~V}$ RC741
- Offset Voltage Null Capability
- Short-Circuit Protection
- No Frequency Compensation Required
- No Latch-up
- Large Common-Mode and Differential Voltage Ranges
- Low Power Consumption


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | RM741: $\pm 22 \mathrm{~V}$ | Operating Temperature Range |
| :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | RC741: $\pm 18 \mathrm{~V}$ .. .500 mW |  |
| Differential Input Voltage | . $\pm 30 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) . . . . . . . . . $300^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | . $\pm 15 \mathrm{~V}$ | Output Short-Circuit Duration (Note 3) . . . . . Indefinite |
| Storage Temperature Range | C to $+150^{\circ} \mathrm{C}$ |  |

ELECTRICAL CHARACTERISTICS $\left(\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM741 |  |  | RC741 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage (Note 4) | $\mathrm{RS} \leqslant 10 \mathrm{k} \Omega$ |  | 1.0 | 5.0 |  | 2.0 | 6.0 | mV |
| Input Offset Current |  |  | 20 | 200 |  | 20 | 200 | nA |
| Input Bias Current |  |  | 80 | 500 |  | 80 | 500 | nA |
| Input Resistance |  | 0.3 | 2.0 |  | 0.3 | 2.0 |  | $\mathrm{M} \Omega$ |
| Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {out }}= \pm 10 \mathrm{~V}$ | 50,000 | 200,000 |  | 20,000 | 200,000 |  |  |
| Output Voltage Swing | $\begin{aligned} & R_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega \\ & \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \end{aligned}$ | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Input Voltage Range |  | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{RS} \leqslant 10 \mathrm{k} \Omega$ | 70 | 90 |  | 70 | 90 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 30 | 150 |  | 30 | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Power Consumption |  |  | 50 | 85 |  | 50 | 85 | mW |
| Transient Response (unity gain) <br> Risetime <br> Overshoot | $\begin{aligned} & \mathrm{V}_{\text {in }}=20 \mathrm{mV}, R_{\mathrm{L}}=2 \mathrm{k} \Omega, \\ & \mathrm{C}_{\mathrm{L}} \leqslant 100 \mathrm{pF} \end{aligned}$ |  | $\begin{aligned} & 0.3 \\ & 5.0 \end{aligned}$ |  |  | $\begin{aligned} & 0.3 \\ & 5.0 \end{aligned}$ |  | $\mu \mathrm{s}$ $\%$ |
| Slew Rate (unity gain) | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  | 0.5 |  |  | 0.5 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{RM} 741 ; 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70{ }^{\circ} \mathrm{C}$ for RC741. |  |  |  |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 6.0 |  |  | 7.5 | mV |
| Input Offset Current | $\begin{aligned} & +125^{\circ} \mathrm{C},+70^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C}, 0^{\circ} \mathrm{C} \end{aligned}$ |  |  | 200 |  |  | 300 | nA |
| Input Bias Current | $\begin{aligned} & +125^{\circ} \mathrm{C},+70^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C}, 0^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ |  |  | 500 |  |  | 800 | nA |
| Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {out }}= \pm 10 \mathrm{~V}$ | 25,000 |  |  | 15,000 |  |  |  |
| Output Voltage Swing | $\begin{aligned} & R_{L} \geqslant 10 k \\ & R_{L} \geqslant 2 k \Omega \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm 12 \\ & \pm 10 \\ & \hline \end{aligned}$ |  |  | $\pm 10$ |  |  | V |
| Common Mode Rejection Ratio | $\mathrm{RS} \leqslant 10 \mathrm{k} \Omega$ | 70 |  |  |  |  |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 150 |  |  |  | $\mu \mathrm{V} / \mathrm{V}$ |


| Supply Current | $+125^{\circ} \mathrm{C}$ |  |  | 2.5 |  |  |  | mA |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
|  | $-55^{\circ} \mathrm{C}$ |  |  | 3.3 |  |  |  | mA |
| Power Consumption | $+125^{\circ} \mathrm{C}$ |  |  |  | 75 |  |  |  |
|  | $-55^{\circ} \mathrm{C}$ |  |  | mW |  |  |  |  |

## NOTES:

1. Rating applies for case temperatures to $+125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+75^{\circ} \mathrm{C}$ for RM 741 .
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Short-circuit may be to ground or either supply. Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature for RM 741 .
4. Offset voltage may be nulled by connecting a $10 \mathrm{k} \Omega$ potentiometer accross the balance pins and connecting the wiper pin to $\mathrm{V}^{-}$.

## GENERAL DESCRIPTION

The RM747 and RC747 integrated circuits are high gain operational amplifiers internally compensated and constructed on a single silicon chip using the planar epitaxial process.
The military version, RM747, operates over a temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The commercial version, RC747, operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.
Combining the features of the 741 with the close parameter matching and tracking of a dual device on a monolithic chip results in unique performance characteristics. Excellent channel separation allows the use of the dual device in all single 741 operational amplifier applications providing high packaging density. It is especially well suited for applications in differential-in, differential-out as well as in potentiometric amplifiers and where gain and phase matched channels are mandatory.

## DESIGN FEATURES

- Short-Circuit Protection
- No Frequency Compensation Required
- No Latch-Up
- Large Common-Mode and Differential Voltage Ranges
- Low Power Consumption
- Parameter Tracking Over Temperature Range
- Gain and Phase Match Between Amplifiers


## SCHEMATIC DIAGRAM (1/2 Shown)



## CONNECTION INFORMATION



ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\begin{aligned} & \mathrm{RM} 747: \pm 22 \mathrm{~V} \\ & \mathrm{RC} 747: \pm 18 \mathrm{~V} \end{aligned}$ | Storage Temperature Range Operating Temperature Range . RM747 | $\begin{aligned} & -65^{\circ} \mathrm{C} \text { to }+150^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C} \text { to }+125^{\circ} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | 500 mW | RC747: | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) | $300^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | $\pm 15 \mathrm{~V}$ | Output Short-Circuit Duration (Note 3) | Indefinite |

ELECTRICAL CHARACTERISTICS $\mathbf{V}_{C C}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise noted)

| PARAMETER | CONDITIONS | RM747 |  |  | RC747 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{S} \leqslant 10 \mathrm{k} \Omega$ |  | 1.0 | 5,0 |  | 2.0 | 6.0 | mV |
| Input Offset Current |  |  | 20 | 200 |  | 20 | 200 | nA |
| Input Bias Current |  |  | 80 | 500 |  | 80 | 500 | nA |
| Input Resistance |  | 0.3 | 2.0 |  | 0.3 | 2.0 |  | MS2 |
| Large-Signal Voltage Gain | $\begin{gathered} R_{L} \geqslant 2 \mathrm{k} \Omega \\ V_{\text {out }}= \pm 10 \mathrm{~V} \end{gathered}$ | 50,000 | 200,000 |  | 50,000 | 200,000 |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{kS}$ | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | V |
|  | $R_{L} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ | $\pm 13$ |  | $\pm 10$ | $\pm 13$ |  | V |
| Input Voltage Range |  | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{R}_{S} \leqslant 10 \mathrm{kS}$ | 70 | 90 |  | 70 | 90 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 30 | 150 |  | 30 | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Power Consumption |  |  | 100 | 170 |  | 100 | 170 | mW |
| Transient Response (unity gain) <br> Risetime <br> Overshoot | $\begin{gathered} V_{\text {in }}=20 \mathrm{mV} \\ R_{\mathrm{L}}=2 \mathrm{k} \Omega \\ C_{L} \leqslant 100 \mathrm{pF} \end{gathered}$ |  | $\begin{aligned} & 0.3 \\ & 5.0 \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & 0.3 \\ & 5.0 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \mu \mathrm{s} \\ & \% \\ & \hline \end{aligned}$ |
| Slew Rate (unity gain) | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  | 0.5 |  |  | 0.5 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Channel Separation | $\mathrm{f}=1 \mathrm{kHz}$ |  | 98 |  |  | 98 |  | dB |
|  |  |  |  |  |  |  |  |  |

The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{RM} 747 ; 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+70^{\circ} \mathrm{C}$ for RC 747 .


## NOTES:

1. Rating applies for case temperatures to $+125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+75^{\circ} \mathrm{C}$ for RM 747 .
2. For supply voltages less than $\pm 15 \mathrm{~V}$ the absolute maximum input voltage is equal to the supply voltage.
3. Short-circuit may be to ground or either supply. Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature for RC 747 .

## GENERAL DESCRIPTION

The RM748 and RC748 integrated circuits are high performance, high gain monolithic operational amplifiers fabricated on a single silicon chip using the planar epitaxial process. Frequency compensation can be tailored externally to cover a broad range of analog applications.
High common-mode voltage range and absence of latch-up tendencies make the RM748 and RC748 ideal for use as a voltage follower. High gain and wide ranges of operating voltages provide superior performance in integrators, summing amplifiers and general feedback applications. Unity gain compensation is achieved by means of a single 30 pF capacitor.
Both RM748 and RC748 are pin compatible with the RM709, LM101 and RM4101. The military version, RM748 operates over a temperature range from $-55^{\circ} \mathrm{C}$ to $+115^{\circ} \mathrm{C}$ while the commercial version RC 748 operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Offset Voltage Null Capability
- Short-Circuit Protection
- No Latch-up
- Large Common-Mode and Differential Voltage Ranges
- Low Power Consumption


## SCHEMATIC DIAGRAM



CONNECTION INFORMATION


ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | RM748: $\pm 22 \mathrm{~V}$ | Operating Temperature Range RM748 |
| :---: | :---: | :---: |
| Interna | RC748: $\pm 18 \mathrm{~V}$ .. .500 mW |  |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) . . . . . . . . . 3000${ }^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | $\pm 15 \mathrm{~V}$ | Output Short-Circuit Duration (Note 3) . . . . Indefinite |
| Storage Temperature Range . | $5^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |  |

ELECTRICAL CHARACTERISTICS $\left(V_{S}= \pm 15 \mathrm{~V}, T_{A}=25^{\circ} \mathrm{C}\right.$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM748 |  |  | RC748 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 1.0 | 5.0 |  | 2.0 | 6.0 | mV |
| Input Offset Current |  |  | 20 | 200 |  | 20 | 200 | nA |
| Input Bias Current |  |  | 80 | 500 |  | 80 | 500 | nA |
| Input Resistance |  | 0.3 | 2.0 |  | 0.3 | 2.0 |  | $\mathrm{M} \Omega$ |
| Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {out }}= \pm 10 \mathrm{~V}$ | 50,000 | 200,000 |  | 20,000 | 200,000 |  |  |
| Output Voltage Swing | $\begin{aligned} & R_{L} \geqslant 10 k \Omega \\ & R_{L} \geqslant 2 k \Omega \end{aligned}$ | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Input Voltage Range |  | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 70 | 90 |  | 70 | 90 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 30 | 150 |  | 30 | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Power Consumption |  |  | 50 | 85 |  | 50 | 85 | mW |
| Transient Response (unity gain) <br> Risetime <br> Overshoot | $\begin{aligned} & V_{\text {in }}=20 \mathrm{mV}, R_{L}=2 k \Omega, \\ & C_{L} \leqslant 100 p F \end{aligned}$ <br> (Note 4) |  | $\begin{aligned} & 0.3 \\ & 5.0 \end{aligned}$ |  |  | $\begin{aligned} & 0.3 \\ & 5.0 \end{aligned}$ |  | $\begin{gathered} \mu \mathrm{s} \\ \% \end{gathered}$ |
| Slew Rate (unity gain) | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \quad$ (Note 4) |  | 0.5 |  |  | 0.5 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+125{ }^{\circ} \mathrm{C}$ for $\mathrm{RM} 748 ; 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+70{ }^{\circ} \mathrm{C}$ for RC748. |  |  |  |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 6.0 |  |  | 7.5 | mV |
| Input Offset Current | $\begin{aligned} & +125^{\circ} \mathrm{C},+70^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C},+70^{\circ} \mathrm{C} \end{aligned}$ |  |  | $\begin{aligned} & 200 \\ & 500 \end{aligned}$ |  |  | $\begin{aligned} & 300 \\ & 800 \end{aligned}$ | nA |
| Input Bias Current | $\begin{aligned} & +125^{\circ} \mathrm{C},+70^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C},+70^{\circ} \mathrm{C} \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & 800 \\ & 800 \\ & \hline \end{aligned}$ | nA |
| Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {out }}= \pm 10 \mathrm{~V}$ | 25,000 |  |  | 15,000 |  |  |  |
| Output Voltage Swing | $\begin{aligned} & \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \\ & \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ |  |  | $\pm 10$ |  |  | V |
| Common Mode Rejection Ratio | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 70 |  |  |  |  |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 150 |  |  |  | $\mu \mathrm{V} / \mathrm{V}$ |

## NOTES:

1. Rating applies for case temperatures to $+125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+75^{\circ} \mathrm{C}$ for RM 748 .
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Short-circuit may be to ground or either supply. Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature for RM 748 .
4. Compensation capacitor: 30 pF .

## GENERAL DESCRIPTION

The RC1437 and RM1537, previously referred to as the 4709, integrated circuits are monolithic dual high gain operational amplifiers. The device is composed of two 709 operational amplifiers fabricated on a single silicon chip. It has all the outstanding features of the 709.
Due to the inherent matching and tracking of parameters, the 1537/1437 has several unique applications: differential in/out amplifiers, non-inverting amplifiers, gain and phase matched channels.

The RM 1537 operates over a temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ}$ C. RC 1437 is the commercial temperature range device for operation from $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Gain and Phase Matching Between Amplifiers
- Low Temperature Drift $\pm 3 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$
- Large Output Voltage Swing $\pm 14 \mathrm{~V}$ Typical

SCHEMATIC DIAGRAM (1/2 Shown)


## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\pm 18 \mathrm{~V}$ | Operating Temperature Range . RM1537: $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| Differential Mode Input Voltage | $\pm 5 \mathrm{~V}$ | RC1437: $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ |
| Common Mode Input Voltage | $\pm \mathrm{V}^{+} \mathrm{v}$ | Storage Temperature Range . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Power Dissipation | 500 mW | Lead Temperature (Soldering, 60s) . . . . . . . . 3000 |
| Derate above $75^{\circ} \mathrm{C}$ | $5.0 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ | Output Short Circuit Duration (250ㅇ). . . . . . . . . . . . 5 s |

ELECTRICAL CHARACTERISTICS (RM1537: $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$; RC 1437 : $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$, unless otherwise noted)

| PARAMETER | CONDITIONS |  |  | RM1537 |  |  | RC1437 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\begin{aligned} & 50 \Omega \leqslant \mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega \\ & \pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V} \end{aligned}$ |  | $\mathrm{T}^{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 1.0 | 5.0 |  | 1.0 | 7.5 | mV |
|  |  |  |  |  |  | 6.0 |  |  | 10 |  |
| Input Offset Current | $\pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V} \mid$ | RM1537: $+25^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ <br> RC1437: $+25^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ <br> RM1537: $-55^{\circ} \mathrm{C}$ <br> RC1437: $0^{\circ} \mathrm{C}$ <br> RM $1537:+25^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  |  | 50 | 200 |  | 50 | 500 | nA |
|  |  |  |  |  |  | 500 |  |  | 750 |  |
| Input Bias Current | $\pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V}$ | $\begin{aligned} & \text { RM1537: }+25^{\circ} \mathrm{C} \text { to }+125^{\circ} \mathrm{C} \\ & \text { RC1437: }+25^{\circ} \mathrm{C} \text { to }+75^{\circ} \mathrm{C} \\ & \hline \text { RM15337: }-55^{\circ} \mathrm{C} \\ & \text { RC1437: } 0^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ |  |  | 0.2 | 0.5 |  | 0.4 | 1.5 |  |
|  |  |  |  |  |  | 1.5 |  |  | 2.0 |  |
| Input Resistance | $\pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V}$ |  |  | 150 | 400 |  | 50 | 150 |  | k $\Omega$ |
| Output Resistance | $\pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V}$ |  |  |  | 150 |  |  | 150 |  | $\Omega$ |
| Power Consumption | $\mathrm{V}^{+}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=\infty$ |  |  |  | 160 | 225 |  | 160 | 225 | mW |
| Large Signal Voltage Gain | $\mathrm{V}^{+}= \pm 15 \mathrm{~V}, \mathrm{~V}_{0}= \pm 10 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  |  | 25 | 45 | 70 | 15 | 45 |  | KV/V |
| Output Voltage Swing | $\begin{array}{ll} \mathrm{V}^{+}= \pm 15 \mathrm{~V} & \mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega \\ & \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \\ \hline \end{array}$ |  |  | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | V |
| Input Common Mode Voltage | $\mathrm{V}^{+}= \pm 15 \mathrm{~V}$ |  |  | $\pm 8$ | $\pm 10$ |  | $\pm 8$ | $\pm 10$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{RS} \leqslant 10 \mathrm{k} \Omega, \pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V}$ |  |  | 70 | 90 |  | 65 | 90 |  | dB |
| Supply Voltage Rejection Ratio | RS $\leqslant 10 \mathrm{k} \Omega, \pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V}$ |  |  |  |  | 150 |  |  | 200 | $\mu \mathrm{V} / \mathrm{V}$ |
| Transient Response <br> Rise Time Overshoot | $\begin{aligned} & \mathrm{V}^{+}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\mathrm{in}}=20 \mathrm{mV}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, \mathrm{C}_{1}=5 \mathrm{nF}, \\ & \mathrm{R}_{1}=1.5 \mathrm{k} \Omega, \mathrm{C}_{2}=200 \mathrm{pF}, \mathrm{R}_{2}=50 \Omega \end{aligned}$ |  |  |  | 0.3 | $\begin{aligned} & 1.0 \\ & 30 \\ & \hline \end{aligned}$ |  | 0.3 | $\begin{aligned} & 1.0 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mu \mathrm{s} \\ & \% \\ & \hline \end{aligned}$ |
| Average Temperature Coefficient of Input Offset Voltage | $\begin{aligned} \pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V} \mathrm{R}_{\mathrm{S}} & =50 \Omega \\ \mathrm{R}_{\mathrm{S}} & =10 \mathrm{k} \Omega \end{aligned}$ |  |  |  | $\begin{aligned} & 1.5 \\ & 3.0 \end{aligned}$ |  |  | $\begin{aligned} & 1.5 \\ & 3.0 \end{aligned}$ |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Average Temperature Coefficient of Input Offset Current | $\pm 9<\mathrm{V}^{+}< \pm 15 \mathrm{~V}$ |  |  |  | 0.7 |  |  | 0.7 |  | $n \mathrm{~A} /{ }^{\circ} \mathrm{C}$ |
| Channel Separation, $f=10 \mathrm{kHz}$ | $\pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V}$ |  |  |  | 90 |  |  | 90 |  | dB |

MATCHING CHARACTERISTICS ( $T_{A}=25^{\circ} \mathrm{C}, \pm 9 \mathrm{~V}<\mathrm{V}^{+}< \pm 15 \mathrm{~V}$ unless otherwise noted)

| PARAMETER | RM1537 |  | RC1437 |  | UNITS |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN | TYP | MAX | MIN |  | MAX |  |
| Voltage Gain |  | $\pm 1.0$ |  |  | $\pm 1.0$ |  | dB |
| Input Bias Current |  | $\pm 100$ |  |  | $\pm 150$ |  | nA |
| Input Offset Current |  | $\pm 15$ |  |  | $\pm 20$ |  | nA |
| Input Offset Voltage |  | $\pm 0.5$ |  |  | $\pm 1.0$ |  | mV |
| Average Temperature Coefficient of Input Offset Voltage |  | $\pm 0.5$ |  |  | $\pm 0.5$ |  | $\mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| Average Temperature Coefficient of Input Offset Current |  | $\pm 0.2$ |  |  | $\pm 0.2$ |  | $\mathrm{nA} /{ }^{\circ} \mathrm{C}$ |

## GENERAL DESCRIPTION

The RM1558 and RC1458 integrated circuits are high gain operational amplifiers internally compensated and constructed on a single silicon chip using the planar epitaxial process.
The military version, RM1558, operates over a temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The commercial version, RC1458, operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.
Combining all of the features of the 741 with the close parameter matching and tracking of a dual device on a monolithic chip results in unique performance characteristics. It is especially well suited for applications where gain and phase matched channels are mandatory.

## DESIGN FEATURES

- Short-Circuit Protection
- No Frequency Compensation Required
- No Latch-Up
- Large Common-Mode and Differential Voltage Ranges
- Low Power Consumption
- Parameter Tracking Over Temperature Range
- Gain and Phase Match Between Amplifiers



## CONNECTION INFORMATION



## Dual 741 General Purpose Operational Amplifier

## ABSOLUTE MAXIMUM RATINGS



ELECTRICAL CHARACTERISTICS $\left(V_{C C}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$ unless otherwise noted)

| PARAMETER | CONDITIONS | RM1558 |  |  | RC1458 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{RS}_{S} \leqslant 10 \mathrm{k} \Omega$ |  | 1.0 | 5.0 |  | 2.0 | 6.0 | mV |
| Input Offset Current |  |  | 30 | 200 |  | 30 | 200 | nA |
| Input Bias Current |  |  | 200 | 500 |  | 200 | 500 | nA |
| Input Resistance |  | 0.3 | 1.0 |  | 0.3 | 1.0 |  | MS2 |
| Large-Signal Voltage Gain | $\begin{aligned} & R_{L} \geqslant 2 \mathrm{k} \Omega \\ & V_{\text {out }}= \pm 10 \mathrm{~V} \end{aligned}$ | 50,000 | 200,000 |  | 50,000 | 200,000 |  | V/V |
| Output Voltage Swing | $R_{L} \geqslant 10 \mathrm{k} \Omega$ | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | V |
|  | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ | $\pm 13$ |  | $\pm 10$ | $\pm 13$ |  | V |
| Input Voltage Range |  | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 70 | 90 |  | 70 | 90 |  | dB |
| Supply Voltage Rejection Ratio | RS $\leqslant 10 \mathrm{k} \Omega$ |  | 30 | 150 |  | 30 | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Power Consumption |  |  | 100 | 150 |  | 100 | 170 | mW |
| Transient Response (unity gain) | $\begin{aligned} V_{\text {in }} & =20 \mathrm{mV} \\ R_{L} & =2 \mathrm{k} \Omega \\ C_{L} & \leqslant 100 \mathrm{pF} \end{aligned}$ |  |  |  |  |  |  |  |
| Risetime |  |  | 0.3 |  |  | 0.3 |  | $\mu \mathrm{s}$ |
| Overshoot |  |  | 5.0 |  |  | 5.0 |  | \% |
| Slew Rate (unity gain) | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  | 0.5 |  |  | 0.5 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Channel Separation | $f=1 \mathrm{kHz}$ |  | 98 |  |  | 98 |  | dB |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{RM} 1558 ; 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+70^{\circ} \mathrm{C}$ for RC1458. |  |  |  |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{L}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 6.0 |  |  | 7.5 | mV |
| Input Offset Current | $\begin{aligned} & +125^{\circ} \mathrm{C},+70^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C}, 0^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & 200 \\ & 500 \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & 300 \\ & 300 \\ & \hline \end{aligned}$ | nA |
| Input Bias Current | $\begin{aligned} & +125^{\circ} \mathrm{C},+70^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C} .+70^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & 500 \\ & 1500 \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & 800 \\ & 800 \\ & \hline \end{aligned}$ | $n \mathrm{~A}$ |
| Large-Signal Voltage Gain | $\begin{gathered} \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \\ \mathrm{~V}_{\text {out }}= \pm 10 \mathrm{~V} \end{gathered}$ | 25,000 |  |  | 25,000 |  |  |  |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\begin{array}{r}  \pm 12 \\ \pm 10 \\ \hline \end{array}$ |  |  | $\pm 10$ |  |  | V |
| Power Consumption | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ |  |  |  |  |  |  |  |
|  | $\mathrm{TA}=+125^{\circ} \mathrm{C}$ |  |  | 150 |  |  | 150 | mW |
|  | $\mathrm{T}^{\prime} \mathrm{A}=-55^{\circ} \mathrm{C}$ |  |  | 200 |  |  | 200 |  |
| Input Voltage Range |  | $\pm 12$ |  |  | $\pm 12$ |  |  | V |

## NOTES:

1. Rating applies for case temperatuers to $+125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+75^{\circ} \mathrm{C}$ for RM 1558 .
2. For supply voltages less than $: 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Short-circuit may be to ground or either supply. Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature for RC1458.

## GENERAL DESCRIPTION

The RM1556/RC1556 are high performance, high gain operational amplifiers. Each amplifier is internally compensated and fabricated on a single silicon chip by the planar epitaxial process.
These amplifiers feature high common-mode and differential voltage range, very low input bias current, optimum performance over a wide range of supply voltage, and freedom from "latch-up." They are ideal for use as voltage followers, comparators, integrators, summing and general purpose amplifiers.
The RM types operate over a temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The RC types operate from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Input Bias Current 15nA Maximum
- Input Offset Current 2nA Maximum
- Input Offset Voltage 4 mV Maximum
- At $\pm 15 \mathrm{~V}$ Current Drain 1.0 mA
- Offset Voltage Nulling (10k pot)
- Slew Rate $2.0 \mathrm{~V} / \mu \mathrm{s}$
- Unity Gain Bandwidth 4 MHz
- Gain Variation 3 dB from $\pm 3 \mathrm{~V}$ to $\pm 20 \mathrm{~V}$
- Open Loop Voltage Gain 106dB


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



Order Part Nos.:
RM1556T, RC1556T

NB Dual In-line
Plastic Package
(Top View)


Order Part No.: RC1556NB

| PIN | FUNCTION |
| :---: | :--- |
| 1 | BAL |
| 2 | -INPUT |
| 3 | +INPUT |
| 4 | V $^{-}$ |
| 5 | BAL |
| 6 | OUTPUT |
| 7 | $V^{+}$ |
| 8 | NC $^{+}$ |

## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | RM1556: $\pm 22 \mathrm{~V}$ <br> RC1556. +18V |  |
| :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | 500 mW | RC1556. . . . . . . . . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) . . . . . . . . . $300^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | $\pm 15 \mathrm{~V}$ | Output Short-Circuit Duration (Note 3) . . . . . Indefinite |
| Storage Temperature Range | $5^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |  |

## RM1556 AND RC1556 ELECTRICAL CHARACTERISTICS

(RM1556: $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant 125^{\circ} \mathrm{C} ; \mathrm{RC} 1556: 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 70^{\circ} \mathrm{C} ; \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM1556 |  |  | RC1556 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k} \Omega$ |  | 2.0 | 4.0 |  | 5.0 | 10 | mV |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 1.0 | 2.0 |  | 5.0 | 10 | $n A$ |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 8.0 | 15 |  | 15 | 30 | nA |
| Input Resistance | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 5.0 |  |  | 3.0 |  | $\mathrm{M} \Omega$ |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 1.0 | 1.5 |  | 1.3 | 3.0 | mA |
| Large Signal Voltage Gain | $\begin{aligned} & \mathrm{T}_{A}=25^{\circ} \mathrm{C} \\ & \mathrm{~V}_{\text {OUT }}= \pm 10 \mathrm{~V}, R_{\mathrm{L}}>2 \mathrm{k} \Omega \end{aligned}$ | 100 | 200 |  | 70 | 100 |  | $\mathrm{V} / \mathrm{mV}$ |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k} \Omega$ |  |  | 6.0 |  |  | 14 | mV |
| Input Offset Current | $+25^{\circ} \mathrm{C}$ to $\mathrm{T}_{\mathrm{H}}$ |  |  | 3.0 |  |  | 14 | $n \mathrm{~A}$ |
|  | $\mathrm{T}_{\mathrm{L}}$ to $+25^{\circ} \mathrm{C}$ |  |  | 5.0 |  |  | 14 |  |
| Input Bias Current |  |  |  | 30 |  |  | 40 | nA |
| Supply Current |  |  |  | 1.9 |  |  | 3.5 | mA |
| Slew Rate (Unity Gain) | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  | 2.0 |  |  | 2.0 |  | $\mathrm{V} / \mathrm{\mu s}$ |
| Bandwidth (Unity Gain) | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  | 4 |  |  | 4 |  | MHz |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {OUT }}= \pm 10 \mathrm{~V}$ | 40 |  |  | 40 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$, | $\pm 12$ | $\pm 13$ |  | $\pm 11$ | $\pm 12$ |  | V |
| Input Voltage Range |  | $\pm 12$ | $\pm 13$ |  | $\pm 11$ | $\pm 12$ |  | V |
| Input Noise Voltage | $\begin{aligned} & \mathrm{R}_{\mathrm{S}}=10 \mathrm{k} \Omega, \mathrm{f}=1.0 \mathrm{kHz}, \\ & \mathrm{AV}=100, B W=1.0 \mathrm{~Hz} \end{aligned}$ |  | 25 |  |  | 25 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| Common-Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k} \Omega$ | 80 | 110 |  | 70 | 110 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{L}} \leqslant 50 \mathrm{k} \Omega$ | 80 | 86 |  | 74 | 83 |  | dB |

## NOTES:

1. For operating at elevated temperatures, the device must be derated based on $150^{\circ} \mathrm{C}$ for RM1556; $100^{\circ} \mathrm{C}$ for RC1556 maximum junction temperature and a thermal resistance of $150^{\circ} \mathrm{C} / \mathrm{W}$ junction to ambient or $45^{\circ} \mathrm{C} / \mathrm{W}$ junction to case.
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Short-circuit to ground rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature for RM1556.

TYPICAL ELECTRICAL DATA


## Dual High Performance Operational Amplifiers

## GENERAL DESCRIPTION

The LH2101A series of dual operational amplifiers are two LM101A type op amps in a single hermetic package. Featuring all the same performance characteristics of the single, these duals offer in addition closer thermal tracking, lower weight, reduced insertion cost, and smaller size than two singles.

The LH2101A is specified for operation over the $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ military temperature range. The LH2201A is specified for operation over the
$-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range. The LH 2301 A is specified for operation over the $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ temperature range.

## DESIGN FEATURES

- Low offset voltage
- Low offset current
- Guaranteed drift characteristics
- Offsets guaranteed over entire common mode and supply voltage ranges
- Slew rate of $10 \mathrm{~V} / \mu \mathrm{s}$ as a summing amplifier


## CONNECTION DIAGRAM

FUNCTION
IN

## AUXILIARY CIRCUITS

(nverting Amplifier with Balancing Circuit

## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . $\pm 22 \mathrm{~V}$ | Operating Temperature Range | LH2101A . $-55^{\circ} \mathrm{C}$ to $115^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| Power Dissipation (Note 1) . . . . . . . . . . . . . . . . 500 mW |  | LH2201A . $-25^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ |
| Differential Input Voltage. . . . . . . . . . . . . . . . . . . $\pm 30 \mathrm{~V}$ |  | LH2301A . . $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) . . . . . . . . . . . . . . . . . . . . . $\pm 15 \mathrm{~V}$ | Storage Temperature Range. | . $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ |
| Output Short-Circuit Duration. . . . . . . . . . . Continuous | Lead Temperature (Soldering, | $10 \mathrm{sec}) . . . . . . . . . .300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS each side (Note 3)

| PARAMETER | CONDITIONS | LIMITS |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LH2101A | LH2201A | LH2301A |  |
| Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k} \Omega$ | 2.0 | 2.0 | 7.5 | $m V$ Max |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 10 | 10 | 50 | $n A$ Max |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 75 | 75 | 250 | $n A$ Max |
| Input Resistance | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 1.5 | 1.5 | 0.5 | $\mathrm{M} \Omega \mathrm{Min}$ |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{S}= \pm 20 \mathrm{~V}$ | 3.0 | 3.3 | 3.0 | $m A$ Max |
| Large Signal Voltage Gain | $\begin{aligned} & T_{A}=25^{\circ} \mathrm{C}, \mathrm{~V}_{S}= \pm 15 \mathrm{~V} \\ & V_{\text {OUT }}= \pm 10 \mathrm{~V}, R_{L} \geqslant 2 \mathrm{k} \Omega \end{aligned}$ | 50 | 50 | 25 | $\mathrm{V} / \mathrm{mV}$ Min |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k} \Omega$ | 3.0 | 3.0 | 10 | $m V$ Max |
| Average Temperature |  | 15 | 15 | 30 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ Max |
| Coefficient of Input Offset Voltage |  |  |  |  |  |
| Input Offset Current |  | 20 | 20 | 70 | $n A$ Max |
| Average Temperature | $25^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{\mathrm{A}} \leqslant 125^{\circ} \mathrm{C}$ | 0.1 | 0.1 | 0.3 | $\mathrm{nA} /{ }^{\circ} \mathrm{C} \operatorname{Max}$ |
| Coefficient of Input Offset Current | $-55^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 25^{\circ} \mathrm{C}$ | 0.2 | 0.2 | 0.6 | $\mathrm{nA} /^{\circ} \mathrm{C} \text { Max }$ |
| Input Bias Current |  | 100 | 100 | 300 | $n A$ Max |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=+125^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 20 \mathrm{~V}$ | 2.5 | 2.5 |  | $m A M a x$ |
| Large Signal Voltage Gain | $\begin{aligned} & V_{S}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}= \pm 10 \mathrm{~V} \\ & R_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \end{aligned}$ | 25 | 25 | 15 | $\mathrm{V} / \mathrm{mV}$ Min |
| Output Voltage Swing | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | $\pm 12$ | $\pm 12$ | $\pm 12$ | $V$ Min |
|  | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega$ | $\pm 10$ | $\pm 10$ | $\pm 10$ | $V$ Min |
| Input Voltage Range | $V_{S}= \pm 20 \mathrm{~V}$ | $\pm 15$ | $\pm 15$ | $\pm 12$ | $\checkmark$ Min |
| Common Mode <br> Rejection Ratio | $\mathrm{RS} \leqslant 50 \mathrm{k} \Omega$ | 80 | 80 | 70 | dB Min |
| Supply Voltage Rejection Ratio | $R_{S} \leqslant 50 \mathrm{k} \Omega$ | 80 | 80 | 70 | dB Min |

NOTES:
(1) The maximum junction temperature of the LH2101A is $150^{\circ} \mathrm{C}$, while that of the LH2201A is $100^{\circ} \mathrm{C}$. For operating temperatures, devices in the flat package, the derating is based on a thermal resistance of $185^{\circ} \mathrm{C} / \mathrm{W}$ when mounted on a $1 / 16$-inch-thick epoxy glass board with 0.03 -inchwide, 2 -ounce copper conductors. The thermal resistance of the dual-in-line package is $100^{\circ} \mathrm{C} / \mathrm{W}$, junction to ambient.
(2) For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
(3) These specifications apply for $\pm 5 \mathrm{~V} \leqslant \mathrm{~V}_{S} \leqslant \pm 20 \mathrm{~V}$ and $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant 125^{\circ} \mathrm{C}$, unless otherwise specified. With the LH2201A, however, all temperature specifications are limited to $-25^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 85^{\circ} \mathrm{C}$. For the LH 2301 A these specifications apply for $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 70^{\circ} \mathrm{C}, \pm 5 \mathrm{~V}$ and $\leqslant \mathrm{V}_{S} \leqslant$ $\pm 15 \mathrm{~V}$. Supply current and input voltage range are specified as $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ for the LH2301A. $\mathrm{C}_{1}=30 \mathrm{pF}$ unless otherwise specified.

## Quad Current Mode Single-Supply Operational Amplifiers

## GENERAL DESCRIPTION

The LM2900 and LM3900 consist of four independent, dual input, internally compensated amplifiers which were designed specifically to operate off a single power supply voltage and to provide a large output voltage swing. These amplifiers make use of a current mirror to achieve the non-inverting input function. Application areas include: AC amplifiers, RC active filters; low frequency triangle, squarewave and pulse waveform generation circuits, tachometers and low speed, high voltage digital logic gates.

## DESIGN FEATURES

- Wide Single Supply Voltage Range 4 V to 36 V
- Supply Current Drain Independent of Supply Voltage
- Low Input Biasing Current 30 nA
- High Open-loop Gain 70 dB
- Wide Bandwidth 2.5 MHz (Unity Gain)
- Larger Gain-Bandwidth Product in Non-Inverting Mode ( $A V=100 @ f=1 \mathrm{MHz}$ )
- Large Output Voltage Swing, $\left(V^{+}-1\right) V_{p . p}$
- Internally Frequency Compensated for Unity Gain
- Output Short-Circuit Protection

SCHEMATIC DIAGRAM (1/4 Shown)


## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage (LM 2900) <br> (LM 3900) | $\begin{aligned} & .+36 \mathrm{~V} \\ & .+32 \mathrm{~V} \end{aligned}$ | Output Short Circuit Duration - . . . . . . . . Continuous One Amplifier, TA $=25^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| Supply Voltage | $\pm 18 \mathrm{~V}$ | Operating Temperature Range (LM 2900). $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Power Dissipation ( $T_{\text {A }}=25^{\circ} \mathrm{C}$ ) (Note 1) | 570 mW | Operating Temperature Range (LM 3900) . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Input Currents, IIN+ or IIN- | 20 mA | Storage Temperature Range . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
|  |  | Lead Temperature (Soldering, 10 sec ) . . . . . . $300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS ( $\mathrm{V}_{\mathrm{CC}}=+15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ unless otherwise noted.)

| PARAMETER | CONDITIONS | LM 2900/LM 3900 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | UNITS |
| Open Loop Voltage Gain | $f=100 \mathrm{~Hz}$ | 1200 | 2800 |  | V/V |
| Input Resistance | Inverting Input |  | 1 |  | $\mathrm{M} \Omega$ |
| Output Resistance |  |  | 8 |  | $k \Omega$ |
| Unity Gain Bandwidth | Inverting Input (Note 2) |  | 2.5 |  | MHz |
| Input Bias Current | Inverting Input |  | 30 | 200 | $n \mathrm{~A}$ |
| Slew Rate | Positive Output Swing |  | 0.5 |  | $\mathrm{V} / \mu \mathrm{s}$ |
|  | Negative Output Swing |  | 20 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Supply Current | $\mathrm{R}_{\mathrm{L}}=\infty$ On All Amplifiers |  | 6.2 | 10 | mA |
| Output Voltage Swing $R_{L}=5.1 \mathrm{k}$ VOUT High | $\mathrm{I}_{1 \mathrm{~N}-}=0,1 \mathrm{~N}+\mathrm{l}=0$ | 13.5 | 14.2 |  | V |
|  | $I_{1 N-}=10 \mu \mathrm{~A}, 1 / \mathrm{N}^{+}=0$ |  | 0.09 | 0.2 | V |
| Output Current Capability | Source | 6 | 18 |  | mA |
|  | Sink (Note 3) | 0.5 | 1.3 |  | mA |
| Power Supply Rejection | $f=100 \mathrm{~Hz}$ |  | 70 |  | dB |
| Mirror Gain | $1 \mathrm{~N}+=200 \mu \mathrm{~A}$ (Note 4) | 0.90 | 1 | 1.1 | $\mu \mathrm{A} / \mu \mathrm{A}$ |
| Mirror Current | (Note 5) |  | 10 | 500 | $\mu \mathrm{A}$ |
| Negative Input Current | (Note 6) |  | 1.0 |  | mA |

## NOTES:

1. For operating at high temperatures, the device must be derated based on a $125^{\circ} \mathrm{C}$ maximum junction temperature and a thermal resistance of $175^{\circ} \mathrm{C} / \mathrm{W}$ which applies for the device soldered in a printed circuit board, operating in a still air ambient.
2. When used as a "non-inverting amplifier", the gain-bandwidth product is not limited to 2.5 MHz . The isolation provided by the "current mirror" allows a constant unity voltage gain feedback for the main inverting amplifier. This means that large values of gain can be achieved at high frequencies and the dominant limit is due to the slew rate of the amplifier. For example: a voltage gain of 100 is easily obtained at 1 MHz and an output voltage swing of $160 \mathrm{mVp}-\mathrm{p}$ can be achieved prior to slew rate limiting. This operational mode is useful for signal frequencies in the 50 kHz to 1 MHz range as would be encountered in IF or carrier frequency applications.
3. The output current sink capability can be increased for large signal conditions by overdriving the inverting input.
4. This spec indicates the current gain of the current mirror which is used as the non-inverting input.
5. Input $V_{B E}$ match between the non-inverting and the inverting inputs occurs for a mirror-current (non-inverting input current) of approximately $10 \mu \mathrm{~A}$. This is therefore a typical design center for many of the application circuits.
6. Clamp transistors are included on the IC to prevent the input voltages from swinging below ground more than approximately $-0.3 \mathrm{~V}_{\mathrm{DC}}$. The negative input currents which may result from large signal overdrive with capacitance input coupling need to be externally limited to values of approximately 1 mA . Negative input currents in excess of 4 mA will cause the output voltage to drop to a low voltage. This maximum current applies to any one of the input terminals. If more than one of the input terminals are simultaneously driven, negative smaller maximum currenis are aiiowed. Com-mon-mode current biasing can be used to prevent negative input voltages; for example, see the "Differentiator Circuit" in the applications section.

Voltage-Controlled Current Source (Transconductance Amplifier)


Free-Running Staircase
Generator/Pulse Counter


Ground Referencing a Differential Input Signal


Triangle/Square Generator


Inverting Amplifier


VBE Biasing


Supplying IIN with Aux. Amp (to Allow High Z Feedback Networks)


Non-Inverting Amplifier


Split Supply ( $\mathrm{V}^{+}=+15 \mathrm{~V}_{\mathrm{DC}} \& \mathrm{~V}^{-}=-15 \mathrm{~V} \mathrm{DC}$ ) Non-Inverting DC Gain

AC Amplifier


## GENERAL DESCRIPTION

The 3078 and 3078A are high-gain monolithic operational amplifiers which can deliver milliamperes of current yet only consume microwatts of standby power. Their operating points are externally adjustable and frequency compensation may be accomplished with one external capacitor. The 3078 and 3078A provide the designer with the opportunity to tailor the frequency response and improve the slew rate without sacrificing power. Operation with a single 1.5 -volt battery is a practical reality with these devices.

The 3078A is a premium device having a supply voltage range of $\mathrm{V}^{ \pm}=0.75 \mathrm{~V}$ to $\mathrm{V}^{ \pm}=15 \mathrm{~V}$ and an operating temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The 3078 has the same lower supply voltage limit but the upper limit is $\mathrm{V}^{+}=+6 \mathrm{~V}$ and $\mathrm{V}^{-}=-6 \mathrm{~V}$. The operating temperature range is from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Low Standby Power: As Low as 700 nW
- Wide Supply Voltage Range: $\pm 0.75$ to $\pm 15 \mathrm{~V}$
- High Peak Output Current: 6.5 mA min.
- Adjustable Quiescent Current
- Output Short-circuit Protection


## APPLICATIONS

- Portable Electronics
- Medical Electronics
- Instrumentation
- Telemetry


## SCHEMATIC DIAGRAM



Figure 1. Schematic Diagram.

## CONNECTION INFORMATION



TE
Metal Can Package


Order Part Nos.: RC3078T, RM3078A T

| PIN | FUNCTION |
| :---: | :--- |
| 1 | COMP |
| 2 | INV. INPUT |
| 3 | NON-INV. INPUT |
| 4 | V $^{-}$ |
| 5 | BIAS |
| 6 | OUTPUT |
| 7 | $V^{+}$ |
| 8 | COMP |

ABSOLUTE MAXIMUM RATINGS
(Absolute Maximum Values at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )

|  | 3078 | 3078 |
| :---: | :---: | :---: |
| DC Supply Voltage (between $\mathrm{V}^{+}$and $\mathrm{V}^{-}$(terminal. | 36 V | 14 V |
| Differential Input Voltage. | $\pm 6 \mathrm{~V}$ | $\pm 6 \mathrm{~V}$ |
| DC Input Voltage | $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ | $\mathrm{V}^{+}$to $\mathrm{V}^{-}$ |
| Input Signal Current | 0.1 mA | 0.1 mA |
| Output Short-Circuit Duration* | No Limitation | No Limitation |
| Device Dissipation. | 250 mW (up to ( $125^{\circ} \mathrm{C}$ ) | 500 mW (up to $70^{\circ} \mathrm{C}$ ) |
| Temperature Range: |  |  |
| Operating. | -55 to $+125^{\circ} \mathrm{C}$ | 0 to $+70^{\circ} \mathrm{C}$ |
| Storage | -65 to $+150^{\circ} \mathrm{C}$ | -65 to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (During Soldering): |  |  |
| At distance $1 / 16 \pm 1 / 32 \mathrm{in}$. ( $1.59 \pm 0.79 \mathrm{~mm}$ ) from case for 10 s max. | $+300^{\circ} \mathrm{C}$ | $+300^{\circ} \mathrm{C}$ |

*Short circuit may be applied to ground or to either supply.

ELECTRICAL CHARACTERISTICS (For Equipment Design)

| CHARACTERISTICS | SYMBOLS | TEST CONDITIONS |  |  | 3078A |  |  |  |  | 3078 |  |  |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | RS | T $=5$. | . $1 \mathrm{M} \Omega$, | $1 \mathrm{Q}=20$ | $\mu \mathrm{A}$ | RSE | $\mathrm{T}=13$ | MS2, 10 | $=100$ | $\mu \mathrm{A}$ |  |
|  |  | $\begin{array}{\|l} \hline \mathrm{v}^{+} \\ \& \\ \mathrm{v}^{-} \end{array}$ | $\begin{aligned} & \mathrm{RS} \\ & \mathrm{~K} \Omega 2 \end{aligned}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{L}} \\ & \mathrm{~K} \Omega \end{aligned}$ | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  |  | $\begin{gathered} \mathrm{T}_{\mathrm{A}}=-55 \text { to } \\ 125^{\circ} \mathrm{C} \end{gathered}$ |  | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  |  | $\begin{gathered} \mathrm{T}_{\mathrm{A}}=0 \text { to } \\ 70^{\circ} \mathrm{C} \end{gathered}$ |  |  |
|  |  |  |  |  | MN | TYP | MAX | MIN | MAX | MIN | TYP | MAX | MIN | MAX |  |
| Input Offset Voitage | $\mathrm{V}_{10}$ | 4 | $\leqslant 10$ | - | - | 0.70 | 3.5 | - | 4.5 | - | 1.3 | 4.5 | - | 5 | mV |
| Input Offset Current | 110 | 6 | - | - | - | 0.50 | 2.5 | - | 5.0 | - | 6 | 32 | - | 40 | nA |
| Input Bias Current | $1 / \mathrm{B}$ |  | - | - | - | 7 | 12 | - | 50 | - | 60 | 170 | - | 200 | nA |
| Open-Loop Diff. Voltage Gain | AOL |  | - | $\geqslant 10$ | 92 | 100 | - | 90 | - | 88 | 92 | - | 86 | - | dB |
| Total Quiescent Current | 10 |  | - | - | - | 20 | 25 | - | 45 | - | 100 | 130 | - | 150 | $\mu \mathrm{A}$ |
| Device Dissipation | $\mathrm{P}_{\mathrm{D}}$ |  | - | - | - | 240 | 300 | - | 540 | - | 1200 | 1560 | - | 1800 | $\mu \mathrm{W}$ |
| Maximum Output Voltage | $\mathrm{V}_{\text {OM }}$ |  | -. | $\geqslant 10$ | $\pm 5.1$ | $\pm 5.3$ | - | $\pm 5$ | - | $\pm 5.1$ | $\pm 5.3$ | - | $\pm 5.0$ | - | V |
| Common-Mode Input Voltage Range | VICR | $\dagger$ | $\leqslant 10$ | - | - | $\begin{array}{\|c} \hline-5.5 \\ \text { to } \\ +5.8 \end{array}$ | - | $\begin{aligned} & \hline-5 \\ & \text { to } \\ & +5 \\ & \hline \end{aligned}$ | - | - | $\begin{gathered} -5.5 \\ \text { to } \\ +5.8 \end{gathered}$ | - | $\begin{aligned} & -5 \\ & \text { to } \\ & +5 \end{aligned}$ | - | V |
| Common-Mode Rejection Ratio | CMRR |  | $\leqslant 10$ | - | 80 | 115 | - | - | - | 80 | 110 | - | - | - | dB |
| Maximum Output Current | $\mathrm{IOM}^{+}$or IOM ${ }^{-}$ |  | - | - | - | 12 | - | 6.5 | 30 | - | 12 | - | 6.5 | 30 | mA |
| Input Offset Voltage Sensitivity: Positive | $\Delta \mathrm{V}_{10} / \Delta \mathrm{V}^{+}$ |  | $\leqslant 10$ | - | 76 | 105 | - | - | - | 76 | 93 | - | - | - | $\mu \mathrm{V} / \mathrm{V}$ |
| Negative | $\Delta \mathrm{V}_{10} / \Delta \mathrm{V}^{-}$ |  |  | - | 76 | 105 | - | - | - | 76 | 93 | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  | RSET $=13 \mathrm{M} \Omega, \mathrm{IQ}=20 \mu \mathrm{~A}$ |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{V}_{10}$ | $\bigoplus_{15}^{4}$ | $\leqslant 10$ | - | - | 1.4 | 3.5 | - | 4.5 | - | - | - | - | - | mV |
| Open-Loop Diff. Voltage Gain | AOL |  | - | $\geqslant 10$ | 92 | 100 | - | 88 | - | - | - | - | - | - | dB |
| Total Quiescent Current | 10 |  | - | - | - | 20 | 30 | - | 50 | - | - | - | - | - | $\mu \mathrm{A}$ |
| Device Dissipation | PD | 15 | - | - | - | 600 | 750 | - | 1350 | - | - | - | - | - | $\mu \mathrm{W}$ |
| Maximum Output Voltage | $\mathrm{V}_{\text {OM }}$ | $\dagger$ | - | $\geqslant 10$ | 13.7 | 14.1 | - | 13.5 | - | - | - | - | - | - | V |
| Common-Mode Rejection Ratio | CMRR |  | $\leqslant 10$ | - | 80 | 106 | - |  | - | - | - | - | - | - | dB |
| Input Bias Current | $1 / \mathrm{B}$ |  | - | - | - | 7 | 14 | - | 55 | - | - | - | - | - | nA |
| Input Offset Current | 110 |  | - | - | - | 0.50 | 2.7 | - | 5.5 | - | - | - | - | - | nA |

ELECTRICAL CHARACTERISTICS (At $\left.T_{A}=25^{\circ} \mathrm{C}\right)$

| TYPICAL VALUES |  |  |  | UNITS | CURVES FIG. NO. | CHARACTERISTICS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3078A |  | 3078 |  |  |  |  |
| $\begin{gathered} \mathrm{V}^{+}=+1.3 \mathrm{~V} \\ \mathrm{~V}^{-}=-1.3 \mathrm{~V} \\ \mathrm{RSET}_{\mathrm{SET}}=2 \mathrm{M} \Omega \\ \mathrm{I}_{\mathrm{Q}}=10 \mu \mathrm{~A} \end{gathered}$ | $\begin{gathered} \mathrm{V}^{+}=+0.75 \mathrm{~V} \\ \mathrm{~V}-=-0.75 \mathrm{~V} \\ \text { RSET }=10 \mathrm{M} \Omega \\ \mathrm{I}_{\mathrm{Q}}=1 \mu \mathrm{~A} \end{gathered}$ | $\begin{gathered} \mathrm{V}^{+}=+1.3 \mathrm{~V} \\ \mathrm{~V}^{-}=-1.3 \mathrm{~V} \\ \text { RSET }=2 \mathrm{M} \Omega \\ \mathrm{I}_{\mathrm{Q}}=10 \mu \mathrm{~A} \end{gathered}$ | $\begin{gathered} \mathrm{V}^{+}=0.75 \mathrm{~V} \\ \mathrm{~V}^{-}=-0.75 \mathrm{~V} \\ \mathrm{RSET}=10 \mathrm{M} \Omega \\ \mathrm{I}_{\mathrm{Q}}=10 \mu \mathrm{~A} \end{gathered}$ |  |  |  |
| 0.7 | 0.9 | 1.3 | 1.5 | mV | 3,13 | $\mathrm{V}_{10}$ |
| 0.3 | 0.054 | 1.7 | 0.5 | nA | 4,14 | 110 |
| 3.7 | 0.45 | 9 | 1.3 | nA | 5,15 | IIB |
| 84 | 65 | 80 | 60 | dB | 6, 11, 12, 16 | AOL |
| 10 | 1 | 10 | 1 | $\mu \mathrm{A}$ | 17 | IQ |
| 26 | 1.5 | 26 | 1.5 | $\mu \mathrm{W}$ | - | PD |
| 1.4 | 0.3 | 1.4 | 0.3 | V | 9,10 | VOPP |
| $\begin{gathered} -0.8 \\ \text { to } \\ +1.1 \\ \hline \end{gathered}$ | $\begin{gathered} -0.2 \\ \text { to } \\ +0.5 \\ \hline \end{gathered}$ | $\begin{gathered} -0.8 \\ \text { to } \\ +1.1 \\ \hline \end{gathered}$ | $\begin{gathered} -0.2 \\ \text { to } \\ +0.5 \\ \hline \end{gathered}$ | V | 10 | VICR |
| 100 | 90 | 100 | 90 | dB | - | CMRR |
| 12 | 0.5 | 12 | 0.5 | mA | 8 | $1 \mathrm{OM}^{ \pm}$ |
| 20 | 50 | 20 | 50 | $\mu \mathrm{V} / \mathrm{V}$ | - | $\Delta \mathrm{V}_{10} / \Delta \mathrm{V} \pm$ |

(Typical Values Intended Only for Design Guidance at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ and $\mathrm{V}^{+}=+6 \mathrm{~V}, \mathrm{~V}^{-}=-6 \mathrm{~V}$ )

| CHARACTERISTICS | SYMBOLS | TEST CONDITIONS | 3078A |  | 3078 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} \mathrm{RSET}_{\mathrm{SE}}=5.1 \mathrm{M} \Omega \\ \mathrm{I}_{\mathrm{Q}}=20 \mu \mathrm{~A} \end{gathered}$ | $\begin{gathered} \mathrm{R}_{\mathrm{SET}}=1 \mathrm{M} \Omega \\ \mathrm{I}_{\mathrm{Q}}=100 \mu \mathrm{~A} \end{gathered}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{SET}}=1 \mathrm{M} \Omega \\ & \mathrm{I}_{\mathrm{Q}}=100 \mu \mathrm{~A} \end{aligned}$ | UNITS |
| Input Offset Voltage Drift | $\Delta \mathrm{V}_{\mathrm{IO}} / \Delta \mathrm{T}_{\mathrm{A}}$ | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ | 5 | 6 | 6 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Offset Current Drift | $\Delta \mathrm{V}_{1 \mathrm{O}} / \Delta \mathrm{T}_{\mathrm{A}}$ | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ | 6.3 | 70 | 70 | $\mathrm{pA} /{ }^{\circ} \mathrm{C}$ |
| Open-Loop Bandwidth | BWOL | 3 dB pt. | 0.3 | 2 | 2 | kHz |
| Slew Rate: Unity Gain | SR | $\begin{gathered} \text { See Figures } \\ 20,21 \\ 10 \% \text { to } 90 \% \\ \text { Rise Time } \end{gathered}$ | 0.027 | 0.04 | 0.04 | $\mathrm{V} / \mu \mathrm{s}$ |
| Comparator |  |  | 0.5 | 1.5 | 1.5 |  |
| Transient Response | - |  | 3 | 2.5 | 2.5 | $\mu \mathrm{s}$ |
| Input Resistance | $\mathrm{R}_{1}$ |  | 7.4 | 1.7 | 0.87 | $\mathrm{M} \Omega$ |
| Output Resistance | $\mathrm{R}_{\mathrm{O}}$ |  | 1 | 0.8 | 0.8 | $\mathrm{K} \Omega$ |
| Equiv. Input Noise Voltage | eN (10 Hz) | $\mathrm{R}_{\mathrm{S}}=0$ | 36 | - | 19 | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| Equiv. Input Noise Current | $\mathrm{i}_{\mathrm{N}}(10 \mathrm{~Hz})$ | $\mathrm{R}_{\mathrm{S}}=1 \mathrm{M} \Omega$ | 0.4 | - | 1 | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |



Figure 2. Functional Block Diagram of the 3078 and 3078A.

## TYPICAL CHARACTERISTICS



Figure 3. Input Offset Voltage versus Total Quiescent Current


Figure 5. Input Bias Current versus Total Quiescent Current


Figure 7. Bias-setting Resistance versus Total Quiescent Current


Figure 4. Input Offset Current versus Total Quiescent Current


Figure 6. Open-loop Voltage Gain versus Total Quiescent Current


Figure 8. Maximum Output Current versus Total Quiescent Current

## TYPICAL CHARACTERISTICS



Figure 9. Output Voltage Swing versus Total Quiescent Current


Figure 11. Open-loop Voltage Gain versus
Frequency-3078


Figure 12. Open-loop Voltage Gain versus
Frequency-3078A


Figure 10. Output and Common-mode Voltage versus Supply Voltage


Figure 13. Input Offset Voltage versus Temperature

## TYPICAL CHARACTERISTICS



Figure 14. Input Offset Current versus Temperature


Figure 16. Open-loop Voltage Gain versus Temperature


Figure 18. Equivalent Input Noise Voltage versus Frequency


Figure 15. Input Bias Current versus Temperature


Figure 17. Total Quiescent Current versus Temperature


Figure 19. Equivalent Input Noise Current versus Frequency

## TYPICAL CHARACTERISTICS



Figure 20. Slew Rate versus Closed-loop Gain-3078


Figure 22. Transient Response and Slew-rate Unity Gain (Inverting) Test Circuit


Figure 24. Phase Compensation Capacitance versus Closed-loop Gain-3078


Figure 21. Slew Rate versus Closed-loop Gain-3078A


Figure 23. Slew-rate, Unit Gain (NonInverting) Test Circuit


Figure 25. Phase Compensation Capacitance versus Closed-Ioop Gain-3078A

Table 1. Unity-gain Slew Rate versus Compensation-3078 and 3078A

| SUPPLY VOLTS: $\mathrm{V}^{+}=6, \mathrm{~V}-=-6$ <br> OUTPUT VOLTAGE $\left(\mathrm{V}_{\mathrm{O}}\right)= \pm 5 \mathrm{~V}$ <br> LOAD RESISTANCE ( $\mathrm{R}_{\mathrm{L}}$ ) $=10 \mathrm{~K} \Omega$ | TRANSIENT RESPONSE: 10\% OVERSHOOT FOR AN OUTPUT <br> VOLTAGE OF 100 mV <br> AMBIENT TEMPERATURE ( $T_{A}$ ) $=25^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNITY GAIN (INVERTING) Fig. 22 |  |  |  |  | UNITY GAIN (NON-INVERTING) <br> Fig. 23 |  |  |  |  |
| COMPENSATION <br> TECHNIQUE | R1 | C1 | R2 | C2 | SLEW RATE | R1 | C1 | R2 | C2 | SLEW <br> RATE |
| $3078 \mathrm{~T}-\mathrm{I}_{\mathrm{Q}}=100 \mu \mathrm{~A}$ | K $\Omega$ | pF | K $\Omega$ | $\mu \mathrm{F}$ | $\mathrm{V} / \mu \mathrm{s}$ | K $\Omega$ | pF | $K \Omega$ | $\mu \mathrm{F}$ | $\mathrm{V} / \mu \mathrm{s}$ |
| Single Capacitor | 0 | 750 | $\infty$ | 0 | 0.0085 | 0 | 1500 | $\infty$ | 0 | 0.0095 |
| Resistor and Capacitor | 3.5 | 350 | $\infty$ | 0 | 0.04 | 5.3 | 500 | $\infty$ | 0 | 0.024 |
| Input | $\infty$ | 0 | 0.25 | 0.306 | 0.67 | $\infty$ | 0 | 0.311 | 0.45 | 0.67 |
| $3078 \mathrm{AT}-\mathrm{I}_{\mathrm{Q}}=20 \mu \mathrm{~A}$ |  |  |  |  |  |  |  |  |  |  |
| Single Capacitor | 0 | 300 | $\infty$ | 0 | 0.0095 | 0 | 800 | $\infty$ | 0 | 0.003 |
| Resistor and Capacitor | 14 | 100 | $\infty$ | 0 | 0.027 | 34 | 125 | $\infty$ | 0 | 0.02 |
| Input | $\infty$ | 0 | 0.644 | 0.156 | 0.29 | $\infty$ | 0 | 0.77 | 0.4 | 0.4 |

## OPERATING CONSIDERATIONS

## Compensation Techniques

The 3078AT and 3078T can be phase-compensated with one or two external components depending upon the closed-loop gain, power consumption, and speed desired. The recommended compensation is a resistor in series with a capacitor connected from terminal 1 to terminal 8. Values of the resistor and capacitor required for compensation as a function of closed loop gain are shown in Figures 24 and 25. These curves represent the compensation necessary at quiescent currents of $20 \mu \mathrm{~A}$ and $100 \mu \mathrm{~A}$, respectively, for a transient with $10 \%$ overshoot. Figures 21 and 22 show the slew rates that can be obtained with the two different compensation techniques. Higher speeds can be achieved with input compensation, but
this increases noise output. Compensation can also be accomplished with a single capacitor connected from terminal 1 to terminal 8 , with speed being sacrificed for simplicity. Table 1 gives an indication of slew rates that can be obtained with various compensation techniques at quiescent currents of $20 \mu \mathrm{~A}$ and $100 \mu \mathrm{~A}$.

## Single Supply Operation

The 3078AT and 3078T can operate from a single supply with a minimum total supply voltage of 1.5 volts. Figures 27 and 28 show the 3078AT or 3078T in inverting and non-inverting 20-dB amplifier configurations utilizing a 1.5 -volt type "AA" cell for a supply. The total power consumption for either circuit is approximately 675 nanowatts. The output voltage swing in this configuration is 300 mV p-p with a $20 \mathrm{~K} \Omega$ load.


NON-INVERTING

${ }^{*} R_{B} \approx \frac{R_{I} R_{F} V_{+}}{\left(R_{1}+R_{F}\right) 7.5 \times 10-3}$
assuming $R_{B} \gg \frac{R_{l} R_{F}}{R_{j}+R_{F}}$

Figure 26. Offset Voltage Null Circuit

## SCHEMATIC DIAGRAM



Figure 27. Inverting 20 dB Amplifier Circuit


Figure 28. Non-inverting 20 dB Amplifier Circuit

## GENERAL DESCRIPTION

The RV3301 and RC3401 consist of four independent amplifiers, with internal frequency compensation, designed to operate from a single power supply.
These amplifiers employ a current mirror to achieve the noninverting inputs.
The current-differencing inputs allow a variety of applications in automotive instrumentation, industrial and consumer circuits for performing active filtering and pulse and waveform generation and processing.

## DESIGN FEATURES

- Wide Supply Voltage Range 4 to 28 V
- Wide Operating Temperature Range $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
- Wide Bandwidth Unity Gain 4 MHz
- Low Input Bias Current 50 nA


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS



ELECTRICAL CHARACTERISTICS ( $\mathrm{V}_{\mathrm{CC}}=+15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=5.0 \mathrm{~K} \Omega, \mathrm{~T}_{\mathrm{A}}=+25{ }^{\circ} \mathrm{C}$ unless otherwise noted.)

| Characteristic | Conditions | NOTE | 3301 |  |  | 3401 |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Open-Loop Voltage Gain | $\begin{aligned} & \mathrm{T}_{A}=+25^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 85^{\circ} \mathrm{C} \\ & 0{ }^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 75^{\circ} \mathrm{C} \end{aligned}$ | 1 | 1000 | $\begin{aligned} & 2000 \\ & 1600 \end{aligned}$ |  | $\begin{aligned} & 1000 \\ & 800 \end{aligned}$ | 2000 |  | V/V |
| Quiescent Power Supply Current (Total for 4 amplifiers) <br> Noninverting inputs open <br> Noninverting inputs grounded |  | 2 |  | $\begin{aligned} & 6.9 \\ & 7.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 10 \\ & 14 \end{aligned}$ |  | $\begin{aligned} & 6.9 \\ & 7.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 10 \\ & 14 \\ & \hline \end{aligned}$ | mA |
| Input Bias Current | $\begin{aligned} & R_{L}=\infty \\ & T_{A}=+25^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+85^{\circ} \mathrm{C} \\ & 0^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+75^{\circ} \mathrm{C} \end{aligned}$ | 3 |  | $\begin{gathered} 50 \\ 100 \end{gathered}$ | 300 |  | 50 | $\begin{aligned} & 300 \\ & 500 \end{aligned}$ | nA |
| Current Mirror Gain | $\mathrm{I}_{\mathrm{r}}=200 \mu \mathrm{~A}$ | 4 | 0.80 | 0.98 | 1.16 |  |  |  | A/A |
| Current Mirror Gain Drift | $-40^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$ |  |  | $\pm 2.5$ |  |  |  |  | \% |
| Output Current Source Capability <br> Sink Capability | $\begin{aligned} & \left(\mathrm{VOH}_{\mathrm{OH}}=0.4 \mathrm{~V}\right) \\ & \left(\mathrm{VOH}_{\mathrm{OH}}=9.0 \mathrm{~V}\right) \\ & \left(\mathrm{VOL}_{\mathrm{OL}}=0.4 \mathrm{~V}\right) \end{aligned}$ | 5 | $\begin{aligned} & 3.0 \\ & 0.5 \end{aligned}$ | $\begin{gathered} 10 \\ 7.0 \\ 0.87 \end{gathered}$ |  | $\begin{aligned} & 5.0 \\ & 0.5 \end{aligned}$ | $\begin{aligned} & 10 \\ & 1.0 \end{aligned}$ |  | mA |
| Output Voltage <br> High Voltage <br> Low Voltage <br> Undistorted Output Swing | (Inverting Input Driven) <br> (Noninverting Input Driven) $\left(0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+75^{\circ} \mathrm{C}\right)$ | $6$ <br> 7 | 13.5 | $\begin{gathered} 14.2 \\ 0.03 \\ 0.6 \end{gathered}$ | 0.1 | $13.5$ $10$ | $\begin{aligned} & 14.2 \\ & 0.03 \\ & 13.5 \end{aligned}$ | 0.1 | V $V(p-p)$ |
| Input Resistance | (Inverting input only) |  | 0.1 | 1.0 |  | 0.1 | 1.0 |  | MS2 |
| Slew Rate | $\left(C_{L}=100 \mathrm{pF}, \mathrm{R}_{\mathrm{L}}=5.0 \mathrm{k}\right.$ ) |  |  | 0.6 |  |  | 0.6 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Unity Gain Bandwidth |  | 8 |  | 4.0 |  |  | 5.0 |  | MHz |
| Phase Margin |  | 8 |  | 70 |  |  | 70 |  | Degrees |
| Power Supply Rejection | $(\mathrm{f}=100 \mathrm{~Hz}$ ) | 9 |  | 55 |  |  | 55 |  | dB |
| Channel Separation | ( $f=1.0 \mathrm{kHz}$ ) |  |  | 65 |  |  | 65 |  | dB |

NOTES: 1. Open loop voltage gain is defined as the voltage gain from the inverting input to the output.
2. The quiescent current wil! increase approximately 0.3 mA for each noninverting input vihich is grounded. Leaving the noninverting inpui open causes the apparent input bias current to increase slightly ( 100 nA ) at high temperatures.
3. Input bias current can be defined only for the inverting input. The noninverting input is not a true "differential input"-as with a conventional IC operational amplifier. As such this input does not have a requirement for input bias current.
4. Current mirror gain is defined as the current demanded at the inverting input divided by the current into the noninverting input.
5. Sink current is specified for linear operation. When the device is used as a gate or a comparator (non-linear operation), the sink capability of the device is approximately 5.0 milliamperes.
6. When used as a noninverting amplifier, the minimum output voltage is the $V_{B E}$ of the inverting input transistor.
7. Peak-to-peak restrictions are due to the variations of the quiescent dc output voltage in the standard configuration.
8. Bandwidth and phase margin are defined with respect to the voltage gain from the inverting input to the output.
9. Power supply rejection is specified at closed loop unity gain, and therefore indicates the supply rejection of both the biasing circuitry and the feedback amplifier.

## GENERAL DESCRIPTION

The 3403A high performance quad op-amp features improved large signal bandwidth and worst case DC specs equal to or better than the standard 741 type general purpose op-amp. The device uses a newly developed type of ground-sensing differential input stage which provides increased slew rate.

## DESIGN FEATURES

- Class AB Output State; No Crossover Distortion
- Output Voltage Swings to Ground in Single Supply Operations
- High Slew Rate $1.2 \mathrm{~V} / \mu \mathrm{s}$
- Single or Split Supply Operation
- Wide Supply Operation 2.5 V to +36 V or $\pm 1.25 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$
- Pin Compatible with LM324 and 3403
- Low Power Consumption $0.8 \mathrm{~mA} /$ amplifier

SCHEMATIC DIAGRAM (1/4 Shown)


CONNECTION INFORMATION


ABSOLUTE MAXIMUM RATINGS

| Supply Voltage, $\mathrm{V}^{+}$. . . . . . . . . . . . . . . 36 V or $\pm 18 \mathrm{~V}$ | Operating Temperature Range |
| :---: | :---: |
| Differential Input Voltage . . . . . . . . . . . . . . . 36 V | RM3503A . . . . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Input Voltage . . . . . . . . . . . . . . . . -0.3 V to +36 V | RC3403A . . . . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Power Dissipation | RV3403A . . . . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to +850${ }^{\circ} \mathrm{C}$ |
| "DB" package . . . 500 MWV (molded DIP epoxy "B') | Storage Temperature Range . . . . . . . $-65{ }^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
|  | Lead Temperature (Soldering, 60s) . . . . . . . . 3000 |

ELECTRICAL CHARACTERISTICS ( $T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{C C}= \pm 15 \mathrm{~V}$ unless otherwise noted)

| PARAMETER | CONDITIONS | RM3503A |  |  | RC/RV3403A |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}}=0$ |  | 2 | 4 |  | 2 | 5 | mV |
| Input Offset Current | $\mathrm{l}_{\text {in }}$ - or $\mathrm{l}_{\text {in }}$ + |  | $\pm 30$ | $\pm 50$ |  | $\pm 30$ | $\pm 50$ | nA |
| Input Bias Current | $\mathrm{l}_{\text {in- }}$ or $\mathrm{l}_{\text {in }}$ + |  | -100 | -200 |  | -100 | -200 | nA |
| Input Common Mode Voltage Range |  | 0 |  | $\mathrm{V}^{+}-2$ | 0 |  | $\mathrm{V}^{+}-2$ | V |
| Supply Current | $\mathrm{R}_{\mathrm{L}}=\infty$ <br> on all op-amps |  | 3 | 4 |  | 3 | 5 | mA |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}}>2 \mathrm{~K} \Omega \Omega$ | 50 | 100 |  | 25* | 100 |  | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{~K} \Omega$ | $\pm 13$ | $\pm 14$ |  | $\pm 13$ | $\pm 14$ |  | V |
| Common Mode Rejection Ratio | DC | 80 | 90 |  | 80 | 90 |  | dB |
| Channel Separation | $\pm 1 \mathrm{kHz}$ to 20 kHz (in ref) |  | -120 |  |  | -120 |  | dB |
| Output Source Current | $\begin{aligned} & \mathrm{V}_{1 \mathrm{~N}+}=1 \mathrm{~V} \\ & \mathrm{~V} \text { IN- }=0 \mathrm{~V} \end{aligned}$ | 20 | 40 |  | 20 | 40 |  | mA |
| Output sink current |  | 10 | 20 |  | 10 | 20 |  | mA |
| Small signal bandwidth |  |  | 2 |  |  | 2 |  | MHz |
| Slew Rate | $A_{V}=1,-10<V_{i}<+10$ |  | 1.2 |  |  | 1.2 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Distortion (Crossover) | $\mathrm{f}=20 \mathrm{kHz}, \mathrm{VO}=10 \mathrm{~V}_{\mathrm{pp}}$ |  | 1 |  |  | 1 |  | \% |
| Power Bandwidth | $\mathrm{VO}=10 \mathrm{~V} p \mathrm{p}$ |  | 40 |  |  | 40 |  | kHz |
| Power Supply Rejection Ratio |  |  | 20 | 45 |  | 20 | 100 | $\mu \mathrm{V} / \mathrm{V}$ |

## ELECTRICAL CHARACTERISTICS GUARANTEED OVER TEMPERATURE

Range: RM3503A: $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
RC3403A: $\quad 0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
RV3403A: $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$

| PARAMETER | RM3503A |  | RC3403A |  | RV3403A |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN | MAX | MIN | MAX | MIN | MAX |  |
| Input Offset Voltage | - | 6.0 | - | 10.0 | - | 10.0 | mV |
| Input Offset Current | - | 200 | - | 200 | - | 200 | nA |
| Input Bias Current | - | -1500 | - | -800 | - | -1500 | $n \mathrm{~A}$ |
| Large Signal Voltage Gain | 25 | - | 15 | - | 15 | - | $\mathrm{V} / \mathrm{mV}$ |
| Output Voltage Swing | $\pm 10$ | - | $\pm 10$ | - | $\pm 10$ | - | V |

LOW VOLTAGE ELECTRICAL CHARACTERISTICS $\left(\mathrm{V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=\mathrm{GND}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$ unless otherwise noted.)

| PARAMETER | CONDITIONS | RM3503A |  |  | RC/RV3403A |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{RS}=0 \Omega$ |  | 2.0 | 5.0 |  | 2.0 | 10 | mV |
| Input Offset Current | $\mathrm{lin}_{\text {in }}-\mathrm{l}_{\text {in }}+$ |  | 30 | 50 |  | 30 | 50 | nA |
| Input Bias Current | $l_{\text {in }-}+l_{\text {in }}+/ 2$ |  | -100 | -200 |  | -100 | -200 | nA |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{~K} \Omega$ | 20 | 200 |  | 20 | 200 |  | $\mathrm{V} / \mathrm{mW}$ |
| Power Supply Rejection Ratio |  |  |  | 50 |  |  | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Output Voltage Range 1 | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{~K} \Omega$ | 3.5 |  |  | 3.5 |  |  | $V_{p \cdot p}$ |
| Power Supply Current | $\mathrm{R}_{\mathrm{L}}=\infty$, all amplifiers |  | 2.5 | 4.0 |  | 2.5 | 5.0 | mA |
| Channel Separation | $1 \mathrm{KHz} \leqslant \mathrm{f} \leqslant .2 \mathrm{MHz}$ (input referred) |  | -120 |  |  | -120 |  | dB |

1 Output will swing to ground.

## 3403A TYPICAL APPLICATIONS



PRECISION POSITIVE-INPUT, ISOLATED OUTPUT
VOLTAGE FREQUENCY CONVERTER

TYPICAL ELECTRICAL DATA


## GENERAL DESCRIPTION

The RC4131/RM4131 are high performance, high gain, internally compensated operational amplifiers fabricated on a single silicon chip using the planar epitaxial process.
Designed as a pin for pin replacement for the RM709, they are also direct replacements for the 741 and LM107. Relative to these latter units, the RC4131/RM4131 features four times the slew rate, and $1 / 2$ the power dissipation at $\pm 20 \mathrm{~V}$.
High common-mode and differential voltage range, very low input bias current, optimum performance over a very wide range of supply voltage, freedom from "latch-up," and operation over the full military temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ make the RM4131 ideal for use as a voltage follower, comparator, integrator, and summing or general purpose feedback amplifier. The RC4131 operates over a temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- 50nA Maximum Input Bias Current
- 10nA Maximum Input Offset Current
- $2 m V$ Maximum Input Offset Voltage
- 1.1 mA Current Drain at $\pm 20 \mathrm{~V}$
- Offset Voltage Nulling ( $10 \mathrm{k} \Omega$ pot.)
- $2.0 \mathrm{~V} / \mu \mathrm{s}$ Slew Rate
- 4 MHz Unity Gain Bandwidth
- 3 dB Gain. Variation From $\pm 3 \mathrm{~V}$ to $\pm 20 \mathrm{~V}$
- 88 dB Minimum Gain $\pm 3 \mathrm{~V}$ to $\pm 20 \mathrm{~V},-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\begin{array}{r} . R M 4131: \pm 22 \mathrm{~V} \\ \text { RC4131: } \pm 18 \mathrm{~V} \end{array}$ | Operating Temperature Range <br> RM4131 . . . . . . . . . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | . . . . 500 mW | RC4131 . . . . . . . . . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Differential Input Voltage | . $\pm 30 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) . . . . . . . . . 300 ${ }^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | . $\pm 15 \mathrm{~V}$ | Output Short-Circuit Duration (Note 3) . . . . . . Indefinite |
| Storage Temperature Range | $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |  |

ELECTRICAL CHARACTERISTICS $\begin{aligned} & \text { RM4131: } \pm 3 \mathrm{~V}<\mathrm{V}_{\mathrm{S}}< \pm 20 \mathrm{~V},-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}, \text { unless otherwise specified. } \\ & \text { RC4131: } \pm 3 \mathrm{~V}<\mathrm{V}_{\mathrm{S}}< \pm 15 \mathrm{~V}, 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C} \text {, unless otherwise specified. }\end{aligned}$


## NOTES:

1. Rating applies for case temperatures to $+125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+75^{\circ} \mathrm{C}$.
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Short circuit may be to ground or either supply. Rating applies to $+1.25^{\circ} \mathrm{C}$ case temperature of $+75^{\circ} \mathrm{C}$ ambient temperature.
4. RM4131: $\mathrm{V}_{\mathrm{S}}= \pm 3.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}= \pm 1.3 \mathrm{~V} ; \mathrm{V}_{\mathrm{S}}= \pm 20 \mathrm{~V}, \mathrm{~V}_{\mathrm{o}}= \pm 15 \mathrm{~V}$. RC4131: $\mathrm{V}_{\mathrm{S}}= \pm 3 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}= \pm 1.3 \mathrm{~V} ; \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}= \pm 10 \mathrm{~V}$.

TYPICAL ELECTRICAL DATA


TYPICAL APPLICATIONS

Low Drift Sample and Hold


High Impedance Bridge Amplifier


## DESIGN FEATURES

- 10 nA Maximum Input Bias Current
- 2 nA Maximum Input Offset Current
- 3 mV Maximum Input Offset Voltage
- $35 \mu \mathrm{~A}$ Maximum Current Drain at $\pm 20 \mathrm{~V}$
- $20 \mathrm{M} \Omega$ Input Impedance
- $\pm 10 \mathrm{~V}$ Min Into a $5 \mathrm{~K} \Omega$ Load
- 3 dB Gain Variation from $\pm 3 \mathrm{~V}$ to $\pm 20 \mathrm{~V}$
- 94 dB Minimum Gain $\pm 3 \mathrm{~V}$ to $\pm 20 \mathrm{~V},-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$


## GENERAL DESCRIPTION

The RM4132/RC4132 are high performance, high gain, micropower, internally compensated operational amplifiers fabricated on a single silicon chip using the planar epitaxial process.
Designed for applications where power supply current is at a premium (such as in battery operated equipments), 4132 characteristics are very similar to those of the Raytheon 4131 general purpose operational amplifier.

The RM4132 is pin compatible with the 709, 741, and 4131, and features high common mode and differential voltage range, $20 \mathrm{M} \Omega$ input impedance, optimum performance over a wide range of supply voltages, freedom from latch-up, and operation over the full military temperature range. The RC4132 operates over the commercial range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION

| TE (TO-99) <br> Metal Can Package (Top View) | NB <br> Dual In-line Package (Top View) |  |  |
| :---: | :---: | :---: | :---: |
|  |  | PIN | FUNCTION |
|  |  | 1 | BAL |
| (1) (1) |  | 2 | -INPUT |
| (1) (1) | $\square 2 \square$ | 3 | +INPUT |
| $\text { (2) } \boldsymbol{m} \boldsymbol{m} \text { (6) }$ | $-3-4$ | 4 | $\mathrm{V}^{-}$ |
|  |  | 5 | BAL |
| (3) (5) |  | 6 | OUTPUT |
| (4) |  | 7 | $\mathrm{V}^{+}$ |
|  | Order Part Nos.: | 8 | NC |
| Order Part Nos.: <br> RM4132T RC4132T | RC4132NB, RM4132DE, RC4132DE |  |  |
| RM4132T, RC4132T |  |  |  |

## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage <br> Internal Power Dissipation (Note 1) Differential Input Voltage. Input Voltage (Note 2) . <br> Storage Temperature Range. <br> Operating Temperature Range RM4132 <br> RC4132. <br> Lead Temperature (Soldering, 60s) <br> Output Short-Circuit Duration (Note 3) | RM4132: $\pm 22 \mathrm{~V}$ <br> RC4132: $\pm 18 \mathrm{~V}$ 500 mW $\pm 30 \mathrm{~V}$ <br> $\pm 15 \mathrm{~V}$ <br> $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ <br> $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ $300^{\circ} \mathrm{C}$ <br> Indefinite |
| :---: | :---: |

ELECTRICAL CHARACTERISTICS $\left( \pm 3 \mathrm{~V} \leqslant \mathrm{~V}_{\mathrm{S}} \leqslant \pm 20 \mathrm{~V}, \mathrm{RM} 4132:-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C} ; \mathrm{RC} 4132: 0^{\circ} \mathrm{C}\right.$ $\leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C}$ Unless otherwise specified)


## NOTES:

1. Rating applies for case temperatures to $125^{\circ} \mathrm{C}$; derate !inear!y at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures aüve $+75^{\circ} \mathrm{C}$.
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Short-circuit may be to ground or either supply. Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature.
4. $V_{\text {OUT }}=$ guaranteed minimum output swing.

TYPICAL ELECTRICAL DATA


## TYPICAL APPLICATIONS

Inverting Amplifier


## Difference Amplifier



FOR MINIMUM OFFSET ERROR DUE TO INPUT BIAS CURRENT
Inverting Summing Amplifier


## Amplifier for Piezoelectric Transducers



Capacitance Multiplier


Temperature Probe


## GENERAL DESCRIPTION

The RM4136 and RC4136 include four independent high gain operational amplifiers internally compensated and constructed on a single silicon chip using the planar epitaxial processes.

These amplifiers meet or exceed all specifications for 741 type amplifiers. Excellent channel separation allows the use of the 4136 quad amplifier in all 741 operational amplifier applications providing the highest possible packaging density.
The specially designed low noise input transistors allow the 4136 to be used in low noise signal processing applications such as audio preamplifiers and signal conditioners.

## DESIGN FEATURES

- Unity Gain Bandwidth, 3 MHz
- Short-Circuit Protection
- No Frequency Compensation Required
- No Latch-up
- Large Common Mode and Differential Voltage Ranges
- Low Power Consumption
- Parameter Tracking Over Temperature Range
- Gain and Phase Match Between Amplifiers

SCHEMATIC DIAGRAM (1/4 Shown)


## CONNECTION INFORMATION

|  | DC and DB <br> Flatpak |
| :--- | :--- | :--- |
| Dual In-line Packages |  |
| (Top View) |  |

## ABSOLUTE MAXIMUM RATINGS



ELECTRICAL CHARACTERISTICS $\left(V_{C C}= \pm 15 \mathrm{~V}, T_{A}=+25^{\circ} \mathrm{C}\right.$ unless otherwise noted.)

| PARAMETER | CONDITIONS | RM4136 |  |  | RV4136, RC4136 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 0.5 | 4.0 |  | 0.5 | * 6.0 | mV |
| Input Offset Current |  |  | 5.0 | 150 |  | 5.0 | * 200 | nA |
| Input Bias Current |  |  | 40 | 400 |  | 40 | * 500 | nA |
| Input Resistance |  | 0.3 | 5.0 |  | 0.3 | 5.0 |  | MS2 |
| Large-Signal Voltage Gain | $\begin{gathered} R_{L} \geqslant 2 \mathrm{k} \Omega 2 \\ V_{\text {out }}= \pm 10 \mathrm{~V} \end{gathered}$ | 50,000 | 300,000 |  | $20,000$ | 300,000 |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{kS}$ | $\pm 12$ | $\pm 14$ |  | * $\pm 12$ | $\pm 14$ |  | V |
|  | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{kS}$ | $\pm 10$ | $\pm 13$ |  | * $\pm 10$ | $\pm 13$ |  | V |
| Input Voltage Range |  | $\pm 12$ | $\pm 14$ |  | * $\pm 12$ | $\pm 14$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 70 | 100 |  | * 70 | 100 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 10 | 150 |  | 10 | * 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Power Consumption | $\mathrm{R}_{\mathrm{L}}=\infty$, All Outputs |  | 210 | 340 |  | 210 | * 340 | mW |
| Transient Response (unity gain) <br> Risetime <br> Overshoot | $\begin{gathered} V_{\text {in }}=20 \mathrm{mV} \\ R_{\mathrm{L}}=2 \mathrm{kS} \\ C_{L} \leqslant 100 \mathrm{pF} \end{gathered}$ |  | $\begin{gathered} 0.13 \\ 5.0 \end{gathered}$ |  |  | $\begin{gathered} 0.13 \\ 5.0 \end{gathered}$ |  | $\begin{aligned} & \mu \mathrm{S} \\ & \% \end{aligned}$ |
| Unity Gain Bandwidth |  |  | 3.0 |  |  | 3.0 |  | MHz |
| Slew Rate (unity gain) | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  | 1.5 |  |  | 1.0 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Channel Separation (Gain $=100$ ) | $\begin{aligned} & f=10 \mathrm{kHz} \\ & R_{S}=1 \mathrm{k} \Omega \end{aligned}$ |  | 90 |  |  | 90 |  | dB |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{RM} 4136 ; 0{ }^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+70^{\circ} \mathrm{C}$ for RC4136. |  |  |  |  |  |  |  |  |
| Input Offset Voltage | RS $\leqslant 10 \mathrm{k} \Omega$ |  |  | 6.0 |  |  | * 7.5 | mV |
| Input Offset Current |  |  |  | * 500 |  |  | 300 | nA |
| Input Bias Current |  |  |  | * 1500 |  |  | 800 | $n \mathrm{~A}$ |
| Large-Signal Voltage Gain | $\begin{gathered} R_{L} \geqslant 2 \mathrm{k} \Omega \\ \mathrm{~V}_{\text {out }}= \pm 10 \mathrm{~V} \end{gathered}$ | 25,000 |  |  | $15,000$ |  |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ |  |  | * $\pm 10$ |  |  | V |
| Power Consumption | $\mathrm{T}_{\mathrm{A}}=\mathrm{High}$ |  | 180 | 300 |  | 180 | * 300 | mW |
|  | $\mathrm{T}_{\mathrm{A}}$ = Low |  | 240 | 400 |  | 240 | * 400 | mW |

* $=$ RV limits


## NOTES:

1. Rating applies for case temperature to $+25^{\circ} \mathrm{C}$; derate linearly at $6.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+25^{\circ} \mathrm{C}$.
2. For supply voltages less than $\pm 15 \mathrm{~V}$ the absolute maximum input voltage is equal to the supply voltage.
3. Short-circuit may be to ground or one amplifier only. ${ }^{\mathrm{I}} \mathrm{CC}=45 \mathrm{~mA}$ (typical).

TYPICAL ELECTRICAL DATA












## TYPICAL ELECTRICAL DATA



ELECTRICAL CHARACTERISTICS COMPARISON ( $V_{C C}= \pm 15 \mathrm{~V}, T_{A}=+25^{\circ} \mathrm{C}$ )

| PARAMETER |  | RC4136 (typ) | RC741 (typ) | LM324 (typ) | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input Offset Voltage |  | 0.5 | 2.0 | 2 | mV |
| Input Offset Current |  | 5 | 10 | 5 | $n \mathrm{~A}$ |
| Input Bias Current |  | 40 | 80 | 55 | $n \mathrm{~A}$ |
| Input Resistance |  | 5 | 2 |  | $\mathrm{M} \Omega$ |
| Large-Signal Voltage Gain$\left(R_{L}=2 \mathrm{k} \Omega\right)$ |  | 300,000 | 200,000 | 100,000 | V/V |
| Output Voltage Swing$\left(R_{L}=2 \mathrm{k} \Omega\right)$ |  | $\pm 13 \mathrm{~V}$ | $\pm 13 \mathrm{~V}$ | $\begin{gathered} 1+V_{C C}-1.2 \mathrm{VI} \\ \text { to }-V_{C C} \end{gathered}$ | $\overline{\mathrm{V}}$ |
| Input Voltage Range |  | $\pm 14 \mathrm{~V}$ | $\pm 13 \mathrm{~V}$ | $\begin{gathered} \left\|+V_{C C}-1.5 V\right\| \\ \text { to }-V_{C C} \end{gathered}$ | $\overline{\mathrm{V}}$ |
| Common-Mode Rejection Ratio |  | 100 | 90 | 85 | dB |
| Supply Voltage Rejection Ratio |  | 10 | 30 | 10 | $\mu \mathrm{V} / \mathrm{V}$ |
| Transient Response(gain = 1) | Risetime | 0.13 | 0.3 |  | $\mu \mathrm{s}$ |
|  | Overshoot | 5 | 5 |  | \% |
| Unity-Gain Bandwidth |  | 3 | 0.8 | 0.8 | MHz |
| Unity-Gain Slew Rate |  | 1.0 | 0.5 | 0.5 | $\mathrm{V} / \mu \mathrm{s}$ |
| Input Noise Voltage$\left(\mathrm{f}_{0}=1 \mathrm{kHz}\right)$ |  | 10 | 22.5 |  | $n \mathrm{~V} / \sqrt{\mathrm{Hz}}$ |
| Output Short-Circuit Current |  | $\pm 45$ | $\pm 25$ |  | mA |

4136 vs. 741
Although the 324 is an excellent device for single-supply applications where ground-sensing is important, it is a poor substitute for four 741's in split-supply circuits.

The simplified input circuit of the 4136 exhibits much lower noise than that of the 324 and exhibits no crossover distortion as compared with the 324 (see illustration). The 324 shows serious crossover distortion and pulse delay in attempting to handle a large-signal input pulse.


Typical Characteristics Curves Comparison

Input Common Mode
Voltage Range as a
Function of Supply Voltage



## 4136 TYPICAL APPLICATIONS

## Stereo Tone Control



400 Hz Lowpass Butterworth Active Filter


Low Frequency Sine Wave Generator with Quadrature Output


RIAA Preamplifier


Triangular-Wave Generator


## 4136 TYPICAL APPLICATIONS



## Power Amplifier



AC Coupled Inverting Amplifier


DC Coupled 1 kHz Low-Pass Active Filter


Voltage Controlled Oscillator (VCO)


## 4136 TYPICAL APPLICATIONS



## 4136 TYPICAL APPLICATIONS



## DESCRIPTION

The RM4156/RC4156 is a monolithic integrated circuit, consisting of four independent high performance operational amplifiers constructed with the planar epitaxial process.

These amplifiers feature guaranteed A.C. performance which far exceeds that of the 741 type amplifiers. Also featured are excellent input characteristics and guaranteed low noise making this device the optimum choice for audio, active filter and instrumentation applications.

## FEATURES

|  | Typical | Guaranteed |
| :--- | :--- | :--- |
| - Unity Gain Bandwidth | 3.5 MHz | 2.8 MHz |
| - High Slew Rate | $1.6 \mathrm{~V} / \mu \mathrm{S}$ | $1.3 \mathrm{~V} / \mu \mathrm{S}$ |
| - Low Noise Voltage | $1.4 \mu \mathrm{~V}$ | $2.0 \mu \mathrm{~V} \mathrm{RMS}$ |
|  |  |  |
| - Indefinite Short Circuit Protection |  |  |
| - No Crossover Distortion |  |  |
| - Low Input Offset and Bias Parameters |  |  |
| - Internal Compensation |  |  |

SCHEMATIC DIAGRAM (1/4 Shown)


CONNECTION INFORMATION


## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\pm 20 \mathrm{~V}$ | Storage Temperature Range | . . . . | -65 to $+150^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | 880 mW | Operating Temperature Range | RM4156 | -55 to $+125^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ |  | RV4156 | -40 to $+85^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | . $\pm 15 \mathrm{~V}$ |  | RC4156 | 0 to $+70^{\circ} \mathrm{C}$ |
| Output Short Circuit Duration (Note 3) | Indefinite | Lead Soldering Temperature 16 | sec) | - $300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS $V_{C C} \pm 15 V_{A}+25^{\circ} \mathrm{C}$ unless otherwise specified

| PARAMETER | CONDITIONS | RM4156 |  |  | RV4156/RC4156 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ |  | 0.5 | 3.0 |  | 1.0 | 5.0 | mV |
| Input Offset Current |  |  | 15 | 30 |  | 30 | 50 | nA |
| Input Bias Current |  |  | 60 | 200 |  | 60 | 300 | nA |
| Input Resistance |  |  | 0.5 |  |  | 0.5 |  | $\mathrm{M} \Omega$ |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 50,000 | 100,000 |  | 25,000 | 100,000 |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{~K} \Omega$ | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | V |
|  | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega$ | $\pm 10$ | $\pm 13$ |  | $\pm 10$ | $\pm 13$ |  | V |
| Input Voltage Range |  | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | V |
| Output Resistance |  |  | 230 |  |  | 230 |  | $\Omega$ |
| Output Short Circuit Current |  |  | 25 |  |  | 25 |  | mA |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ | 80 |  |  | 80 |  |  | dB |
| Power Supply Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ | 80 |  |  | 80 |  |  | dB |
| Supply Current (all amplifiers) | $R_{L}=\infty$ |  | 4.5 | 5.0 |  | 5.0 | 7.0 | mA |
| Transient Response Rise Time |  |  | 50 |  |  | 75 |  | ns |
| Overshoot |  |  | 25\% |  |  | 25\% |  | \% |
|  |  | 1.3 | 1.6 |  | 1.3 | 1.6 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Unity Gain Bandwidth |  | 2.8 | 3.5 |  | 2.8 | 3.5 |  | MHz |
| Phase Margin | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{~K} \Omega \mathrm{R}_{\mathrm{C}}=50 \mathrm{pF}$ |  | 50 |  |  | 50 |  | degrees |
| Full Power Bandwidth | $\mathrm{V}_{0}=20 \mathrm{~V}$-p | 20 | 25 |  | 20 | 25 |  | kHz |
| Input Noise Voltage | $\mathrm{f}=20 \mathrm{~Hz}$ to 20 kHz |  | 1.4 | 2.0 |  | 1.4 | 2.0 | $\mu \mathrm{V}$ RMS |
| Input Noise Current | $\mathrm{f}=20 \mathrm{~Hz}$ to 20 kHz |  | 15 |  |  | 15 |  | pA RMS |
| Channel Separation |  |  | -108 |  |  | -108 |  | dB |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{RM} 4156,-40^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$ for RV4156, $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C}$ for RC4156. |  |  |  |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ |  |  | 5.0 |  |  | 6.5 | mV |
| Input Offset Current |  |  |  | 75 |  |  | 100 | nA |
| Input Bias Current |  |  |  | 325 |  |  | 400 | nA |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 25,000 |  |  | 15,000 |  |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega$ | $\pm 10$ |  |  | $\pm 10$ |  |  | V |
| Supply Current |  |  | 10 |  |  | 10 |  | mA. |
| Average Offset Voltage Drift |  |  | 5 |  |  | 5 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |

[^3]
## 4156

## TYPICAL PERFORMANCE DATA




Small Signal Bandwidth and Phase Margin vs. Load Capacitance


Input Currents vs. Temperature


Output Voltage Swing vs. Frequency


Common Mode Rejection Ratio vs. Temperature


Output Voltage Swing vs. Load Resistance

## AVAILABLE TYPES

| Part Number | Package | Operating Temperature |
| :--- | :--- | :---: |
| RM4156DC | Ceramic | -55 to $+125^{\circ} \mathrm{C}$ |
| RV4156DB | Plastic | -40 to $+85^{\circ} \mathrm{C}$ |
| RV4156DC | Ceramic | -40 to $+85^{\circ} \mathrm{C}$ |
| RC4156DC | Ceramic | 0 to $+70^{\circ} \mathrm{C}$ |
| RC4156DB | Plastic | 0 to $+70^{\circ} \mathrm{C}$ |

HIGH RELIABILITY OPTIONS

| Part Type | Added Screening | Order Part No. |
| :---: | :--- | :--- |
| RM4156DC | With MIL-STD-883 <br> Class B processing | RM4156DC3 |
| RV4156DC <br> RC4156DC | With A+3 processing* <br> including burn-in and <br> tightened AQL | RV4156DC3 <br> RC4156DC3 |
| RV4156DB <br> RC4156DB | With A+2 processing* <br> including "Hot Rail" <br> testing, burn-in, temp <br> cycle and tightened <br> AQL | RV4156DB2 <br> RC4156DB2 |
|  | With A+1 processing* <br> including "Hot Rail" <br> testing, temp cycle <br> and tightened AQL | RV4156DB1 <br> RC4156DB1 |

* Full description contained in the A+ bulletin available at your local Raytheon Sales Office.


## APPLICATIONS

The 4156 Quad Operational Amplifier can be used in almost any 741 application and will provide superior performance. The higher unity-gain bandwidth and slew rate make it ideal for applications requiring good frequency response, such as. active filter circuits, oscillators and audio amplifiers.

The following applications have been selected to illustrate the advantages of using the Raytheon 4156 Quad Operational Amplifier.

## VERSATILE TRIANGLE-AND-SQUARE WAVE GENERATOR

This circuit generates a precise triangle-wave with independently adjustable frequency, offset, and amplitude. A square-wave is also available from a separate output. The circuit exhibits excellent stability in both amplitude and frequency when using the 4156 quad op amp. See Figure 1.


Figure 1. Triangle-and-Square Wave Generator

Amplifier A1 acts as a comparator and will swing between the positive and negative limits, typically +14 V and -13.5 V . The square-wave from amplifier A1 is converted to a triangle-wave by amplifier A2. Amplitude of $\mathrm{V}_{2}$ is adjusted by varying $R_{1}$. For best operation, it is recommended that $R_{1}$ and $V_{R}$ be set to obtain a triangle-wave at $V_{2}$ with $\pm 12 \mathrm{~V}$ amplitude. This will then allow A 3 and A 4 to be used for independent adjustment of output-offset and amplitude over a wide range.

The output frequency can be easily calculated. The switching transitions occur at:

$$
\frac{R_{1}}{R_{1}+R_{2}} \quad V_{2}+\frac{R_{2}}{R_{1}+R_{2}} \quad V_{1 H}=V_{R}
$$

and

$$
\frac{R_{1}}{R_{1}+R_{2}} V_{2}+\frac{R_{2}}{R_{1}+R_{2}} \quad V_{1 L}=V_{R}
$$

where $\mathrm{V}_{1 \mathrm{H}}$ is the positive saturation level and $\mathrm{V}_{1 \mathrm{~L}}$ is the negative saturation level. For a $\pm 12 \mathrm{~V}$ triangle-wave at output of $\mathrm{A} 2, \mathrm{~V}_{\mathrm{R}}$ will need to be approximately 0.12 V and $R_{2} / R_{1}=1.87$.

Amplifiers A3 and A4 are used to independently adjust output offset and amplitude. The output $\mathrm{V}_{4}$ will be:

$$
v_{4}=-\frac{R_{4}}{R_{3}} v_{2}+v_{3}
$$

An asymmetric triangle-wave is needed in some applications. Adding diodes as shown by the dashed lines is a way to vary the positive and negative slopes independently.

Frequency range can be very wide and the circuit will function very well up to about 10 kHz . Transition time for the square-wave at $\mathrm{V}_{1}$ is less than $21 \mu \mathrm{sec}$ when using the 4156.

## ACTIVE FILTERS

The introduction of low-cost quad op amps has had a strong impact on active filter design. The complex multiplefeedback, single-op-amp filter circuits have been rendered obsolete for most applications. State-variable active-filter circuits using three to four op amps per section offer many advantages over the single-op-amp circuits. They are relatively insensitive to the passive-component tolerances and variations. The $Q$, gain, and natural frequency can be independently adjusted. Hybrid construction is very practical because resistor and capacitor values are relatively low and the filter parameters are determined by resistance ratios rather than by single resistors. A generalized circuit diagram of the 2-pole state-variable active filter is shown in Figure 2. The particular input connections and componentvalues can be calculated for specific applications. An important feature of the state-variable filter is that it can be inverting or noninverting and can simultaneously provide three outputs: lowpass, bandpass, and highpass. A notch filter can be realized by adding one summing op amp.


Figure 2. Generalized State-Variable Configuration for Active Filter

The Raytheon 4156 was designed and characterized for use in active filter circuits. Frequency response is fully specified with minimum values for unity-gain bandwidth, slew-rate, and full-power response. Maximum noise is specified. Output swing is excellent with no distortion or clipping. The Raytheon 4156 provides full, undistorted response up to 20 kHz and is ideal for use in highperformance audio and telecommunication equipment.

In the state-variable filter circuit, one amplifier performs a summing function and the other two act as integrators. The choice of passive component values is arbitrary, but must be consistent with the amplifier operating range and input signal characteristics. The values shown for C1, C2, R4, R5 and R6 are arbitrary. Pre-selecting their values will simplify the filter tuning procedures, but other values can be used if necessary.

The generalized transfer function for the state-variable active filter is:

$$
T(s)=\frac{a_{2} s^{2}+a_{1} s+a_{0}}{s^{2}+b_{1} s+b_{0}}
$$

Filter response is conventionally described in terms of a natural frequency $\omega_{0}$ in radians $/ \mathrm{sec}$, and Q , the quality of the complex pole pair. The filter parameters $\omega_{0}$ and Q relate to the coefficients in $T(s)$ as:

$$
\omega_{0}=\sqrt{b_{0}} \text { and } Q=\frac{\omega_{0}}{b_{1}}
$$

The input configuration determines the polarity (inverting or noninverting), and the output selection determines the type of filter response (lowpass, bandpass, or highpass).


Figure 3. Bandpass Active Filter

Notch and all-pass configurations can be implemented by adding another summing amplifier.

Bandpass filters are of particular importance in audio and telecommunication equipment. A design approach to bandpass filters will be shown as an example of the state-variable configuration.

## DESIGN EXAMPLE - BANDPASS FILTER

In this example, the input signal is applied through $\mathrm{R}_{3}$ to the inverting input of the summing amplifier and the output is taken from the first integrator ( $\mathrm{V}_{\mathrm{BP}}$ ). The summing amplifier will maintain equal voltage at the inverting and noninverting inputs, (see equation below).

$$
\frac{\frac{R_{3} R_{5}}{R_{3}+R_{5}}}{R_{4}+\frac{R_{3} R_{5}}{R_{3}+R_{5}}} v_{H P}(s)+\frac{\frac{R_{3} R_{4}}{R_{3}+R_{4}}}{R_{5}+\frac{R_{3} R_{4}}{R_{3}+R_{4}}} V_{L P}(s)+-
$$

These equations can be combined to obtain the transfer function:

$$
V_{B P}(s)=-\frac{1}{R_{1} C_{1} S} V_{H P}(s) \text { and } V_{L P}(s)=-\frac{1}{R_{2} C_{2} S} V_{B P}(s)
$$

$$
\frac{V_{B P}(s)}{V_{i n}(s)}=\frac{\frac{R_{4}}{R_{3}} \frac{1}{R_{1} C_{1}} s}{s^{2}+\frac{R_{7}}{R_{6}+R_{7}}\left(1+\frac{R_{4}}{R_{5}}+\frac{R_{4}}{R_{3}}\right)\left(\frac{1}{R_{1} C_{1}}\right) s+\frac{R_{4}}{R_{5}} \frac{1}{R_{1} C_{1} R_{2} C_{2}}}
$$

Defining $1 / R_{1} C_{1}$ as $\omega_{1}, 1 / R_{2} C_{2}$ as $\omega_{2}$, and substituting in the assigned values for $R_{4}, R_{5}$, and $R_{6}$, then the transfer function simplifies to:


This is now in a convenient form to look at the centerfrequency $\omega_{0}$ and filter Q .

$$
\begin{aligned}
\omega_{0} & =\sqrt{0.1 \omega_{1} \omega_{2}} \\
& =10^{-9} \sqrt{0.1 R_{1} R_{2}}
\end{aligned} \text { and } \quad Q=\left[\begin{array}{l}
1+\frac{R_{7}}{1.1+\frac{10^{4}}{R_{3}}}
\end{array}\right] \omega_{0}
$$

The frequency response for various values of $Q$ are shown in Figure 4.


Figure 4. Bandpass Transfer Characteristics Normalized for Unity Gain and Frequency

These equations suggest a tuning sequence where $\omega_{0}$ is first trimmed via $R_{1}$ or $R_{2}$, then $Q$ is trimmed by varying $R_{7}$ and/or $R_{3}$. An important advantage of the state-variable bandpass filter is that Q can be varied without affecting center frequency $\omega_{0}$.

This analysis has assumed ideal op amps operating within their linear range, which is a valid design approach for a reasonable range of $\omega_{0}$ and $Q$. At extremes of $\omega_{0}$ and at high values of $Q$, the op amp parameters become significant. A rigorous analysis is very complex, but some factors are particularly important in designing active filters:

1. The passive component values should be chosen such that all op amps are operating within their linear region for the anticipated range of input signals. Slew rate, output current rating, and common-mode input range must be considered. For the integrators, the current through the feedback capacitor ( $1=C \mathrm{dV} / \mathrm{dt}$ ) should be included in the output current computations.
2. From the equation for $Q$, it would seem that infinite $Q$ could be obtained by making $R_{7}$ zero. But as $R_{7}$ is made small, the $Q$ becomes limited by the op amp gain at the frequency of interest. The effective closed-loop gain is being increased directly as $R_{7}$ is made smaller, and the ratio of open-loop gain to closed-loop gain is becoming less. The gain and phase error of the filter at high Q is very dependent on the op-amp open-loop gain at $\omega_{0}$.
3. The attenuation at extremes of frequency is limited by the op amp gain and unity-gain bandwidth. For integrators, the finite open-loop op-amp gain limits the accuracy at the low-end. The open-loop roll-off of gain limits the filter attenuation at high frequency.

The Raytheon 4156 Quad Operational Amplifier has much better frequency response than a conventional 741 circuit and is ideal for active filter use. Natural frequencies of up to 10 kHz are readily achieved and up to 20 kHz is practical for some configurations. Q can range up to 50 with very good accuracy and up to 500 with reasonable response. The extra gain of the 4156 at high frequencies gives the Raytheon quad op amp an extra margin of performance in active-filter circuits.

## DESCRIPTION

The RM4157/RC4157 is a monolithic integrated circuit, consisting of four independent high performance operational amplifiers constructed with the planar epitaxial process.

These amplifiers feature guaranteed A.C. performance which far exceeds that of the LM149 type amplifiers. Also featured are excellent input characteristics and guaranteed low noise making this device the optimum choice for audio, active filter and instrumentation applications.

## FEATURES

|  | Typical | Guaranteed |
| :--- | :---: | :---: |
| - Gain Bandwidth Product $\left(\mathrm{Al}_{\mathrm{V}} \geqslant 5\right)$ | 19 MHz | 15 MHz |
| - High Slew Rate $\left(\mathrm{A}_{\mathrm{v}}=5\right)$ | 8 | $6.5 \mathrm{~V} / \mu \mathrm{s}$ |
| - Low Noise Voltage | $1.4 \mu \mathrm{~V}$ | $2.0 \mu \mathrm{~V} \mathrm{RMS}$ |
| - Indefinite Short Circuit Protection |  |  |
| - No Crossover Distortion |  |  |
| - Low Input Offset and Blas Parameters |  |  |
| - Internal Compensation |  |  |

SCHEMATIC DIAGRAM (1/4 Shown)


## CONNECTION INFORMATION



## Quad High Speed Decompensated Operational Amplifier

|  | Quad Wide Band Decompensated ( $\mathrm{N}_{\mathbf{v} \text { min }}=5$ ) Operational Amplifier |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Supply Voltage | . $\pm 20 \mathrm{~V}$ | Storage Temperature Range |  | -65 to $+150^{\circ} \mathrm{C}$ |
| Internal Power Dissipation (Note 1) | 880 mW | Operating Temperature Range | RM4157 | -55 to $+125^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ |  | V4157 | -40 to $+85^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | $\pm 15$ |  | C4157 | 0 to $+70^{\circ} \mathrm{C}$ |
| Output Short Circuit Duration (Note 3) | ndef | g Temperature |  | $300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS
$V_{C C} \pm 15 \mathrm{~V} \mathrm{~T}_{\mathrm{A}}+25^{\circ} \mathrm{C}$ unless otherwise specified

| PARAMETER | CONDITIONS | RM4157 |  |  | - RV4157/RC4157 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ |  | 0.5 | 3.0 |  | - 1.0 | 5.0 | mV |
| Input Offset Current |  |  | 15 | 30 |  | 30 | 50 | nA |
| Input Bias Current |  |  | 60 | 200 |  | 60 | 300 | nA |
| Input Resistance |  |  | 0.5 |  | - | 0.5 |  | $\mathrm{M} \Omega$ |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 50,000 | 100,000 | 4 | 25,000 | 100,000 |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{~K} \Omega$ | $\pm 12$ | $\pm 14$ | , | $\pm 12$ | $\pm 14$ |  | V |
|  | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega$ | $\pm 10$ | $\pm 13$ | + | $\pm 10$ | $\pm 13$ |  | V |
| Input Voltage Range |  | $\pm 12$ | $\pm 14$ |  | $\pm 12$ | $\pm 14$ |  | V |
| Output Resistance |  | 4 | - 230 |  |  | 230 |  | $\Omega$ |
| Output Short Circuit Current |  | - | - 25 |  |  | 25 |  | mA |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ | 80 | - |  | 80 |  |  | dB |
| Power Supply Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ | 80 |  |  | 80 |  |  | dB |
| Supply Current (all amplifiers) | $\mathrm{R}_{\mathrm{L}}=\infty \quad \sqrt{\text { a }}$ |  | 4.5 | 5.0 |  | 5.0 | 7.0 | mA |
| Transient Response <br> Rise Time <br> Overshoot <br> Slew Rate | $A_{V}=5$ | - | 50 |  |  | 60 |  | ns |
|  | $A_{V}=5$ | . | 25\% |  |  | 25\% |  | \% |
|  | $A_{V}=5$ | - 6.5 | 8 |  | 6.5 | 8 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Gain Bandwidth Product | , | 15 | 19 |  | 15 | 19 |  | MHz |
| Phase Margin ( $\mathrm{A}_{V}=5$ ) | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \mathrm{R}_{\mathrm{C}}=50 \mathrm{pF}$ |  | 50 |  |  | 50 |  | degrees |
| Full Power Bandwidth | $\mathrm{V}_{0}=20 \mathrm{Vp-p}$ | 100 | 125 |  | 100 | 125 |  | kHz |
| Input Noise Voltage | f = 20 Hz to 20 kHz |  | 1.4 | 2.0 |  | 1.4 | 2.0 | $\mu \mathrm{V}$ RMS |
| Input Noise Current | $\mathrm{f}=20 \mathrm{~Hz}$ to 20 kHz |  | 15 |  |  | 15 |  | pA RMS |
| Channel Separation | 2 |  | -108 |  |  | -108 |  | dB |

The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for RM4157, $-40^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$ for RV4157, $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+70^{\circ} \mathrm{C}$ for RC4157.

| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ |  | 5.0 |  |  | 6.5 | mV |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Input Offset Current |  |  |  | 75 |  |  | 100 | nA |
| Input Bias Current |  |  |  | 325 |  |  | 400 | nA |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 25,000 |  |  | 15,000 |  |  | $\mathrm{~V} / \mathrm{V}$ |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega$ | $\pm 10$ |  |  | $\pm 10$ |  |  | V |
| Supply Current |  |  | 10 |  |  | 10 |  | mA |
| Average Offset Voltage Drift |  |  | 5 |  |  | 5 |  | $\mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |

Notes: 1. Rating applies for case temperature of $+25^{\circ} \mathrm{C}$ maximum; derate linearity at $6.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for temperatures above $+25^{\circ} \mathrm{C}$.
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Short circuit to ground on one amplifier only.

## GENERAL DESCRIPTION

The RM4531 and RC4531 are high slew rate operational amplifiers intended for applications requiring slew rates up to $30 \mathrm{~V} /$ $\mu \mathrm{s}$ while keeping the DC performance of the 741.

The RM4531 military version operates over a temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The RC4531 operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

High slew rates are achieved through use of an improved input stage which tends to retain small signal characteristics when subjected to large differential input signals. Advanced integrated circuit layout techniques are used to eliminate thermal feedback. The RM4531 and RC4531 feature offset null capability, high gain, and each can be compensated with an external 100pF capacitor connected between the output and compensation terminals.

## DESIGN FEATURES

- Slew Rate $35 \mathrm{~V} / \mu \mathrm{s}$
- Small Signal Bandwidth 1 MHz
- Large Signal Bandwidth 500 kHz
- Supply Voltage $\pm 6 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$
- Pin-for-Pin Replacement for 709, LM101A, 741
- Low Drift Offset-Null Circuitry
- Compensated with Single Capacitor


## SCHEMATIC DIAGRAM



CONNECTION INFORMATION

| TE (TO-99) <br> Metal Can Package <br> (Top View) | DC <br> Dual In-line Package (Top View) | NB Dual In-line Plastic Package (Top View) |
| :---: | :---: | :---: |
| Order Part Nos.: <br> RM4531T, RC4531T | Order Part Nos.: <br> RM4531DC, RC4531DC | Order Part No.: <br> RC4531NB |

## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\begin{aligned} & \text { RM4531: } \pm 22 \mathrm{~V} \\ & \text { RC4531: } \pm 18 \mathrm{~V} \end{aligned}$ | Operating Temperature Range <br> RM4531 . . . . . . . . . . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to +1250 C |
| :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | 500 mW | RC4531 . . . . . . . . . . . . . . . . . . . 000 C to $+70{ }^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 15 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) . . . . . . . . . 3000 ${ }^{\text {C }}$ |
| Input Voltage (Note 2) | $-12.5 \mathrm{~V},+15 \mathrm{~V}$ | Output Short-Circuit Duration (Note 3) . . . . Indefinite |
| Storage Temperature Range | $65^{\circ} \mathrm{C}$ to $+150{ }^{\circ} \mathrm{C}$ |  |

ELECTRICAL CHARACTERISTICS $\left(V_{S}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM4531 |  |  | RC4531 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 2.0 | 5.0 |  | 2.0 | 6.0 | mV |
| Input Offset Current |  |  | 30 | 200 |  | 50 | 200 | nA |
| Input Bias Current |  |  | 300 | 500 |  | 400 | 1500 | nA |
| Input Resistance |  | 0.3 | 20 |  | 0.3 | 20 |  | $\mathrm{M} \Omega$ |
| Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{S}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {out }}= \pm 10 \mathrm{~V}$ | 50,000 | 100,000 |  | 20,000 | 60,000 |  | V/V |
| Input Votlage Range (Note 2) |  | $\pm 10$ |  |  | $\pm 10$ |  |  | V |
| Common Mode Rejection Ratio | $\mathrm{RS}^{5} \leqslant 10 \mathrm{k} \Omega$ | 70 | 100 |  | 70 | 100 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 10 | 150 |  | 10 | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Output Resistance |  |  | 75 |  |  | 75 |  | $\Omega$ |
| Supply Current |  |  | 5.5 | 7.0 |  | 5.5 | 10 | mA |
| Power Consumption |  |  | 165 | 210 |  | 165 | 300 | mW |
| Setting Time, 1\% | $A_{V}=+1, V_{\text {IN }}= \pm 10 \mathrm{~V}$ |  | 1.5 |  |  | 1.5 |  | $\mu \mathrm{s}$ |
| Setting Time, .01\% | $A_{V}=+1, V_{I N}= \pm 10 \mathrm{~V}$ |  | 2.5 |  |  | 2.5 |  | $\mu \mathrm{s}$ |
| Large Signal Overshoot | $A_{V}=+1, V_{\text {IN }}= \pm 10 \mathrm{~V}$ |  | 2.0 |  |  | 2.0 |  | \% |
| Small Signal Risetime | $A_{V}=+1, V_{I N}=400 \mathrm{mV}$ |  | 300 |  |  | 300 |  | ns |
| Small Signal Overshoot | $A_{V}=+1, V_{\text {IN }}=400 \mathrm{mV}$ |  | 5.0 |  |  | 5.0 |  | \% |
| Slew Rate | $A_{V}=100$ |  | 35 |  |  | 35 |  | $\mathrm{V} / \mu \mathrm{s}$ |
|  | $A_{V}=10$ |  | 35 |  |  | 35 |  | $\mathrm{V} / \mu \mathrm{s}$ |
|  | $A V=1$ (non-inv.) |  | 30 |  |  | 30 |  | $\mathrm{V} / \mu \mathrm{s}$ |
|  | $A V=1$ (inv.) |  | 35 |  |  | 35 |  | $\mathrm{V} / \mu \mathrm{s}$ |

The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{RM} 4531 ; 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+70^{\circ} \mathrm{C}$ for RC 4531 .

| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 6.0 |  |  | 7.5 | mV |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: |
| Input Offset Current | $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\min }$ |  |  | 500 |  |  | 300 | nA |
|  | $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\max }$ |  |  | 200 |  |  | 200 | nA |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\min }$ |  |  | 1.5 |  |  | 2.0 | $\mu \mathrm{~A}$ |
|  | $\mathrm{~T}_{\mathrm{A}}=\mathrm{T}_{\max }$ |  |  | 0.5 |  |  | 1.5 | $\mu \mathrm{~A}$ |
| Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {out }}= \pm 10 \mathrm{~V}$ | 25,000 |  |  | 15,000 |  |  |  |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ | $\pm 13$ |  | $\pm 10$ | $\pm 13$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 70 | 90 |  |  |  |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 10 | 150 |  |  |  | $\mu \mathrm{~V} / \mathrm{V}$ |
| Supply Current | $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\max }$ |  | 4.5 | 5.5 |  | 4.5 | 5.5 | mA |

## NOTES:

1. Rating applies for case temperatures to $+125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+75^{\circ} \mathrm{C}$ for RM 4531 .
 input voltage decreased by 1 volt for every 1 volt decrease in the negative supply voltage.
2. Short-circuit may be to ground or to either supply Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature for RM4531.

## GENERAL DESCRIPTION

The 4558 integrated circuit is a dual high gain operational amplifier internally compensated and constructed on a single silicon chip using the planar epitaxial process.

Combining the features of the 741 with the close parameter matching and tracking of a dual device on a monolithic chip results in unique performance characteristics. Excellent channel separation allows the use of the dual device in single 741 operational amplifier applications providing the highest possible packaging density. It is especially well suited for applications in differential-in, differential-out as well as in potentiometric amplifiers and where gain and phase matched channels are mandatory.

## DESIGN FEATURES

- 2.5 MHz Unity Gain Bandwidth Guaranteed
- Supply Voltage $\pm 22 \mathrm{~V}$ for RM4558 and $\pm 15 \mathrm{~V}$ for RC4558
- Short-Circuit Protection
- No Frequency Compensation Required
- No Latch-Up
- Large Common-Mode and Differential Voltage Ranges
- Low Power Consumption
- Parameter Tracking Over Temperature Range
- Gain and Phase Match Between Amplifiers

SCHEMATIC DIAGRAM (1/2 Shown)


## CONNECTION INFORMATION



Order Part Nos.:
RC4558T, RM4558T

## DE and NB <br> Dual In-line Packages <br> (Top View)



Order Part Nos.:
RC4558NB, RV4558NB
RC4558DE, RV4558DE RM4558DE

## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\begin{aligned} & \text { RM4558: } \pm 22 \mathrm{~V} \\ & \text { RC4558: } \pm 18 \mathrm{~V} \end{aligned}$ |  |
| :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | 500 mW | RC4558: $0^{\circ} \mathrm{C}$ to $+70{ }^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) . . . . . . . . . . 300º |
| Input Voltage (Note 2) | $\pm 15 \mathrm{~V}$ | Output Short-Circuit Duration (Note 3) . . . . . . Indefinite |
| Storage Temperature Range | ${ }^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |  |

ELECTRICAL CHARACTERISTICS $\left(V_{C C}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM4558 |  |  | RV/RC4558 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 1.0 | 5.0 |  | 2.0 | 6.0 | mV |
| Input Offset Current |  |  | 5.0 | 200 |  | 30 | 200 | nA |
| Input Bias Current |  |  | 40 | 500 |  | 200 | 500 | $n \mathrm{~A}$ |
| Input Resistance |  | 0.3 | 1.0 |  | 0.3 | 1.0 |  | $\mathrm{M} \Omega$ |
| Large-Signal Voltage Gain | $\begin{gathered} R_{L} \geqslant 2 \mathrm{k} \Omega \\ V_{\text {out }}= \pm 10 \mathrm{~V} \end{gathered}$ | 50,000 | 300,000 |  | 20,000 | 300,000 |  |  |
| Output Voltage Swing | $\begin{gathered} R_{L} \geqslant 10 k \Omega \\ R_{L} \geqslant 2 k \Omega \end{gathered}$ | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \pm 12 \\ & \pm 10 \end{aligned}$ | $\begin{aligned} & \pm 14 \\ & \pm 13 \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Input Voltage Range |  | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{kS}$ | 70 | 100 |  | 70 | 100 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{RS}^{5} \leqslant 10 \mathrm{k} \Omega$ |  | 10 | 150 |  | 10 | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Power Consumption (All Amplifiers) | $\mathrm{R}_{\mathrm{L}}=\infty$ |  | 100 | 170 |  | 100 | 170 | mW |
| Transient Response (unity gain) <br> Risetime <br> Overshoot | $\begin{gathered} V_{I N}=20 \mathrm{mV} \\ R_{L}=2 \mathrm{k} \Omega \\ C_{L} \leqslant 100 \mathrm{pF} \end{gathered}$ |  | $\begin{gathered} 0.3 \\ 15.0 \end{gathered}$ |  |  | $\begin{gathered} 0.3 \\ 15.0 \\ \hline \end{gathered}$ |  | $\begin{aligned} & \mu \mathrm{s} \\ & \% \\ & \hline \end{aligned}$ |
| Slew Rate (unity gain) | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  | 0.5 |  |  | 0.5 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Channel Separation (Gain $=100$ ) | $\begin{aligned} & f=10 \mathrm{kHz} \\ & \mathrm{RS}=1 \mathrm{k} \Omega \end{aligned}$ |  | 90 |  |  | 90 |  | dB |
| Unity Gain Bandwidth (Gain = 1) |  | 2.5 | 3.0 |  | 2.0 | 3.0 |  | MHz |

The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{RM} 4558 ; 0^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+70^{\circ} \mathrm{C}$ for RC4558;
$-40^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$ for RV4558

| Input Offset Voltage | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  |  | 6.0 |  |  | 7.5 | mV |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Offset Current |  |  |  | 500 |  |  | $300 / 500^{*}$ | nA |
| Input Bias Current |  |  |  | 1500 |  |  | $800 / 1500$ | nA |
| Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ <br>  <br>  <br> $\mathrm{V}_{\mathrm{out}}= \pm 10 \mathrm{~V}$ | 25,000 |  |  | 15,000 |  |  |  |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ |  |  | $\pm 10$ |  |  | V |
| Power Consumption | $\mathrm{VS}= \pm 15 \mathrm{~V}$ |  |  |  |  |  |  |  |
|  | $\mathrm{TA}=+1250 \mathrm{C}$ |  | 90 | 150 |  | 90 | 150 | mW |

MATCHING CHARACTERISTICS ( $V_{C C}= \pm 15 \mathrm{~V}, T_{A}=25^{\circ} \mathrm{C}$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM4558 | RC4558 | TYP |
| :--- | :---: | :---: | :---: | :---: |

NOTE 1: Rating applies for case temperatures to $125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+75^{\circ} \mathrm{C}$ for RM 4558 .
NOTE 2: For supply voltages less than +15 V , the absolute maximum input voltage is equal to the supply voltage.
NOTE 3: Short circuit may be to ground on one amp only. Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature for RC4558 and to $+85^{\circ} \mathrm{C}$ ambient temperature for RV4558.

TYPICAL ELECTRICAL DATA


Open Loop Voltage Gain as a
Function of Frequency


Typical Output Voltage as a
Function of Supply Voltage


Quiesent Current as a Function of Supply Voltage



Open Loop Gain as a


Output Voltage Swing as a



Common Mode Range as a Function of Supply Voltage


Power Consumption as a
Function of Ambient Temperature


Output Voltage Swing as a
Function of Frequency



## TYPICAL ELECTRICAL DATA




## GENERAL DESCRIPTION

The 4559 integrated circuit is a dual high performance operational amplifier internally compensated and constructed on a single silicon chip using the planar epitaxial process.
These amplifiers feature guaranteed AC performance which far exceeds that of the 741-type amplifiers. The specially designed low-noise input transistors allow the 4559 to be used in low-noise signal processing applications such as audio pre amplifiers and signal conditioners.

The 4559 also has more output drive than 741 -type amplifiers and can be used to drive a 600 ohm load.

## FEATURES

|  | Typical | Guaranteed |
| :---: | :---: | :---: |
| Unity Gain Bandwidth | 4.0 MHz | 3.0 MHz |
| Slew Rate | $2.0 \mathrm{~V} / \mu \mathrm{sec}$ | $1.5 \mathrm{~V} / \mu \mathrm{sec}$ |
| Low Noise Voltage | $1.4 \mu \mathrm{~V}_{\text {RMS }}$ | $2.0 \mu \mathrm{~V}_{\mathrm{RMS}}$ |
| - Supply Voltage $\pm 22 \mathrm{~V}$ for RM4559 and $\pm 18 \mathrm{~V}$ for RC4559 |  |  |
| - No Frequency Compensation Required |  |  |
| - No Latch Up |  |  |
| Large Common Mode and Differential Voltage Ranges |  |  |
| - Low Power Consumption |  |  |
| Parametric Tracking Over Temperature Range |  |  |
| Gain and Phase Match Between Amplifiers |  |  |

- Supply Voltage $\pm 22 \mathrm{~V}$ for RM4559 and $\pm 18 \mathrm{~V}$ for RC4559
- No Frequency Compensation Required
- No Latch Up
- Large Common Mode and Differential Voltage Ranges
- Low Power Consumption
- Parametric Tracking Over Temperature Range
- Gain and Phase Match Between Amplifiers


## SCHEMATIC DIAGRAM (1/2 Shown)



## CONNECTION INFORMATION

TE (TO-99)
Metal Can Package
(Top View)

## Dual High Performance Operational Amplifier

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage . . . . . . . . . . . . . . . . . RM4559: $\pm 22 \mathrm{~V}$
RC4559: $\pm 18 \mathrm{~V}$
Internal Power Dissipation (Note 1) . . . . . . . . 500 mW
Differential Input Voltage. . . . . . . . . . . . . $\pm 30 \mathrm{~V}$
Input Voltage (Note 2). . . . . . . . . . . . . $\pm 15 \mathrm{~V}$
Storage Temperature Range. . . . . . . . $-655^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Temperature Range
RM4559 ................... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
RV4559 .................. $40^{\circ} \mathrm{C}$ to $+85{ }^{\circ} \mathrm{C}$
RC4559 ....................... $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 60 sec ) ......... $300^{\circ} \mathrm{C}$
Output Short-Circuit Duration (Note 3). . . . . . . Indefinite

ELECTRICAL CHARACTERISTICS ( $T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}= \pm 15 \mathrm{~V}$ unless otherwise specified.)

|  |  | RM4559 |  |  | RV/RC4559 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PARAMETER | CONDITIONS | MIN | TYP | MAX | MIN | TYP | MAX | UNITS |
| Input Offset Voltage | $\mathrm{RS}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 1.0 | 5.0 |  | 2.0 | 6.0 | mV |
| Input Offset Current |  |  | 5 | 100 |  | 5 | 100 | nA |
| Input Bias Current |  |  | 40 | 250 |  | 40 | 250 | nA |
| Input Resistance |  | 0.3 | 1.0 |  | 0.3 | 1.0 |  | $\mathrm{M} \Omega$ |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {out }}= \pm 10 \mathrm{~V}$ | 50,000 | 300,000 |  | 20,000 | 300,000 |  | V/V |
| Output Voltage Swing | $\begin{aligned} & R_{L} \geqslant 3 k \Omega \\ & R_{L} \geqslant 600 \Omega \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm 12 \\ & \pm 9.5 \end{aligned}$ | $\begin{aligned} & \pm 13 \\ & \pm 10 \end{aligned}$ |  | $\begin{aligned} & \pm 12 \\ & \pm 9.5 \end{aligned}$ | $\begin{aligned} & \pm 13 \\ & \pm 10 \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Input Voltage Range |  | $\pm 12$ | $\pm 13$ |  | $\pm 12$ | $\pm 13$ |  | V |
| Common Mode Rejection Ratio | RS $\leqslant 10 \mathrm{k} \Omega$ | 80 | 100 |  | 80 | 100 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 10 | 75 |  | 10 | 75 | $\mu \mathrm{V} / \mathrm{V}$ |
| Supply Current | $\mathrm{R}_{\mathrm{L}}=\infty$ (All Amplifiers) |  | 3.3 | 5.6 |  | 3.3 | 5.6 | mA |
| Transient Response (unity gain) <br> Rise Time | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=20 \mathrm{mV}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, \\ & \mathrm{C}_{\mathrm{L}} \leqslant 100 \mathrm{pf} \end{aligned}$ |  | 80 |  |  | 80 |  | nsec |
| Overshoot |  |  | 18 |  |  | 18 |  | \% |
| Slew Rate (unity gain) |  | 1.5 | 2.0 |  | 1.5 | 2.0 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Unity Gain Bandwidth |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  | MHz |
| Full Power Bandwidth | $\mathrm{V}_{\mathrm{O}}=20 \mathrm{~V}_{\mathrm{p}-\mathrm{p}}$ | 24 | 32 |  | 24 | 32 |  | kHz |
| Input Noise Voltage | $\mathrm{f}=20 \mathrm{~Hz}$ to 20 kHz |  | 1.4 | 2.0 |  | 1.4 | 2.0 | $\mu \mathrm{V}$ RMS |
| Input Noise Current | $\mathrm{f}=20 \mathrm{~Hz}$ to 20 kHz |  | 25 |  |  | 25 |  | pA RMS |
| Channel Separation | $\begin{aligned} & \text { Gain }=100 \\ & \mathrm{f}=10 \mathrm{kHz}, \mathrm{R}_{\mathrm{S}}=1 \mathrm{k} \Omega \end{aligned}$ |  | 90 |  |  | 90 |  | dB |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for RM4559; $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C}$ for RC4559 |  |  |  |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{RS}^{5} \leqslant 10 \mathrm{k} \Omega$ |  |  | 6.0 |  |  | 7.5 | mV |
| Input Offset Current |  |  |  | 300 |  |  | 200 | nA |
| Input Bias Current |  |  |  | 500 |  |  | 500 | nA |
| Large-Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega, \mathrm{V}_{\text {out }}= \pm 10 \mathrm{~V}$ | 25,000 |  |  | 15,000 |  |  |  |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ |  |  | $\pm 10$ |  |  | V |
| Supply Current (All Amplifiers) | $\begin{aligned} & \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=\infty \\ & \mathrm{T}_{\mathrm{A}}=+125^{\circ} \mathrm{C} \\ & \mathrm{~T}_{\mathrm{A}}=-55^{\circ} \mathrm{C} \end{aligned}$ |  | 3 4 | $\begin{gathered} 5 \\ 6.6 \end{gathered}$ |  | 3 4 | $\begin{gathered} 5 \\ 6.6 \end{gathered}$ | mA |

MATCHING CHARACTERISTICS $\quad\left(V_{C C}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM4559 <br> TYP | RC4559 <br> TYP | UNITS |
| :--- | :---: | :---: | :---: | :---: |
| Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 0.5$ | $\pm 1.0$ | dB |
| Input Bias Current |  | $\pm 15$ | $\pm 15$ | nA |
| Input Offset Current |  | $\pm 7.5$ | $\pm 7.5$ | nA |
| Input Offset VoItage | $\mathrm{RS} \geqslant 10 \mathrm{k} \Omega$ | $\pm 0.1$ | $\pm 0.2$ | mV |

## NOTES:

1. Rating applies for case temperatures to $125^{\circ} \mathrm{C}$; derate linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperatures above $+75^{\circ} \mathrm{C}$ for RM 4559 .
2. For supply voltages less than -15 V , the absolute maximum input voltage is equal to the supply voltage.
3. Short circuit may be to ground on one amp only. Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature for RC4559 and to $+85^{\circ} \mathrm{C}$ ambient temperature for RV4559.

## TYPICAL ELECTRICAL DATA



## TYPICAL ELECTRICAL DATA



Channel Separation




Total Harmonic Distortion vs Output Voltage


Distortion vs Frequency $\mathrm{V}_{\mathrm{o}}=\mathbf{1 v r m s}$
(\%! NOILYOLSIO JINOWY $\forall H 7 \forall \perp O 1$


## GENERAL DESCRIPTION

The RC4739 dual low-noise operational amplifier is fabricated on a single silicon chip using the planar epitaxial process. It was designed primarily for preamplifiers in consumer and industrial signal processing equipment. The device is pin compatible with the $\mu \mathrm{A} 739$ and MC1303, however, compensation is internal. This permits a lowered external parts count and simplfied application.
The RC4739 is available in molded dual in-line 14 -pin package and operated over the commercial temperature range from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Internally Compensated Replacement for $\mu \mathrm{A} 739$ and MC1303
- Signal-to-Noise Ratio 76 dB (RIAA 10 mV ref.)
- Channel Separation 125 dB
- Unity Gain Bandwidth 3 MHz
- Output Short-Circuit Protected
- $0.1 \%$ Distortion at 8.5 V RMS Output into $2 \mathrm{k} \Omega$ Load

SCHEMATIC DIAGRAM
(1/2 Shown)


CONNECTION INFORMATION


## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage | $\pm 18 \mathrm{~V}$ | Storage Temperature Range | $-65{ }^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: |
| Internal Power Dissipation (Note 1) | 500 mW | Operating Temperature Range | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ | Lead Temperature (Soldering, 60s) | $300^{\circ} \mathrm{C}$ |
| Input Voltage (Note 2) | $\pm 15 \mathrm{~V}$ | Output Short-Circuit Duration (Note 3) | Indefinite |

ELECTRICAL CHARACTERISTICS $\left(V_{C C}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$ unless otherwise noted.)

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 2.0 | 6.0 | mV |
| Input Offset Current |  |  | 5.0 | 200 | $n \mathrm{~A}$ |
| Input Bias Current |  |  | 40 | 500 | nA |
| Input Resistance |  | 0.3 | 5.0 |  | $\mathrm{M} \Omega$ |
| Large-Signal Voltage Gain | $\begin{aligned} & R_{L} \geqslant 2 \mathrm{k} \Omega \\ & V_{\text {out }}= \pm 10 \mathrm{~V} \end{aligned}$ | 20,000 | 300,000 |  | V/V |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{k} \Omega$ | $\pm 12$ | $\pm 14$ |  | V |
|  | $R_{L} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ | $\pm 13$ |  | V |
| Input Voltage Range |  | $\pm 12$ | $\pm 14$ |  | V |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ | 70 | 100 |  | dB |
| Supply Voltage Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 10 | 150 | $\mu \mathrm{V} / \mathrm{V}$ |
| Power Consumption |  |  | 105 | 170 | mW |
| Transient Response (unity gain) Risetime | $\begin{aligned} & \mathrm{V}_{\text {in }}=20 \mathrm{mV} \\ & \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \\ & \mathrm{C}_{\mathrm{L}} \leqslant 100 \mathrm{pF} \end{aligned}$ |  | 0.15 |  | $\mu \mathrm{s}$ |
| Transient Response (unity gain) Overshoot | $\begin{aligned} & \mathrm{V}_{\text {in }}=20 \mathrm{mV} \\ & \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \\ & C_{L} \leqslant 100 \mathrm{pF} \end{aligned}$ |  | 10 |  | \% |
| Slew Rate (unity gain) | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ |  | 1.0 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Broadband Noise Voltage | $\begin{aligned} & \mathrm{BW}_{\mathrm{W}}=10-30 \mathrm{KHz} \\ & \mathrm{R}_{\mathrm{S}}=1 \mathrm{k} \Omega \end{aligned}$ |  | 2.5 |  | $\mu V_{\text {RMS }}$ |
| Channel Separation | $\begin{aligned} & \mathrm{f}=1.0 \mathrm{kHz} \\ & \mathrm{AV}=40 \mathrm{~dB} \\ & \mathrm{R}_{\mathrm{S}}=1 \mathrm{k} \Omega \\ & \hline \end{aligned}$ |  | 125 |  | dB |
| The following specification apply for $0^{\circ} \mathrm{C} \leqslant T_{A} \leqslant 70^{\circ} \mathrm{C}$ unless otherwise specified. |  |  |  |  |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{k} \Omega$ |  | 3.0 | 7.5 | mV |
| Input Offset Current |  |  | 7.0 | 300 | $n \mathrm{~A}$ |
| Input Bias Current |  |  | 50 | 800 | nA |
| Large-Signal Voltage Gain | $\begin{aligned} & R_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega \\ & \mathrm{~V}_{\text {out }}= \pm 10 \mathrm{~V} \end{aligned}$ | 15,000 | 200,000 |  |  |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{k} \Omega$ | $\pm 10$ | $\pm 13$ |  | V |
| Power Consumption | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ |  |  |  |  |
|  | $\mathrm{T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ |  | 100 | 150 | mW |
|  | $\mathrm{T}^{\prime} \mathrm{A}=0^{\circ} \mathrm{C}$ |  | 110 | 220 | mW |

## NOTES:

1. Rating applies for ambient temperatures below $+70^{\circ} \mathrm{C}$.
2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage
3. Short-circuit may be to ground, typically 45 mA . Rating applies to $+125^{\circ} \mathrm{C}$ case temperature or $+75^{\circ} \mathrm{C}$ ambient temperature.

## TYPICAL ELECTRICAL DATA




Typical Output Voltage as a Function of Supply Voltage


Quiesent Current as a
Function of Supply Voltage


Input Offset Current as a Function of Ambient Temperature


Open Loop Gain as a Function of Temperature


Output Voltage Swing as a Function of Load Resistance


Transient Response




Output Voltage Swing as a
Function of Frequency


Voltage Follower
Large-Signal Pulse Response


## TYPICAL ELECTRICAL DATA



## TYPICAL APPLICATIONS



## DESCRIPTION

The HA-4741 is a monolithic integrated circuit, consisting of four independent operational amplifiers constructed with the planar epitaxial process.

These amplifiers feature AC and DC performance which exceed that of the 741 type amplifiers. Its superior bandwidth, slew rate and noise characteristics make it an excellent choice for active filter or audio amplifier applications.

## FEATURES

- Unity Gain Bandwidth 3.5 MHz (typical)
- High Slew Rate $1.6 \mathrm{~V} / \mu \mathrm{S}$ (typical)
- Low Noise Voltage $9 \mathrm{nV} / \sqrt{\mathrm{Hz}}$ (typical)
- Input Offset Voltage 0.5 mV (typical)
- Input Bias Current 60nA (typical)
- Indefinite Short Circuit Protection
- No Crossover Distortion
- Internal Compensation
- Wide Power Supply Range $\pm 2 \mathrm{~V}$ to $\pm 20 \mathrm{~V}$

SCHEMATIC DIAGRAM (1/4 Shown)


## CONNECTION INFORMATION

Order Part Nos.:
HA1-4741-2
HA1-4741-8
HA1-4741-5
HA3-4741-5



ELECTRICAL CHARACTERISTICS $\mathrm{V}_{\mathrm{CC}} \pm 15 \mathrm{~V} \mathrm{~T}_{\mathrm{A}}+25^{\circ} \mathrm{C}$ unless otherwise specified

| PARAMETER | CONDITIONS | HA-4741-2 |  |  | HA-4741-5 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ |  | 0.5 | 3.0 |  | 1.0 | 5.0 | mV |
| Input Offset Current |  |  | 15 | 30 |  | 30 | 50 | nA |
| Input Bias Current |  |  | 60 | 200 |  | 60 | 300 | nA |
| Input Resistance |  |  | 0.5 |  |  | 0.5 |  | $\mathrm{M} \Omega$ |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | 50,000 | 100,000 |  | 25,000 | 50,000 |  | V/V |
| Input Voltage Range |  | $\pm 12$ |  |  | $\pm 12$ |  |  | V |
| Output Resistance |  |  | 300 |  |  | 300 |  | $\Omega$ |
| Output Current | $\mathrm{V}_{\text {OUT }} \pm 10 \mathrm{~V}$ | $\pm 5$ | $\pm 15$ |  | $\pm 5$ | $\pm 15$ |  | mA |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega \Delta \mathrm{~V}= \pm 5 \mathrm{~V}$ | 80 |  |  | 80 |  |  | dB |
| Supply Current (all amplifiers) | $\mathrm{R}_{\mathrm{L}}=\infty$ |  | 4.5 | 5.0 |  | 5.0 | 7.0 | mA |
| Transient Response |  |  |  |  |  |  |  |  |
| Overshoot |  |  | 25\% |  |  | 25\% |  | \% |
| Slew Rate |  |  | 1.6 |  |  | 1.6 |  | $\mathrm{V} / \mu \mathrm{s}$ |
| Unity Gain Bandwidth |  |  | 3.5 |  |  | 3.5 |  | MHz |
| Full Power Bandwidth | $\mathrm{V}_{0}=20 \mathrm{Vp-p} \mathrm{R}_{\mathrm{L}}=2 \mathrm{~K}$ |  | 25 |  |  | 25 |  | kHz |
| Input Noise Voltage | $\mathrm{f}=1 \mathrm{kHz}$ |  | 9 |  |  | 9 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| Channel Separation |  |  | 108 |  |  | 108 |  | dB |

The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for $\mathrm{HA}-4741-2,0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C}$ for HA-4741-5.

| Input Offset Voltage | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega$ |  | 4.0 | 5.0 |  | 5.0 | 6.5 | mV |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Input Offset Current |  |  |  | 75 |  |  | 100 | nA |
| Input Bias Current |  |  |  | 325 |  |  | 400 | nA |
| Large Signal Voltage Gain | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega \mathrm{~V}_{0 \mathrm{UT}} \pm 10 \mathrm{~V}$ | 25,000 |  |  | 15,000 |  |  | $\mathrm{~V} / \mathrm{V}$ |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}} \geqslant 10 \mathrm{~K} \Omega$ | $\pm 12$ | $\pm 13.7$ |  | $\pm 12$ | $\pm 13.7$ |  | V |
|  | $\mathrm{R}_{\mathrm{L}} \geqslant 2 \mathrm{~K} \Omega$ | $\pm 10$ | $\pm 12.5$ |  | $\pm 10$ | $\pm 12.5$ |  | V |
| Supply Current (all Amplifiers) |  |  | 10 |  |  | 10 |  | mA |
| Average Offset Voltage Drift |  |  | 5 |  |  | 5 |  | $\mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| Common Mode Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega \Delta \mathrm{~V} \pm 5 \mathrm{~V}$ | 74 |  |  | 74 |  |  | dB |
| Power Supply Rejection Ratio | $\mathrm{R}_{\mathrm{S}} \leqslant 10 \mathrm{~K} \Omega \Delta \mathrm{~V} \pm 5 \mathrm{~V}$ | 80 |  |  | 80 |  |  | dB |

Notes: 1. Rating applies for case temperature of $+25^{\circ} \mathrm{C}$ maximum; derate linearity at $6.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for temperatures above $+25^{\circ} \mathrm{C}$.
2. For supply voltage less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
3. Short circuit to ground on one amplifier only.

## TYPICAL PERFORMANCE DATA




Power Supply Rejection Ratio vs. Temperature


Input Noise vs. Frequency


Slew Rate vs. Supply Voltage


Channel Separation vs. Frequency


Transient Response vs. Temperature


Normalized AC Parameters vs. Temperature


Power Consumption vs. Temperature.


Small Signal Bandwidth and Phase Margin vs. Load Capacitance


Input Currents vs. Temperature


Output Voltage Swing vs. Load Resistance


Output Voltage Swing vs. Frequency


Common Mode Rejection Ratio vs. Temperature

AVAILABLE TYPES

| Part Number | Package | Operating Temperature |
| :--- | :--- | :---: |
| HA1-4741-2 | Ceramic | -55 to $+125^{\circ} \mathrm{C}$ |
| HA1-4741-8* | Ceramic | -55 to $+125^{\circ} \mathrm{C}$ |
| HA1-4741-5 | Ceramic | 0 to $+70^{\circ} \mathrm{C}$ |
| HA3-4741-5 | Plastic | 0 to $+70^{\circ} \mathrm{C}$ |

* Processed to MIL-STD-883 Class B



## SECTION 2

Wideband Amplifier

## CONTENTS

## GENERAL DESCRIPTION

The RM733/RC733 integrated circuit is a monolithic video amplifier with differential inputs and differential outputs. It offers three selectable voltage gains of 10,100 , or 400 and adjustable gain of 10 to 400 using a single resistor. No external frequency compensation is necessary for any gain option. The circuit and process designs are optimized to give a stable gain ( $\pm 10 \%$ ), wide bandwidth (DC to 120 MHz ), high input resistance ( $250 \mathrm{k} \Omega$ ), and low phase shift that is linear up to 10 MHz ( $2^{\circ}$ per MHz).
The RM733/RC733 is designed for use as a read head amplifier for magnetic tape, drum, or disc memories using phase of NRZ encoding. It will also function as a preamplifier for high speed film or plated wire memory systems; as a video or pulse amplifier, pulse height detector, peak detector.
Applications for the RM733/RC733 include bulk computer
memory systems, very high speed random access memory systems, communications systems, nuclear event instrumentation, frequency counters, and other systems where the specific design features of the RM733/RC733 are required.
The RM733 video amplifier will operate over the complete military temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ while the commercial version, the RC733, operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Wide Bandwidth DC to 120 MHz
- Low Linear Phase Shift $2 \tau / \mathrm{MHz}$ to 10 MHz
- Selectable Voltage Gains 10, 100, or 400
- Excellent Pulse Characteristics
- High Input Resistance $250 \mathrm{k} \Omega$


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



ABSOLUTE MAXIMUM RATINGS
Supply Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . $\pm 8.0 \mathrm{~V}$
Differential Input Voltage. . . . . . . . . . . . . . . . $\pm 5.0 \mathrm{~V}$
Common Mode Input Voltage . . . . . . . . . . . . $\pm 6.0 \mathrm{~V}$
Input Current. . . . . . . . . . . . . . . . . . 10 mA
Internal Power Dissipation Metal Can (Note 1) . . . 500 mW
Flat Pack . . . . . . . . . . . . . . . . . . . . . . . . 570 mW

Operating Temperature Range
RM733 $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
RC733
$0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature Range. . . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 60s) . . . . . . . . . . . . $300^{\circ} \mathrm{C}$

## ELECTRICAL CHARACTERISTICS

 (Note 2)| PARAMETER | (Note 3) | CONDITIONS | RM733 |  |  | RC733 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Differential Voltage Gain | Gain 1 |  | 300 | 400 | 500 | 250 | 400 | 600 |  |
|  | Gain 2 |  | 90 | 100 | 110 | 80 | 100 | 120 |  |
|  | Gain 3 |  | 9.0 | 10 | 11 | 8.0 | 10 | 12 |  |
| Bandwidth | Gain 1 | $\mathrm{RS}=50 \Omega$ |  | 40 |  |  | 40 |  | MHz |
|  | Gain 2 |  |  | 90 |  |  | 90 |  |  |
|  | Gain 3 |  |  | 120 |  |  | 120 |  |  |
| Risetime | Gain 1 | $\mathrm{R}_{\mathrm{S}}=50 \Omega, \mathrm{~V}_{\text {OUT }}=1 \mathrm{~V}_{\text {PP }}$ |  | 10.5 |  |  | 10.5 |  | ns |
|  | Gain 2 |  |  | 4.5 | 10 |  | 4.5 | 12 |  |
|  | Gain 3 |  |  | 2.5 |  |  | 2.5 |  |  |
| Propagation Delay | Gain 1 | $\mathrm{R}_{\mathrm{S}}=50 \Omega, \mathrm{~V}_{\text {OUT }}=1 \mathrm{VPP}$ |  | 7.5 |  |  | 7.5 |  |  |
|  | Gain 2 |  |  | 6.0 | 10 |  | 6.0 | 10 | ns |
|  | Gain 3 |  |  | 3.6 |  |  | 3.6 |  |  |
| Input Resistance | Gain 1 |  |  | 4.0 |  |  | 4.0 |  |  |
|  | Gain 2 |  | 20 | 30 |  | 10 | 30 |  | $k \Omega$ |
|  | Gain 3 |  |  | 250 |  |  | 250 |  |  |
| Input Capacitance |  | Gain 2 |  | 2.0 |  |  | 2.0 |  | pF |
| Input Offset Current |  |  |  | 0.4 | 3.0 |  | 0.4 | 5.0 | $\mu \mathrm{A}$ |
| Input Bias Current |  |  |  | 9.0 | 20 |  | 9.0 | 30 | $\mu \mathrm{A}$ |
| Input Noise Voltage |  | $\mathrm{RS}=50 \Omega, \mathrm{BW}=1 \mathrm{kHz}$ to 10 MHz |  | 12 |  |  | 12 |  | $\mu \mathrm{Vrms}$ |
| Input Voltage Range |  |  | $\pm 1.0$ |  |  | $\pm 1.0$ |  |  | V |
| Common Mode Rejection Ratio | Gain 2 | $\mathrm{V}_{\mathrm{CM}}= \pm 1 \mathrm{~V}, \mathrm{R} \leqslant 100 \mathrm{kHz}$ | 60 | 86 |  | 60 | 86 |  | dB |
|  |  | $V_{C M}= \pm 1 \mathrm{~V}, \mathrm{f}=5 \mathrm{MHz}$ |  | 60 |  |  | 60 |  |  |
| Supply Voltage Rejection Ratio | Gain 2 | $\Delta V_{S}= \pm 0.5 \mathrm{~V}$ | 50 | 70 |  | 50 | 70 |  | dB |
| Output Offset Voltage | Gain 1 |  |  | 0.6 | 1.5 |  | 0.6 | 1.5 |  |
|  | Gain 2 Gain 3 |  |  | 0.35 | 1.0 |  | 0.35 | 1.5 | V |
| Output Common Mode Voltage |  |  | 2.4 | 2.9 | 3.4 | 2.4 | 2.9 | 3.4 | V |
| Output Voltage Swing |  |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  | VPP |
| Output Sink Current |  |  | 2.5 | 3.6 |  | 2.5 | 3.6 |  | mA |
| Output Resistance |  |  |  | 20 |  |  | 20 |  | $\Omega$ |
| Power Supply Current |  |  |  | 18 | 24 |  | 18 | 24 | mA |

## NOTES:

1. For RM733 the rating applies for case temperature to $+125^{\circ} \mathrm{C}$; derate RM733T linearly at $6.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperature above $75^{\circ} \mathrm{C}$. For RC733T, the rating applies for ambient temperatures to $70^{\circ} \mathrm{C}$. For RM733CQ, derate linearly at $7.2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for ambient temperature above $75^{\circ} \mathrm{C}$.
2. $V_{S}= \pm 6.0 \mathrm{~V} ; T_{A}=25^{\circ} \mathrm{C}$ unless otherwise noted.
3. Gain 1: G1A and G1B connected together; Gain 2: G2A and G2B connected together; Gain 3: Gain select pins open.

## ELECTRICAL CHARACTERISTICS

(The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 125^{\circ} \mathrm{C}$ for the RM 733 and $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 70^{\circ} \mathrm{C}$ for the $\mathrm{RC} 733, \mathrm{~V}_{\mathrm{S}}= \pm 6.0 \mathrm{~V}$ )

| PARAMETER | CONDITIONS | LM733 |  |  | LM733C |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Differential Voltage Gain Gain 1 |  | 200 |  | 600 | 250 |  | 600 |  |
| Gain 2 |  | 80 |  | 120 | 80 |  | 120 |  |
| Gain 3 |  | 8.0 |  | 12.0 | 8.0 |  | 12.0 |  |
| Input Resistance Gain 2 |  | 8 |  |  | 8 |  |  | $k \Omega$ |
| Input Offset Current |  |  |  | 5 |  |  | 6 | $\mu \mathrm{A}$ |
| Input Bias Current |  |  |  | 40 |  |  | 40 | $\mu \mathrm{A}$ |
| Input Voltage Range |  | $\pm 1$ |  |  | $\pm 1$ |  |  | V |
| Common-Mode Rejection Ratio Gain 2 |  | 50 |  |  | 50 |  |  | dB |
| Supply Voltage Rejection Ratio Gain 2 |  | 50 |  |  | 50 |  |  | db |
| Output Offset Voltage Gain 1 |  |  |  | 1.5 |  |  | 1.5 | V |
| Gain 2 and 3 |  |  |  | 1.2 |  |  | 1.5 | V |
| Output Voltage Swing |  | 2.5 |  |  | 2.8 |  |  | $\checkmark \mathrm{p}$-p |
| Output Sink Current |  | 2.2 |  |  | 2.5 |  |  | mA |
| Power Supply Current |  |  |  | 27 |  |  | 27 | mA |

## SECTION 3

Voltage Regulators

## CONTENTS

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4195 Fixed $\pm 15$-Volt Dual-Tracking ..... 3-9Voltage Regulator
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## GENERAL DESCRIPTION

The LM105 series are positive voltage regulators, each constructed on a silicon chip by the planar epitaxial process.
They are similar to the LM100, except for an extra gain stage to improve regulation. In both linear and switching regulator circuits with outputs greater than 4.5 V , these devices are direct plug-in replacements for the LM100.
The LM105 military version operates from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The LM305/LM305A are commercial versions which operate from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.
These regulators feature fast response to load and line transients, freedom from oscillations with varying resistive and reactive loads, and reliable starts on any load within ratings.
The LM205 is the same as the LM105 except its performance is guaranteed from $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$.

## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## DESIGN FEATURES

- Output Voltage Adjustable from 4.5 V to 40 V
- Output Currents in Excess of 10A by Adding External Transistors
- Load Regulation Better Than 0.1\%, Full Load With Current Limiting
- DC Line Regulation Guaranteed at $0.03 \% / \mathrm{V}$
- Ripple Rejection of 0.01\%/V
- 45mA Output Current Without External Pass Transistor


## TYPICAL APPLICATIONS



ABSOLUTE MAXIMUM RATINGS

| Input Voltage . . . . . . LM105, LM205, LM305A: 50V | Operating Temperature Range $\text { LM105 . . . . . . . . . . . . . . . . . . . . }-55^{\circ} \mathrm{C} \text { to }+150^{\circ} \mathrm{C}$ |
| :---: | :---: |
| Input-Output Voltage Differential . . . . . . . . . . . . 40V | LM205 . . . . . . . . . . . . . . . . . . . $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Power Dissipation (Note 1) | LM305/305A . . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| LM105, LM205, LM305A . . . . . . . . . . . . . . 800mW | Storage Temperature Range . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| LM305 . . . . . . . . . . . . . . . . . . . . . . . . . . . 500mW | Lead Temperature (Soldering, 10s) . . . . . . . . $300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS (Note 2)


## NOTES:

1. The maximum junction temperature of the LM105 is $150^{\circ} \mathrm{C}$ and $85^{\circ} \mathrm{C}$ for the LM305. For operating at elevated temperatures, devices in the TO-5 package must be derated based on a thermal resistance of $150^{\circ} \mathrm{C} / \mathrm{W}$ junction to ambient, or $45^{\circ} \mathrm{C} / \mathrm{W}$ junction to case. For the flat package, the derating is based on a thermal resistance of $185^{\circ} \mathrm{C} / \mathrm{W}$ when mounted on a $1 / 16$-inch thick epoxy glass board with ten, 0.03 -inch-wide, 2 -ounce copper conductors. Peak dissipations to 1 W are allowable providing the dissipation rating is not exceeded with the power averaged over a five second interval, for the LM105, and averaged over a two second inverval for the LM305,
2. These specifications apply for input and output voltages within the ranges given, and for a divider impedance seen by the feedback terminal of $2 \mathrm{k} \Omega$, unless otherwise specified. The load and line regulation specifications are for constant junction temperature. Temperature drift effects must be taken into account separately when the unit is operating under conditions of high dissipation.
3. The output currents given, as well as the load regulation, can be increased by the addition of external transistors. The improvement factor will be roughly equal to the composite current gain of the added transistors.
4. No external pass transistor.

## GENERAL DESCRIPTION

The RM723/RC723 integrated circuits are monolithic voltage regulators constructed on a single silicon chip. They consist of a temperature compensated reference amplifier, error amplifier, a power series pass transistor capable of 150 mA , and current limiting circuitry.

They feature low standby current drain, low temperature drift and high ripple rejection.
These devices are designed for use as a logic card regulator, small instrument power supply, or, by use of an external pass transistor, as a negative or floating regulator. They may also be used where local voltage supply regulation is required for linear and digital circuits. Provision is made for adjustable current limiting and remote shutdown.
The RM723 operates over the full military temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The RC723 operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Positive or Negative Supply Operation
- Series, Shunt, Switching or Floating Operation
- 0.01\% Line and Load Regulation
- Output Voltage Adjustable from 2V to 37V
- Output Current to 150 mA Without External Pass Transistor


## SCHEMATIC DIAGRAM



CONNECTION INFORMATION


## ABSOLUTE MAXIMUM RATINGS

| Pulse Voltage from $\mathrm{V}^{+}$to $\mathrm{V}^{-}(50 \mathrm{~ms})$ | RM723: 50V | Internal Power Dissipation-DIP (Note 1) | 900mW |
| :---: | :---: | :---: | :---: |
| Continuous Voltage from $\mathrm{V}^{+}$to $\mathrm{V}^{-}$. | 40 V | Operating Temperature Range |  |
| Input-Output Voltage Differential | 40 V | RC723 | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Maximum Output Current | 150 mA | RM723 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Current from $\mathrm{V}_{\mathrm{Z}}$ | 25 mA | Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Current from V ${ }_{\text {REF }}$ | 15 mA | Lead Temperature (Soldering, 60s) | $300^{\circ} \mathrm{C}$ |
| Internal Power Dissipation-Metal Can | 900 mW |  |  |

## ELECTRICAL CHARACTERISTICS <br> (Note 2)

| PARAMETER | CONDITIONS | RM723 |  |  | RC723 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Line Regulation | $V_{\text {IN }}=12 \mathrm{~V}$ to $\mathrm{V}_{\text {IN }}=15 \mathrm{~V}$ |  | 0.01 | 0.1 |  | 0.01 | 0.1 | \% V OUT |
|  | $\mathrm{V}_{\text {IN }}=12 \mathrm{~V}$ to $\mathrm{V}_{\text {IN }}=40 \mathrm{~V}$ |  | 0.02 | 0.2 |  | 0.1 | 0.5 |  |
|  | $\begin{aligned} & -55^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant+125^{\circ} \mathrm{C} \\ & V_{I N}=12 \mathrm{~V} \text { to } V_{\text {IN }}=15 \mathrm{~V} \end{aligned}$ |  |  | 0.3 |  |  | 0.3 |  |
| Load Regulation | $\mathrm{I}_{\mathrm{L}}=1 \mathrm{~mA}$ to $\mathrm{I}_{\mathrm{L}}=50 \mathrm{~mA}$ |  | 0.03 | 0.15 |  | 0.03 | 0.2 | \% V OUT |
|  | $\begin{aligned} & -55^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant+125^{\circ} \mathrm{C} \\ & \mathrm{I}_{\mathrm{L}}=1 \mathrm{~mA} \text { to } \mathrm{I}_{\mathrm{L}}=50 \mathrm{~mA} \end{aligned}$ |  |  | 0.6 |  |  | 0.6 |  |
| Ripple Rejection | $f=50 \mathrm{~Hz}$ to $10 \mathrm{kHz}, \mathrm{C}_{\text {REF }}=0$ |  | 74 |  |  | 74 |  | dB |
|  | $\mathrm{f}=50 \mathrm{~Hz}$ to $10 \mathrm{kHz}, \mathrm{C}_{\text {REF }}=5 \mu \mathrm{~F}$ |  | 86 |  |  | 86 |  |  |
| Average Temperature Coeffieient of Output Voltage | $\begin{aligned} & -55^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant+125^{\circ} \mathrm{C}(\mathrm{RM}) \\ & 0^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 70^{\circ} \mathrm{C}(R \mathrm{C}) \end{aligned}$ |  | 0.002 | 0.015 |  | 0.003 | 0.015 | \%/ ${ }^{\circ} \mathrm{C}$ |
| Short Circuit Current Limit | $\mathrm{R}_{\text {SC }}=10 \Omega, \mathrm{~V}_{\text {OUT }}=0$ |  | 65 |  |  | 65 |  | mA |
| Reference Voltage |  | 6.95 | 7.15 | 7.35 | 6.80 | 7.15 | 7.50 | V |
| Output Noise Voltage | $\mathrm{BW}=100 \mathrm{~Hz}$ to $10 \mathrm{kHz}, \mathrm{C}_{\text {REF }}=0$ |  | 20 |  |  | 20 |  | $\mu \mathrm{V}_{\text {rms }}$ |
|  | $\mathrm{BW}=100 \mathrm{~Hz}$ to $10 \mathrm{kHz}, \mathrm{C}_{\text {REF }}=5 \mu \mathrm{~F}$ |  | 2.5 |  |  | 2.5 |  |  |
| Long Term Stability |  |  | 0.1 |  |  | 0.1 |  | $\% / 1000 \mathrm{hr}$ |
| Standby Current Drain | $I_{L}=0, V_{\text {IN }}=30 \mathrm{~V}, \mathrm{~V}_{O}=V_{\text {REF }}$ |  | 2.3 | 3.5 |  | 2.3 | 4.0 | mA |
| Input Voltage Range |  | 9.5 |  | 40 | 9.5 |  | 40 | V |
| Output Voltage Range |  | 2.0 |  | 37 | 2.0 |  | 37 | V |
| Input-Output Voltage Differential |  | 3.0 |  | 38 | 3.0 |  | 38 | V |

## NOTES:

1. Derate metal can package at $6.8 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ and dual in-line package at $7.8 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for operation at ambient temperatures above $+25^{\circ} \mathrm{C}$.
2. Unless otherwise specified, $T_{A}=25^{\circ} C, V_{I N}=V^{+}=V_{C}=12 \mathrm{~V}, V^{-}=0, V_{O U T}=5 \mathrm{~V}, I_{L}=1 \mathrm{~mA}, R_{S C}=0, C_{i}=100 \mathrm{pF}, C_{R E F}=0$, divider impedance as seen by error amplifier $\leqslant 10 \mathrm{k} \Omega$.
3. For metal can applications where $V_{Z}$ is required, an external 6.2 zener should be connected in series with $V_{\text {OUT }}$.

## GENERAL DESCRIPTION

The RM4194 and RC4194 are dual polarity tracking regulators designed to provide balanced or unbalanced positive and negative output voltages at currents to 200 mA . A single external resistor adjustment can be used to change both outputs between the limits of $\pm 50 \mathrm{mV}$ and $\pm 42 \mathrm{~V}$.

These devices are designed for local "on-card" regulation, eliminating distribution problems associated with single-point regulation. To simplify application the regulators require a minimum number of external parts.
The device is available in two package types to accommodate various power requirements. The TK (TO-66) power package can dissipate up to $3 W$ at $T_{A}=25^{\circ} \mathrm{C}$. The DC 14-pin dual inline will dissipate up to $1 W$.

## DESIGN FEATURES

- Simultaneously Adjustable Outputs With One Resistor to $\pm 42 \mathrm{~V}$
- Load Current $\pm 200 \mathrm{~mA}$ with $0.2 \%$ Load Regulation
- Internal Thermal Shutdown at $\mathrm{T}_{\mathrm{i}}=175^{\circ} \mathrm{C}$
- External Balance for $\pm \mathrm{V}_{0}$ Unbalancing
- 3W Power Dissipation


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Input Voltage $\pm$ V to Ground . . . . <br> Input-Output Voltage Differential | RM4194: $\pm 45 \mathrm{~V}$ | Load Current |  |
| :---: | :---: | :---: | :---: |
|  | RC4194: $\pm 35 \mathrm{~V}$ | DC Package | . 150 mA |
|  | RM4194: $\pm 45 \mathrm{~V}$ | TK Package | . 250 mA |
|  | RC4194: $\pm 35 \mathrm{~V}$ | DB Package | . 100 mA |
| Power Dissipation at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | Operation Junction Temperature Range |  |
| DC Package | 1W | RM4194 | $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| TK Package | 3.0W | RC4194 | $.0^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| DB Package | 625 mW | Storage Temperature Range. | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
|  |  | Lead Temperature (Soldering, 10s) | . $+300^{\circ} \mathrm{C}$ |

## ELECTRICAL CHARACTERISTICS

$\left( \pm 5 \leqslant V_{\text {OUT }} \leqslant V_{\text {MAX }} ; R M 4194:-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{j} \leqslant+125^{\circ} \mathrm{C} ; \mathrm{RC} 4194: 0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{j} \leqslant+70^{\circ} \mathrm{C}\right)$ (Note 2)

| PARAMETER | CONDITIONS | RM4194 |  |  | RC4194 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Line Regulation | $\Delta \mathrm{V}_{\text {IN }}=0.1 \mathrm{~V}_{\text {IN }}$ |  | 0.04 | 0.1 |  | 0.04 | 0.1 | \%VOUT |
| Load Regulation | $\begin{aligned} & 4194 \mathrm{TK}: I_{\mathrm{L}}=1 \text { to } 200 \mathrm{~mA} \\ & 4194 D \mathrm{C}: I_{\mathrm{L}}=1 \text { to } 100 \mathrm{~mA}, \\ & T_{j}=+25^{\circ} \mathrm{C} \end{aligned}$ |  | 0.001 | 0.002 |  | 0.002 | 0.004 | $\% \mathrm{~V}^{\circ} / \mathrm{mA}$ |
|  | $\begin{array}{\|l\|} \text { RM4194 }=\mathrm{t}_{\mathrm{j}}=-55^{\circ} \mathrm{C}-+125^{\circ} \mathrm{C} \\ \text { RC4194 }=\mathrm{t}_{\mathrm{j}}=0^{\circ} \mathrm{C}-+70^{\circ} \mathrm{C} \\ \hline \end{array}$ |  | 0.002 | 0.004 |  | 0.002 | 0.004 | $\% \mathrm{~V}^{\circ} / \mathrm{mA}$ |
| TC of Output Voltage |  |  | 0.002 | 0.015 |  | 0.002 | 0.015 | \%/ ${ }^{\circ} \mathrm{C}$ |
| TC of Output Voltage |  |  | 0.002 | 0.015 |  | 0.003 | 0.015 | \%/oc |
| Stand-By Current Drain (Note 1) | $V_{\text {IN }}=V_{\text {MAX }}, V_{O}=0 V$ |  | +0.3 | +1.0 |  | +0.3 | +1.5 | mA |
|  | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {MAX }}, \mathrm{V}_{\mathrm{O}}=0 \mathrm{~V}$ |  | -1.2 | -2.0 |  | -1.2 | -3.0 |  |
| Input Voltage Range |  | $\pm 9.5$ |  | $\pm 45$ | $\pm 9.5$ |  | $\pm 35$ | V |
| Output Voltage Scale Factor | $\mathrm{R}_{\text {set }}=71.5 \mathrm{~K}, \mathrm{~T}_{\mathrm{j}}=25^{\circ} \mathrm{C}$ | 2.42 | 2.5 | 2.58 | 2.38 | 2.5 | 2.62 | K $\Omega / \mathrm{V}$ |
| Output Voltage Range | $\mathrm{R}_{\text {set }}=71.5 \mathrm{~K}$ | 0.05 |  | $\pm 42$ | 0.05 |  | $\pm 32$ | V |
| Output Voltage Tracking |  |  |  | 1.0 |  |  | 2.0 | \% |
| Ripple Rejection | $\mathrm{f}=120 \mathrm{~Hz}, \mathrm{~T}_{\mathrm{j}}=25^{\circ} \mathrm{C}$ |  | 70 |  |  | 70 |  | dB |
| Input-Output Voltage Differential | $\begin{aligned} & I_{L}=50 \mathrm{~mA} \\ & T_{A}=+25^{\circ} \mathrm{C} \end{aligned}$ | 3.0 |  |  | 3.0 |  |  | V |
| Output Short Circuit Current | VIN $= \pm 30 \mathrm{~V}$ Max. |  | 300 |  |  | 300 |  | mA |
| Output Noise Voltage | $\begin{aligned} & C_{L}=4.7 \mu \mathrm{~F}, \mathrm{~V}_{\mathrm{O}}= \pm 15 \mathrm{~V} \\ & \mathrm{f}=10 \mathrm{~Hz} \text { to } 100 \mathrm{KHz} \end{aligned}$ |  | 250 |  |  | 250 |  | $\mu \mathrm{V}$ RMS |
| Internal Thermal Shutdown |  |  | 175 |  |  | 175 |  | ${ }^{\circ} \mathrm{C}$ |

## THERMAL CHARACTERISTICS

| PARAMETER | CONDITIONS | PACKAGE |  |  |
| :--- | :--- | :---: | :---: | :---: |
|  |  | DB | DC | TK (TO-66) |
| Power Dissipation | TA $=25^{\circ} \mathrm{C}$ | 625 mW | 1 W | 3 W |
|  | $\mathrm{~T} \mathrm{C}=25{ }^{\circ} \mathrm{C}$ | 1.25 W | 2.2 W | 17.5 W |
| Thermal Resistance | Junction to Ambient, $\theta \mathrm{J}-\mathrm{A}$ | $160^{\circ} \mathrm{C} / \mathrm{W}$ | $128^{\circ} \mathrm{C} / \mathrm{W}$ | $41.6^{\circ} \mathrm{C} / \mathrm{W}$ |
|  | Junction to Case, $\theta \mathrm{J}-\mathrm{C}$ | $80^{\circ} \mathrm{C} / \mathrm{W}$ | $55^{\circ} \mathrm{C} / \mathrm{W}$ | $7.15^{\circ} \mathrm{C} / \mathrm{W}$ |

## NOTE:

1. ${ }^{ \pm}$Quiescent will increase by $50 \mu \mathrm{~A} / \mathrm{V}_{\text {OUT }}$ on positive side and $100 \mu \mathrm{~A} / \mathrm{V}_{\text {OUT }}$ on negative side.
2. The specifications above apply for the given junction temperatures since pulse test conditions are used.

## TYPHCAL ELECTRICAL TEST DATA



## TYPICAL APPLICATIONS



## GENERAL DESCRIPTION

The RM4195 and RC4195 are dual polarity tracking regulators designed to provide balanced positive and negative 15 V output voltages at currents to 100 mA . These devices are designed for local "on-card" regulation eliminating distribution problems associated with single point regulation. The regulator is intended for ease of application. Only two external components are required for operation (two $10 \mu \mathrm{~F}$ bypass capacitors).
The device is available in three package types to accommodate various applications requiring economy, high power dissipation, and reduced component density.

## destan featunes

- $\pm 15 \mathrm{~V}$ Operational Amplifier Power at Reduced Cost and Component Density
- Thermal Shutdown at $\mathrm{T}_{\mathrm{j}}=+175^{\circ} \mathrm{C}$ in Addition to ShortCircuit Protection
- Output Currents to 100 mA
- May be Used as Single Output Regulator with up to +50 V Output
- Available in TO-66, TO-99, and 8-Pin Plastic Mini-DIP


## SCHEMATIC DIAGRAM



TK (TO-66) Power Package (Bottom View)

TE Metal Can Package (Top View)


Order Part Nos.:
RC4195T, RM4195T

NB Dual In-line
(Top View)


Order Part No.: RC4195NB

Note: The RM/RC4195 is available on special order in the DC (14-pin) ceramic package.

## ABSOLUTE MAXIMUM RATINGS

| Input Voltage $\pm \mathrm{V}$ to Ground | $\pm 30 \mathrm{~V}$ | Operating Junction Temperature Range |  |
| :---: | :---: | :---: | :---: |
| Power Dissipation @ $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | RM4195 . . . . . . . . . . . . . . . | $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| TK Package | 2.4W | RC4195 | $0^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| T Package | 800 mW | Storage Temperature Range |  |
| NB Package | 600 mW | RM4195 | $-65{ }^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Load Current |  | RC4195 | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| TK Package | 150 mA | Lead Temperature (Soldering, 10s) | $\ldots+300^{\circ} \mathrm{C}$ |
| T, and NB Package | 100 mA |  |  |

ELECTRICAL CHARACTERISTICS ( $I_{L}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CC}}= \pm 20 \mathrm{~V}, \mathrm{C}_{\mathrm{L}}=10 \mu \mathrm{~F}$ unless otherwise specified) (Note 1)

| PARAMETER | CONDITIONS | RM4195 |  |  | RC4195 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Line Regulation | $V_{\text {IN }}= \pm 18$ to $\pm 30 \mathrm{~V}$ |  | 2 | 20 |  | 2 | 20 | mV |
| Load Regulation | $\mathrm{I}_{\mathrm{L}}=1$ to 100 mA |  | 5 | 30 |  | 5 | 30 | mV |
| Output Voltage Temperature Stability |  |  | 0.005 | 0.015 |  | 0.005 | 0.015 | \%/ ${ }^{\circ} \mathrm{C}$ |
| Standby Current Drain | $\mathrm{V}_{\text {IN }}= \pm 30 \mathrm{~V}, \mathrm{I}_{\mathrm{L}}=0 \mathrm{~mA}$ |  | $\pm 1.5$ | $\pm 2.5$ |  | $\pm 1.5$ | $\pm 3.0$ | mA |
| Input Voltage Range |  | 18 |  | 30 | 18 |  | 30 | V |
| Output Voltage | $\mathrm{T}_{\mathrm{j}}=+25^{\circ} \mathrm{C}$ | 14.8 | 15 | 15.2 | 14.5 | 15 | 15.5 | V |
| Output Voltage Tracking |  |  | $\pm 50$ | $\pm 150$ |  | $\pm 50$ | $\pm 300$ | mV |
| Ripple Rejection | $f=120 \mathrm{~Hz}, \mathrm{~T}_{\mathrm{j}}=+25^{\circ} \mathrm{C}$ |  | 75 |  |  | 75 |  | dB |
| Input-Output Voltage Differential | $\mathrm{I}_{\mathrm{L}}=50 \mathrm{~mA}$ | 3 |  |  | 3 |  |  | V |
| Short-Circuit Current | $\mathrm{T}_{\mathrm{j}}=+25^{\circ} \mathrm{C}$ |  | 220 |  |  | 220 |  | mA |
| Output Noise Voltage | $\begin{aligned} & \mathrm{T}_{\mathrm{j}}=+25^{\circ} \mathrm{C} \\ & \mathrm{f}=100 \mathrm{~Hz} \text { to } 10 \mathrm{kHz} \end{aligned}$ |  | 60 |  |  | 60 |  | $\mu \mathrm{V}$ RMS |
| Internal Thermal Shutdown |  |  | 175 |  |  | 175 |  | ${ }^{\circ} \mathrm{C}$ |

## THERMAL CHARACTERISTICS

| PARAMETER | CONDITIONS | PACKAGE |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | NB | T (TO-99) | TK (TO-66) |  |
| Power Dissipation | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 0.6 | 0.8 | 2.4 | W |
|  | $\mathrm{~T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$ |  | 2.1 | 9 |  |
| Thermal Resistance | $\theta_{\mathrm{J}-\mathrm{C}}$ |  | 70 | 17 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  | $\theta_{\mathrm{J}-\mathrm{A}}$ | 210 | 185 | 62 |  |

## NOTE:

1. The specifications above apply for the given junction temperatures since pulse test conditions are used.

TYPICAL ELECTRICAL TEST DATA


## TYPICAL APPLICATIONS



## COMPENSATION

For most applications, the compensation technique shown in the data sheet is sufficient. The positive regulator section of the 4194 is compensated by a $0.001 \mu f$ ceramic disc capacitor from the C+ terminal to ground. The negative regulator requires compensation at two points. The first is the C - pin, which should have $0.001 \mu \mathrm{f}$ to the -Vin pin , or case. A ceramic disc is best here also. The second compensation point for the negative side is the -Vout terminal, which ideally should be a $4.7 \mu \mathrm{f}$ solid tantalum capacitor with enough reserve voltage capacity to avoid the momentary shorting and reforming which can occur with tantalum caps. For systems where the cost of a solid tantalum capacitor cannot be justified, it is usually sufficient to use an aluminum capacitor with a $0.03 \mu \mathrm{f}$ ceramic disc in parallel to bypass high frequencies. In addition, if the rectifier filter capacitors have poor high frequency characteristics (like aluminum electrolytics) or if any impedance is in series with the + Vin and $-V i n$ terminals, it is necessary to bypass these two points with $0.01 \mu \mathrm{f}$ ceramic disc capacitors. Just as with monolithic op-amps, some applications may not require these bypass caps, but if in doubt, be sure to include them.
All compensation and bypass caps should have short leads, solid grounds, and be located as close to the RM/RC4194 as possible. Refer to Figure 1 for recommended compensation circuitry.


Figure 1. 4194 Recommended Compensation

## PROTECTION

In systems using monolithic voltage regulators, a number of conditions can exist which, left uncorrected, will destroy the regulator. Fortunately, regulators can easily be protected against these potentially destructive conditions. Monolithic regulators can be destroyed by any reversal of input or output voltage polarity, or if the input voltage drops below the output voltage in magnitude. These conditions can be caused by
inductive loads at the inputs or outputs of the regulator. Other problems are caused by heavy loads at the unregulated inputs to the regulator, which might cause the input voltage to drop below the output voltage at turn-off. If any of the preceding problem conditions are present in your system, it is recommended that you protect the regulator using diodes. These diodes should be high speed types capable of handling large current surges. Figure 2 shows all six of the possible protection diodes. The diodes at the inputs and outputs prevent voltages at those points from becoming reversed. Diodes from outputs to inputs prevent the output voltage from exceeding the input voltage. Chances are that the system under consideration will not require all six diodes, but if in doubt, be sure to include them.


Figure 2. 4194 Regulator Showing all Protective Diodes

## BROWNOUT PROTECTION

The RM/RC4195 is one of the most easily applied and troublefree monolithic IC's available. When used within the data sheet ratings (package power dissipation, maximum output current, minimum and maximum input voltages) it provides the most cost-effective source of regulated $\pm 15$ volts for powering linear IC's.
Sometimes occasions arise in which the RM/RC4195 ratings must be exceeded. One example is the "brownout." During a brownout, line voltages may be reduced to as low as 75 VRMS, causing the input voltage to the RM/RC4 195 to drop below the $\pm 18 \mathrm{~V}$ DC minimum. When this happens, the negative output voltage can go positive. Refer to the schematic diagram on pg. to see how this happens.
When the positive input voltage drops below +18 V , the PNP current source can saturate, causing current, $i$, to drop to zero. This removes all drive from the negative pass transistor, $\mathrm{Q}_{1}$. The negative output is then free to be pulled positive by resistors $R_{1}, R_{2}$, and $R_{3}$. The total value of $R_{1}+R_{2}+R_{3}$ is 30 K ohms, so the maximum amount of current available is approximately 5 mA .

In general, this is not enough current to damage most IC's which the 4195 might be supplying, but it is a potentially
destructive condition. Fortunately, it is easy to protect against. As shown in the typical application circuit below, a diode, D, can be connected to the negative output.
If a small signal silicon diode is used, it will clamp the negative output voltage at about +0.55 V . A Schottky barrier or germanium device would clamp the voltage at about +0.3 V . Another cure which will keep the negative output negative at all times is the 1 Mohm resistor connected between the +15 V output and the C- terminal. This resistor will then supply drive to the negative output transistor, $\mathrm{Q}_{1}$, causing it to saturate to $-\mathrm{V}_{1}$ during the brownout.


## HEATSINKING FOR 4194 AND 4195

Voltage Regulators are power devices which are used in a wide range of applications.
When operating these devices near their extremes of load current, ambient temperature and input-output differential, consideration of package dissipation becomes important to avoid thermal shutdown at $175^{\circ} \mathrm{C}$. Both the 4194 and 4195 have this feature to prevent damage to the device. It typically starts affecting load regulation approximately $2^{\circ} \mathrm{C}$ below $175^{\circ} \mathrm{C}$.
${ }^{*}$ To avoid shutdown, some form of heatsinking should be used or one of the above operating conditions would need to be derated.

The following is the basic equation for junction temperature:

$$
\begin{equation*}
T_{j}=T_{A}+P_{D} \theta_{j-A} \tag{1}
\end{equation*}
$$

where $\quad \mathrm{T}_{\mathrm{j}}=$ junction temperature $\left({ }^{\circ} \mathrm{C}\right)$
$\mathrm{T}_{\mathrm{A}}=$ ambient air temperature $\left({ }^{\circ} \mathrm{C}\right)$
$P_{D} \quad=$ power dissipated by device (W)
$\theta_{\mathrm{j}-\mathrm{A}}=$ thermal resistance from junction to ambient air ( ${ }^{\circ} \mathrm{C} / \mathrm{W}$ )
The power dissipated by the voltage regulator can be detailed as follows:

$$
\begin{equation*}
P_{D}=\left(V_{I N}-V_{O U T}\right) \times I_{O}+V_{I N} \times I_{Q} \tag{2}
\end{equation*}
$$

where $V_{\text {IN }}=$ input voltage
VOUT $=$ regulated output voltage
$I_{\mathrm{O}}=$ load current
IQ = quiescent current drain
*In allowing for process deviations, the user should work with a maximum allowable function temperature of $150^{\circ} \mathrm{C}$.

Let's look at an application where a user is trying to determine whether the RM4194 in a high temperature environment will need a heatsink.
Given: $\mathrm{T}_{\mathrm{j}}$ at thermal shutdown $\mid \mathrm{V}_{\mathrm{IN}}=40 \mathrm{~V}$

$$
\begin{aligned}
& =150^{\circ} \mathrm{C} \\
& \mathrm{~T}_{\mathrm{A}}=125^{\circ} \mathrm{C} \\
& \theta_{\mathrm{j}-\mathrm{A}}=41.6^{\circ} \mathrm{C} / \mathrm{W}, \mathrm{TK} \\
& V_{\text {OUT }}=30 \mathrm{~V} \\
& I_{Q}=1 \mathrm{~mA}+75 \mu \mathrm{~A} / \\
& \text { VOUT } \times 30 \mathrm{~V} \\
& \text { (TO-66) pkg. } \\
& =3.25 \mathrm{~mA} \text { (1) }
\end{aligned}
$$ (see data sheet)

$$
\begin{aligned}
& \theta_{j-A}={ }^{T_{j}-T_{A}} P_{D} \\
& P_{D}={ }_{T_{j}-T_{A}}^{\theta_{j A}}=\left(V_{I N}-V_{O U T}\right) \times I_{O}+V_{I N} \times I_{Q}
\end{aligned}
$$

Solve for 10 ,

$$
\begin{aligned}
\mathrm{I}_{\mathrm{O}} & =\frac{T_{\mathrm{j}}-T_{A}}{\theta_{\mathrm{j}-\mathrm{A}}\left(\mathrm{~V}_{\text {IN }}-V_{O U T}\right)}-\frac{V_{I N} \times I_{Q}}{\left(V_{I N}-V_{O U T}\right)} \\
\mathrm{I}_{\mathrm{O}} & =\frac{50^{\circ} \mathrm{C}-125^{\circ} \mathrm{C}}{41.6^{\circ} \mathrm{C} / \mathrm{W} \times 10 \mathrm{~V}}-\frac{40 \times 3.25 \times 10^{-3}}{10} \\
& =50 \mathrm{~mA}-13 \mathrm{~mA} \simeq 47 \mathrm{~mA}
\end{aligned}
$$

If this supply current does not provide at least a $10 \%$ margin under worst case load conditions, heatsinking should be employed. If reliability is of prime importance, the multiple regulator approach should be considered.

In equation 1, $\theta_{\mathrm{j}-\mathrm{A}}$ can be broken into the following components:

$$
\theta_{\mathrm{j}-\mathrm{A}}=\theta_{\mathrm{j}-\mathrm{c}}+\theta_{\mathrm{C}-\mathrm{s}}+\theta_{\mathrm{s}-\mathrm{A}}
$$

where $\theta_{\mathrm{j}-\mathrm{c}}=$ junction-to-case thermal resistance
$\theta_{\text {c-s }}=$ case-to-heatsink thermal resistance
$\theta_{\mathrm{S}-\mathrm{A}}=$ heatsink-to-ambient thermal resistance

In the above example, let's say that the user's load current is 200 mA and he wants to calculate the combined $\theta_{\mathrm{c}-\mathrm{s}}$ and $\theta_{\mathrm{s}-\mathrm{A}}$ he needs:
Given: $10=200 \mathrm{~mA}$,

$$
\begin{aligned}
\theta_{\mathrm{j}-\mathrm{A}} & =\frac{\mathrm{T}_{\mathrm{j}}-\mathrm{T}_{\mathrm{A}}}{\left(\mathrm{~V}_{\text {IN }}-V_{O U T}\right) \times \mathrm{IO}_{\mathrm{O}}+\mathrm{V}_{\text {IN }} \times \mathrm{I}_{\mathrm{Q}}} \\
& =\frac{50^{\circ} \mathrm{C}-125^{\circ} \mathrm{C}}{10 \mathrm{~V} \times 200 \mathrm{~mA}+40 \times 3.25 \times 10^{-3}} \\
& =11.75^{\circ} \mathrm{C} / \mathrm{W}
\end{aligned}
$$

[^4]Given: $\quad \theta_{\mathrm{j}-\mathrm{c}}=7.15^{\circ} \mathrm{C} / \mathrm{W}$ for the 4194 in the TK package,

$$
\theta_{\mathrm{c}-\mathrm{s}}+\theta_{\mathrm{S}-\mathrm{A}}=11.75^{\circ} \mathrm{C} / \mathrm{W}-7.15^{\circ} \mathrm{C} / \mathrm{W}=4.6^{\circ} \mathrm{C} / \mathrm{W}
$$

When using heatsink compound with a metal-to-metal interface, a typical $\theta_{\mathrm{c}-\mathrm{s}}=0.5^{\circ} \mathrm{C} / \mathrm{W}$ for the TK package. The remain-
ing $\theta_{\mathrm{S}}$ - of approximately $4^{\circ} \mathrm{C} / \mathrm{W}$ is a large enough thermal resistance to be easily provided by a number of heatsinks currently available. Table 1 is a brief selection guide to heatsink manufacturers.

## TABLE 1

Commercial Heatsink Selection Guide
No attempt has been made to provide a complete list of all heatsink manufacturers. This list is only representative.

| TO-3 AND TO-66 |  |
| :---: | :---: |
| $\theta \mathbf{S A} *\left({ }^{\circ} \mathrm{C} / \mathrm{W}\right)$ | Manufacturer/Series or Part Number |
| 0.3-1.0 | Thermalloy - 6441, 6443, 6450, 6470, 6560, 6590, 6660, 6690 |
| 1.0-3.0 | Wakefield - 641 <br> Thermalloy - 6123, 6135, 6169, 6306, 6401, 6403, 6421, 6423, 6427, 6442, 6463, 6500 |
| 3.0-5.0 | Wakefield - 621, 623 <br> Thermalloy - 6606, 6129, 6141, 6303 <br> IERC - HP <br> Staver - V3-3-2 |
| 5.0-7.0 | Wakefield - 690 <br> Thermalloy - 6002, 6003, 6004, 6005, 6052, 6053, 6054, 6176, 6301 <br> IERC - LB <br> Staver - V3-5-2 |
| 7.0-10.0 | Wakefield - 672 <br> Thermalloy - 6001, 6016, 6051, 6105, 6601 <br> IERC - LA, uP <br> Staver - V1-3, V1-5, V3-3, V3-5, V3-7 |
| 10.0-25.0 | Thermalloy - 6013, 6014, 6015, 6103, 6104, 6105, 6117 |
| TO-99 |  |
| 12.0-20.0 | Wakefield - 260 <br> Thermalloy - 1101, 1103 Staver - V3A-5 |
| 20.0-30.0 | ```Wakefield - 209 Thermalloy - 1116, 1121, 1123, 1130, 1131, 1132, 2227, 3005 IERC - LP Staver - F5-5``` |
| 30.0-50.0 | $\begin{aligned} & \text { Wakefield - } 207 \\ & \text { Thermalloy - 2212, 2215, 225, 2228, 2259, 2263, } 2264 \\ & \text { Staver - F5-5, F6-5 } \end{aligned}$ |
|  | $\begin{aligned} & \text { Wakefield - 204, 205, } 208 \\ & \text { Thermalloy - 1115, 1129, 2205, 2207, 2209, 2210, 2211, 2226, 2230, 2257, 2260, } 2262 \\ & \text { Staver - F1-5, F5-5 } \end{aligned}$ |
| CASE 199, CASE 313 |  |
| 10.0-15.0 | $\begin{aligned} & \text { Thermallov - 6030, } 6032,6034 \\ & \text { Staver - V4-3-192, V-5-1 } \end{aligned}$ |
| 15.0-20.0 | $\begin{aligned} & \text { Thermalloy }-6106 \\ & \text { Staver - V4-3-128, V6 } \end{aligned}$ |
| 20.0-30.0 | Wakefield - 295 <br> Thermalloy - 6025, 6107 |

## TABLE 1 Commercial Heatsink Selection Guide (Cont.)

|  |  | DUAL-INLINE-PIN ICS |  |
| :---: | :--- | :--- | :---: |
| $\theta$ SA* $\left({ }^{\circ} \mathbf{C} /\right.$ W $)$ |  | Manufacturer/Series or Part Number |  |
| 20 | Thermalloy -6007 |  |  |
| 30 | Thermalloy -6010 |  |  |
| 32 | Thermalloy -6011 |  |  |
| 34 | Thermalloy -6012 |  |  |
| 45 | IERC - LIC |  |  |
| 60 | Wakefield -650,651 |  |  |

*All values are typical as given by mfgr. or as determined from characteristic curves supplied by manufacturer.

Staver Co., Inc.: 41-51 N. Saxon Ave., Bay Shore, NY 11706
IERC: 135 W. Magnolia Blvd., Burbank, CA 91502
Thermalloy: P.O. Box 34829, 2021 W. Valley View Ln., Dallas, TX
Wakefield Engin Ind: Wakefield, MA 01880


## SECTION 4

Voltage References

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Precision Reference

## GENERAL DESCRIPTION

The LM129 and LM329 family are precision multicurrent temperature compensated 6.9 V zener references with dynamic impedances a factor of 10 to 100 less than discrete diodes. Constructed in a single silicon chip, the LM129 uses active circuitry to buffer the internal zener allowing the device to operate over a 0.5 mA to 15 mA range with virtually no change in performance. The LM129 and LM329 are available with selected temperature coefficients of $0.001,0.002,0.005$ and $0.01 \% /{ }^{\circ} \mathrm{C}$. These new references also have excellent long term stability and low noise.

A new subsurface breakdown zener used in the LM129 gives lower noise and better long term stability than conventional IC zeners. Further the zener and temperature compensating transistor are made by a planar process so they are immune to problems that plague ordinary zeners. For example, there is virtually no voltage shifts in zener voltage due to temperature cycling and the device is insensitive to stress on the leads. The LM129 can be used in place of conventional zeners with im-
proved performance. The low dynamic impedance simplifies biasing and the wide operating current allows the replacement of many zener types.
The LM129 is packaged in a 2-lead TO-46 package and is rated for operation over a $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ temperature range. The LM329 for operation over $0-70^{\circ} \mathrm{C}$ is available in both a hermetic TO-46 package and a TO-92 epoxy package.

## DESIGN FEATURES

- 0.6 mA to 15 mA operating current
- $0.6 \Omega$ dynamic impedance at any current
- Available with temperature coefficients of $0.001 \% /{ }^{\circ} \mathrm{C}$
- $7 \mu \mathrm{~V}$ wideband noise
- $5 \%$ initial tolerance
- 0.002\% long term stability
- Low cost

SCHEMATIC DIAGRAMS


CONNECTION INFORMATION


## ABSOLUTE MAXIMUM RATINGS



ELECTRICAL CHARACTERISTICS
(Note 1)

| PARAMETER | CONDITIONS | LM129A, B, C |  |  | LM329B, C, D |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Reverse Breakdown Voltage | $\begin{aligned} & \mathrm{T}_{A}=25^{\circ} \mathrm{C}_{1} \\ & 0.6 \mathrm{~mA} \leqslant \mathrm{I}_{\mathrm{R}} \leqslant 15 \mathrm{~mA} \end{aligned}$ | 6.7 | $6.9$ | 7.2 | 6.55 | 6.9 | 7.25 | V |
| Reverse Breakdown Change with Current | $\begin{aligned} & \mathrm{T}_{A}=25^{\circ} \mathrm{C}, \\ & 0.6 \mathrm{~mA} \leqslant \mathrm{I}_{\mathrm{R}} \leqslant 15 \mathrm{~mA} \end{aligned}$ |  | 9 | $14$ |  | 9 | 20 | mV |
| Reverse Dynamic Impedance | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{I}_{\mathrm{R}}=1 \mathrm{~mA}$ |  | 0.6 | - 1 |  | 0.8 | 2 | $\Omega$ |
| RMS Noise | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \\ & 10 \mathrm{~Hz} \leqslant \mathrm{~F} \leqslant 10 \mathrm{kHz} \end{aligned}$ |  | 7 | 20 |  | 7 | 100 | $\mu \mathrm{V}$ |
| Long Term Stability | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=45^{\circ} \mathrm{C} \pm 0.1^{\circ} \mathrm{C}, \\ & \mathrm{I}_{\mathrm{R}}=1 \mathrm{~mA} \pm 0.3 \% \end{aligned}$ |  | $20$ |  |  | 20 |  | ppm |
| Temperature Coefficient <br> LM129A | $\mathrm{I}_{\mathrm{R}}=1 \mathrm{~mA}$ |  | 6 | 10 |  |  |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| LM129B, LM329B |  |  | 15 | 20 |  | 15 | 20 |  |
| LM129C, LM329C |  |  | 30 | 50 |  | 30 | 50 |  |
| LM329D |  |  |  |  |  | 50 | 100 |  |
| Change In Reverse Breakdown Temperature Coefficient | $1 \mathrm{~mA} \leqslant \mathrm{I}_{\mathrm{R}} \leqslant 15 \mathrm{~mA}$ |  | 1 |  |  | 1 |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| Reverse Breakdown Change with Current | $1 m A \leqslant / R \leqslant 15 m A$ |  | 12 |  |  | 12 |  | mV |
| Reverse Dynamic Impedance | $1 \mathrm{~mA} \leqslant 1 \mathrm{R} \leqslant 15 \mathrm{~mA}$ |  | 0.8 |  |  | 1 |  | $\Omega$ |

## NOTE:

1. These specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for the LM129 and $0^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+70^{\circ} \mathrm{C}$ for the LM329 unless otherwise specified.

## TYPICAL PERFORMANCE CHARACTERISTICS



## TYPICAL APPLICATIONS



External Reference for Temperature Transducer


## TYPICAL APPLICATIONS (Cont.)



## GENERAL DESCRIPTION

The LM199/LM399 are precision, temperature-stabilized monolithic zeners offering temperature coefficients a factor of ten better than high quality reference zeners. Constructed on a single monolithic chip is a temperature stabilizer circuit and an active reference zener. The active circuitry reduces the dynamic impedance of the zener to about $0.5 \Omega$ and allows the zener to operate over 0.5 mA to 10 mA current range with essentially no change in voltage or temperature coefficient. Further, a new subsurface zener structure gives low noise and excellent long term stability compared to ordinary monolithic zeners. The package is supplied with a thermal shield to minimize heater power and improve temperature regulation.
The LM199 series references are exceptionally easy to use and free of the problems that are often experienced with ordinary zeners. There is virtually no hysteresis in reference voltage with temperature cycling. Also, the LM199 is free of voltage shifts due to stress on the leads. Finally, since the unit is temperature stabilized, warm up time is fast.

The LM199 can be used in almost any application in place of ordinary zeners with improved performance. Some ideal applications are analog to digital converters, calibration standards, precision voltage or current sources or precision power
supplies. Further in many cases the LM199 can replace references in existing equipment with a minimum of wiring changes.
The LM199 series devices are packaged in a standard hermetic TO-46 package inside a thermal shield. The LM199 is rated for operation from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ while the LM299 is rated for operation from $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ and the LM399 is rated from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Guaranteed $0.0001 \% /{ }^{\circ} \mathrm{C}$ temperature coefficient
- Low dynamic impedance $-0.5 \Omega$
- Initial tolerance on breakdown voltage $-2 \%$
- Sharp breakdown at $400 \mu \mathrm{~A}$
- Wide operating current $-500 \mu \mathrm{~A}$ to 10 mA
- Wide supply range for temperature stabilizer
- Guaranteed low noise
- Low power for stabilization -300 mW at $25^{\circ} \mathrm{C}$
- Long term stability - 20 ppm


## SCHEMATIC DIAGRAMS



## CONNECTION INFORMATION



FUNCTIONAL BLOCK DIAGRAM


## ABSOLUTE MAXIMUM RATINGS



## ELECTRICAL CHARACTERISTICS (Note 2)

| PARAMETER | CONDITIONS |  | LM199, LM299 |  |  | LM399 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | - TYP | MAX | MIN | TYP | MAX |  |
| Reverse Breakdown Voltage | $0.5 \mathrm{~mA} \leqslant \mathrm{I}_{\mathrm{R}} \leqslant 10 \mathrm{~mA}$ |  | 6.8 | 695 | 7.1 | 6.6 | 6.95 | 7.3 | V |
| Reverse Breakdown Voltage Change With Current | $0.5 \mathrm{~mA} \leqslant 1 \leqslant 10 \mathrm{~mA}$ |  |  | 6 | \% 9 |  | 6 | 12 | mV |
| Reverse Dynamic Impedance | $1 \mathrm{R}=1 \mathrm{~mA}$ |  |  | . 0.5 | 1 |  | 0.5 | 1.5 | $\Omega$ |
| Reverse Breakdown <br> Temperature Coefficient | $\left.\begin{array}{l} -55^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 85^{\circ} \mathrm{C} \\ 85^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 125^{\circ} \mathrm{C} \end{array}\right\} \quad \mathrm{LM} 199$ |  | , | 0.00003 | 0.0001 |  |  |  | \%/ ${ }^{\circ} \mathrm{C}$ |
|  |  |  |  | 0.0005 | 0.0015 |  |  |  |  |
|  | $\begin{aligned} & -25^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{\mathrm{A}} \leqslant 85^{\circ} \mathrm{C} \\ & 0^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{\mathrm{A}} \leqslant 70^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ | LM299 |  | 0.00003 | 0.0001 |  |  |  |  |
|  |  | LM399 |  | , |  |  | 0.00003 | 0.0002 |  |
| RMS Noise | $10 \mathrm{~Hz} \leqslant \mathrm{f} \leqslant 10 \mathrm{kHz}$ |  |  | 7 | 20 |  | 7 | 50 | $\mu \mathrm{V}$ |
| Long Term Stability | Stabilized, $22^{\circ} \mathrm{C} \leqslant T_{\mathrm{A}} \leqslant 28^{\circ} \mathrm{C}$, <br> 1000 Hours, $I_{R}=1 \mathrm{~mA} \pm 0.1 \%$ |  |  | 20 |  |  | 20 |  | ppm |
| Temperature Stabilizer Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Still Air, $\mathrm{V}_{\text {S }}=30 \mathrm{~V}$ |  |  | 8.5 | 14 |  | 8.5 | 15 | mA |
|  | $\mathrm{T}_{\mathrm{A}}=-55^{\circ} \mathrm{C}$ / ${ }_{\text {a }}$ |  |  | 22 | 28 |  |  |  |  |
| Temperature Stabilizer Supply Voltage (Note 3) | * |  | 9 |  | 40 | 9 |  | 40 | V |
| Warm-Up Time to 0.05\% | $\mathrm{V}_{\mathrm{S}}=30 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  |  | 3 |  |  | 3 |  | Seconds |
| Initial Turn-on Current | $9 \leqslant V_{S} \leqslant 40 . T_{A}=25$ |  |  | 140 | 200 |  | 140 | 200 | mA |

## NOTES:

1. The substrate is electrically connected to the negative terminal of the temperature stabilizer. The voltage that can be applied to either terminal of the reference is 40 V more positive or 0.1 V more negative than the substrate.
2. These specifications apply for 30 V appried to the temperature stabilizer and $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$ for the $\mathrm{LM} 199 ;-25^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$ for the LM299 and $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 770^{\circ} \mathrm{C}$ for the LM399.
3. CAUTION. If the device is operated for more than 60 seconds with heater supply voltage between 2 V and 9 V the heater temperature control circuitry is not properly blased and the device can rise to approximately $+150^{\circ} \mathrm{C}$.

## TYPICAL PERFORMANCE CHARACTERISTICS



## TYPICAL APPLICATIONS



## TYPICAL APPLICATIONS (Cont.)



## TYPICAL APPLICATIONS (Cont.)

OV to 20V Power Reference


Bipolar Output Reference


## GENERAL DESCRIPTION

The LM199A/LM299A/LM399A are precision, temperaturestabilized monolithic zeners offering temperature coefficients a factor of ten better than high quality reference zeners. Constructed on a single monolithic chip is a temperature stabilizer circuit and an active reference zener. The active circuitry reduces the dynamic impedance of the zener to about $0.5 \Omega$ and allows the zener to operate over 0.5 mA to 10 mA current range with essentially no change in voltage or temperature coefficient. Further, a new subsurface zener structure gives low noise and excellent long term stability compared to ordinary monolithic zeners. The package is supplied with a thermal shield to minimize heater power and improve temperature regulation.

The LM199A series references are exceptionally easy to use and free of the problems that are often experienced with ordinary zeners. There is virtually no hysteresis in reference voltage with temperature cycling. Also, the LM199A is free of voltage shifts due to stress on the leads. Finally, since the unit is temperature stabilized, warm up time is fast.

The LM199A can be used in almost any application in place of ordinary zeners with improved performance. Some ideal applications are analog to digital converters, calibration standards, precision voltage or current sources or precision power supplies.

Further in many cases the LM199A can replace references in existing equipment with a minimum of wiring changes.
The LM199A series devices are packaged in a standard hermetic TO-46 package inside a thermal shield. The LM199 is rated for operation from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ while the LM299A is rated for operation from $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ and the LM399A is rated from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Guaranteed $0.00005 \%$ © temperature coefficient
- Low dynamic impedance $-0.5 \Omega$
- Initial tolerance on breakdown voltage $-2 \%$
- Sharp breakdown at $400 \mu \mathrm{~A}$
- Wide operating current - $500 \mu \mathrm{~A}$ to 10 mA
- Wide supply range for temperature stabilizer
- Guaranteed low noise
- Low power for stabilization -300 mW at $25^{\circ} \mathrm{C}$
- Long term stability - 20 pm


## SCHEMATIC DIAGRAMS



## CONNECTION INFORMATION



FUNCTIONAL BLOCK DIAGRAM


## ABSOLUTE MAXIMUM RATINGS



## ELECTRICAL CHARACTERISTICS

| PARAMETER | CONDITIONS | LM199A/LM299A |  |  | LM399A |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Reverse Breakdown Voltage | $0.5 \mathrm{~mA} \leqslant 1 \mathrm{R} \leqslant 10 \mathrm{~mA}$ | 6.8 | 6.95 | 7.1 | 6.6 | 6.95 | 7.3 | V |
| Reverse Breakdown Voltage Change With Current | $0.5 \mathrm{~mA} \leqslant 1 \leqslant 10 \mathrm{~mA}$ |  |  | - 9 |  | 6 | 12 | mV |
| Reverse Dynamic Impedance | $1 \mathrm{R}=1 \mathrm{~mA}$ |  | 0.5 | 1 |  | 0.5 | 1.5 | $\Omega$ |
| Reverse Breakdown <br> Temperature Coefficient | $\begin{aligned} & -55^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 85^{\circ} \mathrm{C} \\ & 85^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{\mathrm{A}} \leqslant 125^{\circ} \mathrm{C} \end{aligned}$ |  | 0.00002 | 0.00005 |  |  |  | \%/ ${ }^{\circ} \mathrm{C}$ |
|  |  |  | 0.0005 | 0.0010 |  |  |  |  |
|  | $-25^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 85^{\circ} \mathrm{C}$ LM299A <br> $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 70^{\circ} \mathrm{C}$ 1 M 399 A |  | 0.00002 | 0.00005 |  |  |  |  |
|  |  |  |  |  |  | 0.00003 | 0.0001 |  |
| RMS Noise | $10 \mathrm{~Hz} \leqslant \mathrm{f} \leqslant 10 \mathrm{kHz}$ |  | 7 | 20 |  | 7 | 50 | $\mu \mathrm{V}$ |
| Long Term Stability | $\begin{aligned} & \text { Stabilized, } 22^{\circ} \mathrm{C} \leqslant \mathrm{~T}_{A} \leqslant 28^{\circ} \mathrm{C} \text {, } \\ & 1000 \text { Hours, } I_{R}=1 \mathrm{~mA}=0.1 \% \end{aligned}$ |  | 20 |  |  | 20 |  | ppm |
| Temperature Stabilizer Supply Current | $\begin{aligned} & T_{A}=25^{\circ} \mathrm{C}, \text { Still Air, } \mathrm{V}_{\mathrm{S}}=30 \mathrm{~V} \\ & \mathrm{~T}_{\mathrm{A}}=-55^{\circ} \mathrm{C} \end{aligned}$ |  | 8.5 | 14 |  | 8.5 | 15 | mA |
|  |  |  | 22 | 28 |  |  |  |  |
| Temperature Stabilizer Supply Voltage (Note 3) |  | 9 |  | 40 | 9 |  | 40 | V |
| Warm-Up Time to 0.05\% | $V_{S}=30 \mathrm{~V}, \mathrm{TA}-25^{\circ} \mathrm{C}$ |  | 3 |  |  | 3 |  | Seconds |
| Initial Turn-on Current | $9 \leqslant V_{S} \leqslant 40, T_{A}=25^{\circ} \mathrm{C}$ |  | 140 | 200 |  | 140 | 200 | mA |

## NOTES:

1. The substrate is electrically eomnected to the eqative terminal of the temperature stabilizer. The voltage that can be applied to either terminal of the reference is 40 V more positive or 0.1 V more negative than the substrate.
2. These specifications apply for 30 V aplited to the temperature stabilizer and $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+125^{\circ} \mathrm{C}$ for the LM199A; $-25^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+85^{\circ} \mathrm{C}$ for the LM299A and $0^{\circ} \mathrm{C}$ § T A = $470^{\circ} \mathrm{C}$ for the LM399A.
3. CAUTION. If the delve is operated for more than 60 seconds with heater supply voltage between 2 V and SV the heater temperature controi circuitry is not properfy biased and the device can rise to approximately $+150^{\circ} \mathrm{C}$.

## TYPICAL APPLICATIONS

For typical applications, see 199 data sheet beginning on page 4-7.

## TYPICAL PERFORMANCE CHARACTERISTICS




## SECTION 5

## Comparators

## CONTENTS

111, 211, 311 Precision Voltage Comparators ..... 5-2
139, 239, 339, 2901, 3302 Quad Single-Supply ..... 5-4
Comparators
710 High-Speed Differential ..... 5-8
Voltage Comparator
2111, 2211, 2311 Dual Precision Voltage ..... 5-10
Comparators

## GENERAL DESCRIPTION

The LM111, LM211, and LM311 are voltage comparators with about one-thousandth the input current of the LM106 and LM107. These comparators are designed to operate from standard $\pm 15 \mathrm{~V}$ operational amplifier supplies to a single +5 V supply used for IC logic. Their outputs are compatible with DTL, RTL, TTL, and MOS devices. Offset balancing is provided, and the outputs can be OR wired.
The LM111 operates over the full military temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The LM211 is the same as the LM111 except its performance is guaranteed from $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. The LM311 is the commercial version which operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Input Current 150nA Maximum
- Operates from +5 V Supply
- Offset Current 20nA Maximum


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Total Supply Voltage (V84) . . . . . . . . . . . . . . . . 36V |  |
| :---: | :---: |
| Output to Negative Supply ( $\mathrm{V}_{74}$ ) . . LM111/LM211: 50V |  |
|  |  |
| Ground to Negative Supply Voltage ( $\mathrm{V}_{14}$ ) | 30 V |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ |
| Input Voltage (Note 1) | $\pm 15 \mathrm{~V}$ |
| Power Dissipation (Note 2) | 500 mW |

Output to Negative Supply (V74) . . LM111/LM211: 50V LM311: 40V
Ground to Negative Supply Voltage ( $\mathrm{V}_{14}$ ) . . . . . . . 30V
Input Voltage (Note 1) . . . . . . . . . . . . . . . . . . . $\pm 15 \mathrm{~V}$
Power Dissipation (Note 2) . . . . . . . . . . . . . . . 500mW

Output Short-Circuit Duration Operating Temperature Range

M22$0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$Lead Temperature (Soldering, 10s)$300^{\circ} \mathrm{C}$

## ELECTRICAL CHARACTERISTICS (Note 3)

| PARAMETER | CONDITIONS | LM111/211 |  | LM311 |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | TYP | MAX | TYP | MAX |  |
| Input Offset Voltage (Note 4) | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k}$ | 0.7 | 3.0 | 2.0 | 7.5 | mV |
| Input Offset Current (Note 4) | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 4.0 | 10 | 6.0 | 50 | $n A$ |
| Input Bias Current | $\mathrm{TA}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 60 | 100 | 100 | 250 | nA |
| Voltage Gain | $\mathrm{TA}^{\prime}=25^{\circ} \mathrm{C}$ | 200 |  | 200 |  | $\mathrm{V} / \mathrm{mV}$ |
| Response Time (Note 5) | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 200 |  | 200 |  | ns |
| Saturation Voltage | $\mathrm{VIN} \leqslant-5 \mathrm{mV}, \mathrm{IOUT}^{\prime}=50 \mathrm{~mA}, \mathrm{~T}_{\text {A }}=25{ }^{\circ} \mathrm{C}$ | 0.75 | 1.5 | 0.75 | 1.5 | V |
| Strobe On Current | $\mathrm{TA}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 3.0 |  | 3.0 |  | mA |
| Output Leakage Current | $\mathrm{V}_{\text {IN }} \geqslant 5 \mathrm{mV}, \mathrm{V}_{\text {OUT }}=35 \mathrm{~V}, \mathrm{~T}_{\text {A }}=25^{\circ} \mathrm{C}$ | 0.2 | 10 | 0.2 | 50 | nA |
| Input Offset Voltage (Note 4) | RS $\leqslant 50 \mathrm{k}$ |  | 4.0 |  | 10 | mV |
| Input Offset Current (Note 4) |  |  | 20 |  | 70 | nA |
| Input Bias Current |  |  | 150 |  | 300 | nA |
| Input Voltage Range |  | $\pm 14$ |  | $\pm 14$ |  | V |
| Saturation Voltage | $\begin{aligned} & \mathrm{V}^{+} \geqslant 4.5 \mathrm{~V}, \mathrm{~V}^{-}=0, \mathrm{~V}_{\mathrm{IN}} \leqslant-6 \mathrm{mV} \\ & \text { ISINK } \leqslant 8 \mathrm{~mA} \end{aligned}$ | 0.23 | 0.4 | 0.23 | 0.4 | V |
| Output Leakage Current | $\mathrm{V}_{\text {IN }} \geqslant 5 \mathrm{mV}, \mathrm{V}_{\text {OUT }}=35 \mathrm{~V}$ | 0.1 | 0.5 |  |  | $\mu \mathrm{A}$ |
| Positive Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 5.1 | 6.0 | 5.1 | 7.5 | mA |
| Negative Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 4.1 | 5.0 | 4.1 | 5.0 | mA |

## NOTES:

1. This rating applies for $\pm 15 \mathrm{~V}$ supplies. The positive input voltage limit is 30 V above the negative supply. The negative input voltage limit is equal to the negative supply voltage of 30 V below the positive supply, whichever is less.
2. The maximum junction temperature of the LM111 is $150^{\circ} \mathrm{C}$, while that of the LM311 is $+85^{\circ} \mathrm{C}$. For operating at elevated temperatures, devices in the TO-5 package must be derated based on a thermal resistance of $150^{\circ} \mathrm{C} / \mathrm{W}$, junction to ambient, or $45^{\circ} \mathrm{C} / \mathrm{W}$, junction to case. For the flat pack, derate based on a thermal resistance of $185^{\circ} \mathrm{C} / \mathrm{W}$ when mounted on a $1 / 16$-inch-thick epoxy glass board with ten, 0.03 -inch-wide, 2 ounce copper conductors. The thermal resistance of the dual-in-line (DE) package is $100^{\circ} \mathrm{C} / \mathrm{W}$, junction to ambient.
3. These specifications apply for $\mathrm{V}_{S}= \pm 15 \mathrm{~V}$ and $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+125^{\circ} \mathrm{C}$, unless otherwise stated. With the LM 311 , however, all temperature specifications are limited to $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{A} \leqslant+70^{\circ} \mathrm{C}$. The offset voltage, offset current and bias current specifications apply for any supply voltage from a single 5 V supply up to $\pm 15 \mathrm{~V}$ supplies.
4. The offset voltages and offset currents given are the maximum values required to drive the output within a volt of either supply with a 1 mA load. Thus, these parameters define an error band and take into account the worst case effects of voltage gain and input impedance.
5. The response time specified (see definitions) is for a 100 mV input step with 5 mV overdrive.

## GENERAL DESCRIPTION

These devices offer higher frequency operation and faster switching than can be had from internally compensated quad op amps. Intended for single-supply applications, the Darlington PNP input stage allows them to compare voltages that include ground. The two-stage common-emitter output circuit provides gain and output sink capacity of 3.2 mA at an output level of 400 mV . The outpu: collector is left open, permitting the designer to drive devices in the range of 2 V to 36 V .
They are intended for applications not needing response time less than $1 \mu \mathrm{~s}$, but demanding excellent op amp input parameters of offset voltage and current, and bias current, to insure accurate comparison with reference voltage.

## DESIGN FEATURES

- Input Common Mode Voltage Range Includes Ground
- Wide Single Supply Voltage Range, 2 to 36 V
- Output Compatible with TTL, DTL, ECL, MOS and CMOS Logic Systems
- Very Low Supply Current Drain (.8mA) Independent of Supply Voltage

SCHEMATIC DIAGRAM (1/4 shown)


## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

|  | LM139/LM239/LM339 LM139A/LM239A/LM339A LM2901 | LM3302 |
| :---: | :---: | :---: |
| Supply Voltage, $\mathrm{V}^{+}$ | $36 V_{\text {DC }} \sim r^{ \pm} 18 V_{\text {DC }}$ | $28 V_{\text {DC }}$ or $\pm 14 V_{\text {DC }}$ |
| Differential Input Voltage | 36 V DC | 28 V DC |
| Input Voltage | $-0.3 \vee \mathrm{DC}$ to $+36 V^{\text {DC }}$ | -0.3 $V^{\text {DC }}$ to $+28 \vee \mathrm{VC}$ |
| Power Dissipation (Note 1) |  |  |
| Molded DIP | 570 mW | 570 mW |
| Cavity DIP | 900 mW |  |
| Flat Pack | 800 mW |  |
| Output Short-Circuit to GND, (Note 2) | Continuous | Continuous |
| Input Current ( $\mathrm{V}_{\text {IN }}<-0.3 \mathrm{~V}_{\mathrm{DC}}$ ), ( Note 3) | 50 mA | 50 mA |
| Operating Temperature Range |  | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| LM339A | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |  |
| LM239A | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  |
| LM139A | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |  |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 seconds) | $300^{\circ} \mathrm{C}$ | $300^{\circ} \mathrm{C}$ |

ELECTFICAL CHARACTERISTICS $\left(\mathrm{V}^{+}=5 \mathrm{~V}_{\mathrm{DC}}\right.$, Note 4$)$

| PARAMIETER | CONDITIONS | LM139A |  |  | LM239A, LM339A |  |  | LM139 |  |  | LM239, LM339 |  |  | LM2901 |  |  | LM3302 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Note 9) |  | $\pm 1.0$ | $\pm 2.0$ |  | $\pm 1.0$ | $\pm 2.0$ |  | . $\pm 2.0$ | $\pm 5.0$ |  | $\pm 2.0$ | $\pm 5.0$ |  | $\pm 2.0$ | $\pm 7.0$ |  | $\pm 3$ | $\pm 20$. | mV VC |
| Input Bias Current | $\operatorname{IIN}(+)$ or IIN(-) with Output in Linear Range, $T_{A}=25^{\circ} \mathrm{C}$, (Note 5 ) |  | 25 | 100 |  | 25 | 250 |  | 25 | 100 |  | 25 | 250 |  | 25 | 250 |  | 25 | 500 | nADC |
| Input Offset Current | $\operatorname{IIN}(+)-\operatorname{IIN}(-), T_{A}=25^{\circ} \mathrm{C}$ |  | $\pm 3.0$ | $\pm 25$ |  | $\pm 5.0$ | $\pm 50$ |  | $\pm 3.0$ | $\pm 25$ |  | $\pm 5.0$ | $\pm 50$ |  | $\pm 5$ | $\pm 50$ |  | $\pm 3$. | $\pm 100$ | nADC |
| Input Common-Mode Voltage Rançe | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, (Note 6) | 0 |  | $\mathrm{v}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | 0 |  | $\mathrm{v}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | 0 |  | $\mathrm{V}^{+}-1.5$ | $V D C$ |
| Supply Current | $\mathrm{R}_{\mathrm{L}}=\infty$ on all Comparators, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 0.8 | 2.0 |  | 0.8 | 2.0 |  | 0.8 | 2.0 |  | 0.8 | 2.0 |  | 0.8 | 1.0 |  | 0.8 | 2 | mADC |
|  | $\mathrm{R}_{\mathrm{L}}=\infty, \mathrm{V}^{+}=30 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 | 2.5 |  |  |  |  |
| Voltage Gain | $\begin{aligned} & R_{L} \geqslant 15 \mathrm{k} \Omega, \mathrm{~V}^{+}=15 \mathrm{~V}_{\mathrm{DC}}\left(\mathrm{To}_{0}\right. \\ & \text { Support Large } \mathrm{V}_{\mathrm{O}} \text { Swing), } \mathrm{T}_{A}=25^{\circ} \mathrm{C} \end{aligned}$ | 50 | 200 |  | 50 | 200 |  |  | 200 |  |  | 200 |  | 25 | 100 | - | 2 | 30 |  | $\mathrm{V} / \mathrm{mV}$ |
| Large Signal Response Time | $\begin{aligned} & V_{I N}=T T L \text { Logic Swing, } V_{R E F}= \\ & 1.4 \vee D C, V_{R L}=5 \mathrm{VDC}, R_{L}=5.1 \mathrm{kS}, \\ & T_{A}=25^{\circ} \mathrm{C} . \end{aligned}$ |  | 300 |  |  | 300 |  |  | 300 |  |  | 300 |  |  | 300 |  |  | 300 |  | ns |
| Response Time | $\begin{aligned} & V_{R L}=5 V_{D C,} R_{L}=5.1 \mathrm{k} \Omega, \\ & T_{A}=25^{\circ} \mathrm{C},(\text { Note } 7) \end{aligned}$ |  | 1.3 |  |  | 1.3 |  |  | 1.3 |  |  | 1.3 |  |  | 1.3 |  |  | 1.3 |  | $\mu \mathrm{s}$. |
| Output Sink Current | $\begin{aligned} & V_{I N(-) \geqslant 1} \geqslant V_{D C}, V_{I N(+)}=0, \\ & V_{O} \leqslant 1.5 \vee_{D C}, T_{A}=25^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ | 6.0 | 16 |  | 6.0 | 16 |  | 6.0 | 16 |  | 6.0 | 16 |  | 6.0 | 16 |  | 2.0 | 16 |  | mADC |
| Saturation Voltage | $\begin{aligned} & V_{I N(-)} \geqslant 1 \mathrm{VDC}_{\mathrm{DC}}, V_{I N(+)}=0, \\ & \mathrm{ISINK} \leqslant 4 \mathrm{~mA}, \mathrm{~T}_{A}=25^{\circ} \mathrm{C} \end{aligned}$ |  | 250 | 400 |  | 250 | 400 |  | 250 | 400 |  | 250 | 400 |  |  | 400 |  | 250 | 500 | $m V_{D C}$ |
| Output Leakage Current | $\begin{aligned} & V_{1 N(+)} \geqslant 1 \mathrm{~V}_{D C}, V_{I N(-)}=0, \\ & V_{O}=5 V_{D C}, T_{A}=25^{\circ} \mathrm{C} \end{aligned}$ |  | 0.1 |  |  | 0.1 |  |  | 0.1 |  |  | 0.1 |  |  | 0.1 |  |  | 0.1 |  | nADC |
| Input Offset Voltage | (Note 9) |  |  | 4.0 |  |  | 4.0 |  |  | 9.0 |  |  | 9.0 |  | 9 | 15 |  |  | 40 | $m V_{D C}$ |
| Input Offset Current | $\ln (+)-\ln (-)$ |  |  | $\pm 100$ |  |  | $\pm 150$ |  |  | $\pm 100$ |  |  | $\pm 150$ |  | 50 | 200 |  |  | 300 . | $n A_{D C}$ |
| Input Bias Current | $\operatorname{liN(+)}$ or IIN(-) with Output in Linear Range |  |  | 300 |  |  | 400 |  |  | 300 |  |  | 400 |  | 200 | 500 |  |  | 1000 | ${ }^{n} A_{D C}$ |
| Input Common-Mode Voltage Range |  | 0 |  | $\mathrm{V}^{+}-2.0$ | 0 |  | $\mathrm{V}^{+}-2.0$ | 0 |  | $\mathrm{V}^{+\ldots 2.0}$ | 0 |  | $\mathrm{V}^{+-2.0}$ | 0 |  | $\mathrm{V}^{+}-2.0$ | 0 |  | $\mathrm{V}^{+}-2.0$ | VDC |
| Saturation Voltage | $\begin{aligned} & V_{I N(-) \geqslant 1 V_{D C}, V_{I N(+)}=0,} \\ & I_{S I N K} \leqslant 4 \mathrm{~mA} \end{aligned}$ |  |  | 700 |  |  | 700 |  |  | 700 |  |  | 700 |  | 400 | 700 |  |  | 700 | $m V_{D C}$ |
| Output Leakage Current | $\begin{aligned} & V_{I N(+)} \geqslant 1 V_{D C}, V_{I N(-)}=0, \\ & V_{O}=30 V_{D C} \end{aligned}$ |  |  | 1.0 |  |  | 1.0 |  |  | 1.0 |  |  | 1.0 |  |  | 1.0 |  |  | 1.0 | $\mu \mathrm{ADC}$ |
| Differential Input Voltage | Keep all $\mathrm{V}_{\mathrm{IN}}{ }^{\prime} \mathrm{s} \geqslant 0 \mathrm{~V}_{\mathrm{DC}}$ (or $\mathrm{V}^{-}$, <br> if used), (Note 8) |  | . | $\mathrm{v}^{+}$ |  |  | $\mathrm{v}^{+}$ |  |  | 36 |  |  | 36 | 0 |  | $\mathrm{v}^{+}$ |  |  | V cc | $V_{D C}$ |

NOTES

1. For operating at high temperatures, the LM339/LM339A, LM2901, LM3302 must be derated based on a $125^{\circ} \mathrm{C}$ maximum junction temperature and a thermal resistance of $175^{\circ} \mathrm{C} / \mathrm{W}$ which applies for the device soldered in a printed circuit board, operating in a still air ambient. The LM239 and LM139 must be derated based on a $150^{\circ} \mathrm{C}$ maxi
Short circuits from the output to $\mathrm{V}^{+}$can cause excessive heating and eventual destruction. The maximum output current is approximately 20 mA independent of the magnitude of $\mathrm{V}^{+}$
2. This input current will only exist when the voltage at any of the input leads is driven negative. It is due to the collector-base junction of the input PNP transistors becoming fofward biased and thereby acting as input diode clamps, in addition to this diode action, there is also lateral NPN parasitic transistor action on the IC chip. This transistor action can cause the output voltages of the comparators to go to the $\mathrm{V}^{+}$voltage level (or to ground for a large overdrive) for the time duration that an input is driven negative. This is not destructive and normal output states will reestablish when the input voltage, which was negative; again returns to a value greater than -0.3 VDC .
3. These specifications apply for $\mathrm{V}^{+}=5 \mathrm{~V}$. temperature specifications are limited to $0^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+70^{\circ} \mathrm{C}$, and the LM2901, LM 3302 temperature range is $-40^{\circ} \mathrm{C} \leqslant T_{A} \leqslant+85^{\circ} \mathrm{C}$
4. The direction of the input current is out of the IC due to the PNP input stage. This current is essentially constant, independent of the state of the output so no loading change exists on the reference or input lines.

6 . The input common-mode voltage or either input signal voltage should not be allowed to go negative by more than 0.3 V . The upper end of the common-mode voltage range is $\mathrm{V}^{+}-1.5 \mathrm{~V}$, but either or bot t inputs can go to +30 VDC without damage
 voltage state must not be less than $-0.3 \mathrm{~V}_{\mathrm{DC}}$ (or $0.3 \mathrm{~V}_{\mathrm{DC}}$ below the magnitude of the negative power supply, if used).
voltage state must not be less than -0.3 VDC (or 0.3 VDC .
10. For input signals that exceed $\mathrm{V}_{\mathrm{C}} \mathrm{C}$, only the overdriven comparator is affected. With a 5 V supply, $\mathrm{V}_{\mathrm{IN}}$ should be limited to 25 V max, and a limiting resistor should be used on all inputs that might exceed the positive supply.

339 TYPICAL APPLICATIONS

## Single Supply $\left(\mathrm{V}^{+}=15 \mathrm{~V}_{\mathrm{DC}}\right)$



ORing the Outputs


One-Shot Multivibrator with Input Lock Out



TTL to MOS Logic Converter



Split Supply $\left(V^{+}=+15 V_{D C} \& V^{-}=-15 V_{D C}\right)$


## GENERAL DESCRIPTION

The RM710 and RC710 integrated circuits are monolithic, high speed, differential voltage comparators. Manufactured by the planar process, component matching is inherent. Characteristic of the devices is low offset voltage and low drift parameters as well as high accuracy and fast response.

These voltage comparators are specially designed for a variety of applications such as high speed A/D converter, memory sense amplifier, zero crossing detector, amplitude discriminator and variable threshold Schmitt trigger.
The RM710 operates over the full military temperature range from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The RC710, commercial equivalent of the RM710, operates over a temperature from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

## DESIGN FEATURES

- Low Offset Voltage and Drift Over Entire Temperature Range
- Fast Response Time
- Output Logic Compatible With All Existing Integrated Logic Forms
- Meets or Exceeds All Environmental Requirements of MIL-S-19500, MIL-STD-202, and MIL-STD-750


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Positive Supply Voltage . . . . . . . . . . . . . . . . . +14V | Operating Temperature Range |
| :---: | :---: |
| Negative Supply Voltage . . . . . . . . . . . . . . . . . -7.0V | RM710 . . . . . . . . . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Peak Output Current . . . . . . . . . . . . . . . . 10.0mA | RC710 . . . . . . . . . . . . . . . . . . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Differential Input Voltage . . . . . . . . . . . . . . . $\pm 5.0 \mathrm{~V}$ | Internal Power Dissipation (Note 1) |
| Input Voltage . . . . . . . . . . . . . . . . . . . . . . $\pm 7.0 \mathrm{~V}$ | TO-5 . . . . . . . . . . . . . . . . . . . . . . . . . . . . 300mW |
| Storage Temperature Range . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ | Flat Package . . . . . . . . . . . . . . . . . . . . 200 mW |
| Lead Temperature (Soldering, 60s) . . . . . . . . $300^{\circ} \mathrm{C}$ |  |

ELECTRICAL CHARACTERISTICS $\left(\mathrm{V}^{+}=12.0 \mathrm{~V}, \mathrm{~V}^{-}=-6.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25{ }^{\circ} \mathrm{C}\right.$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM710 |  |  | RC710 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Input Offset Voltage (Note 3) | $R_{S} \leqslant 200 \Omega$ |  | 0.6 | 2.0 |  | 1.6 | 5.0 | mV |
| Input Offset Current (Note 3) |  |  | 0.75 | 3.0 |  | 1.8 | 5.0 | $\mu \mathrm{A}$ |
| Input Bias Current |  |  | 13 | 20 |  | 16 | 25 | $\mu \mathrm{A}$ |
| Voltage Gain |  | 1250 | 1700 |  | 1000 | 1500 |  | V/V |
| Output Resistance |  |  | 200 |  |  | 200 |  | $\Omega$ |
| Output Sink Current | $\Delta V_{\text {in }} \geqslant 5 \mathrm{mV}, \mathrm{V}_{\text {out }}=0$ | 2.0 | 2.5 |  | 1.6 | 2.5 |  | mA |
| Response Time (Note 2) |  |  | 40 | 60 |  | 40 |  | ns |
| The following specifications apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$. |  |  |  |  | The following specifications apply for $\mathbf{0}^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+70^{\circ} \mathrm{C}$. |  |  |  |
| Input Offset Voltage (Note 3) | RS $\leqslant 200 \Omega$ |  |  | 3.0 |  |  | 0.5 | mV |
| Average Temperature Coefficient of Input Offset Voltage | $\begin{aligned} & \mathrm{RS}=20 \Omega, \mathrm{~T}_{\mathrm{A}}=\text { Low to } \\ & \mathrm{T}_{\mathrm{A}}=\mathrm{High}, \mathrm{R}_{\mathrm{S}}=20 \Omega \end{aligned}$ |  | 3.5 | 10 |  | 5.0 | 20 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ to $\mathrm{T}_{A}=$ Low |  | 2.7 | 10 |  |  |  |  |
| Input Offset Current (Note 3) | $\mathrm{T}_{\mathrm{A}}=+125^{\circ} \mathrm{C}$ |  | 0.25 | 3.0 |  |  |  | $\mu \mathrm{A}$ |
|  | $\mathrm{T}_{\mathrm{A}}=$ Low |  | 1.8 | 7.0 |  |  | 7.5 |  |
| Average Temperature Coefficient of Input Offset Current | $\mathrm{T}_{A}=25^{\circ} \mathrm{C}$ to $\mathrm{T}_{A}=\mathrm{High}$ |  | 5.0 | 25 |  | 15 | 50 | nA/oc |
|  | $\mathrm{T}_{A}=25^{\circ} \mathrm{C}$ to $\mathrm{T}_{A}=$ Low |  | 15 | 75 |  | 24 | 100 |  |
| Input Bias Current | TA $=$ Low |  | 27 | 45 |  | 25 | 40 | $\mu \mathrm{A}$ |
| Input Voltage Range | $\mathrm{V}-=-7.0 \mathrm{~V}$ | $\pm 5.0$ |  |  | $\pm 5.0$ |  |  | V |
| Common Mode Rejection Ratio | $\mathrm{RS}^{5} \leqslant 200 \Omega$ | 80 | 100 |  | 70 | 98 |  | dB |
| Differential Input Voltage Range |  | $\pm 5.0$ |  |  | $\pm 5.0$ |  |  | V |
| Voltage Gain |  | 1000 |  |  | 800 |  |  |  |
| Positive Output Level | $\Delta \mathrm{V}_{\text {in }} \geqslant 5 \mathrm{mV}, 0 \leqslant \mathrm{l}_{\text {out }} \leqslant 5.0 \mathrm{~mA}$ | 2.5 | 3.2 | 4.0 | 2.5 | 3.2 | 4.0 | V |
| Negative Output Level | $\Delta V_{\text {in }} \geqslant 5 \mathrm{mV}$ | -1.0 | -0.5 | 0 | -1.0 | -0.5 | 0 | V |
| Output Sink Current | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=\text { Low, } \Delta \mathrm{V}_{\text {in }} \geqslant 5 \mathrm{mV}, \\ & \mathrm{~V}_{\text {out }}=0 \end{aligned}$ | 0.5 | 2.3 |  | 0.5 |  |  | mA |
|  | $\begin{aligned} & T_{A}^{A}=\text { High, } \Delta V_{\text {in }} \geqslant 5 \mathrm{mV}, \\ & \mathrm{~V}_{\text {out }}=0 \end{aligned}$ | 0.5 | 1.7 |  | 0.5 |  |  |  |
| Positive Supply Current | $\mathrm{V}_{\text {out }} \leqslant 0$ |  | 5.2 | 9.0 |  | 5.2 | 9.0 | mA |
| Negative Supply Current |  |  | 4.6 | 7.0 |  | 4.6 | 7.0 | mA |
| Power Consumption |  |  | 90 | 150 |  | 90 | 150 | mW |

## NOTES:

1. The thermal characteristics are based on a maximum chip temperature of $160^{\circ} \mathrm{C}$. Derate maximum power dissipation of $\mathrm{TO}-5 \mathrm{Can}$ by $6.7 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for $\mathrm{T}_{A} \geqslant 114^{\circ} \mathrm{C}$, and of Flat Pak by $5.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for $\mathrm{T}_{A} \geqslant 103^{\circ} \mathrm{C}$. The ratings apply for $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant+125^{\circ} \mathrm{C}$.
2. The response time specified (see definitions) is for a 100 mV input step with 5 mV overdrive.
3. The input offset voltage and input offset current are specified for a logic threshold voltage as follows: For RM710 grade 1.8 V at $-55^{\circ} \mathrm{C}, 1.4 \mathrm{~V}$ at $+25^{\circ} \mathrm{C}$ and 1.0 V at $+125^{\circ} \mathrm{C}$. For RC 710 grade 1.5 V at $+25^{\circ} \mathrm{C}$ and 1.2 V at $+70^{\circ} \mathrm{C}$.

## GENERAL DESCRIPTION

The LH2111 series of dual voltage comparators are two LM111 type comparators in a single hermetic package. Featuring all the same performance characteristics of the single, these duals offer in addition closer thermal tracking, lower weight, reduced insertion cost and smaller size than two singles. For additional information see the LM111 data sheet and National's Linear Application Handbook.

The LH2111 is specified for operation over the $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ military temperature range. The LH2211 is specified for operation over the $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range. The

LH2311 is specified for operation over the $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ temperature range.

## DESIGN FEATURES

| - Wide operating supply range | $\pm 15 \mathrm{~V}$ to a <br> single +5 V |
| :--- | ---: |
| - Low input currents | 6 nA |
| - High sensitivity | $10 \mu \mathrm{~V}$ |
| - Wide differential input range | $\pm 30 \mathrm{~V}$ |
| - High output drive | $50 \mathrm{~mA}, 50 \mathrm{~V}$ |

## CONNECTION INFORMATION



## AUXILIARY CIRCUITS



## ABSOLUTE MAXIMUM RATINGS



## ELECTRICAL CHARACTERISTICS - each side (Note 3)

| PARAMETER | CONDITIONS | LIMITS |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LH2111 | LH2211 | LH2311 |  |
| Input Offset Voltage (Note 4) | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k}$ | 3.0 | 3.0 | 7.5 | $m \vee \operatorname{Max}$ |
| Input Offset Current (Note 4) | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 10 | 10 | 50 | $n A$ Max |
| Input Bias Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 100 | 100 | 250 | $n A$ Max |
| Voltage Gain | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 200 | 200 | 200 | $\mathrm{V} / \mathrm{mV}$ Typ |
| Response Time (Note 5) | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 200 | 200 | 200 | ns Typ |
| Saturation Voltage | $\begin{aligned} & V_{I N} \leqslant-5 \mathrm{mV}, \mathrm{IOUT}=50 \mathrm{~mA} \\ & \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{aligned}$ | 1.5 | 1.5 | 1.5 | $\checkmark$ Max |
| Strobe On Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 3.0 | 3.0 | 3.0 | mA Typ |
| Output Leakage Current | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}} \geqslant 5 \mathrm{mV}, \mathrm{~V}_{\mathrm{OUT}}=35 \mathrm{~V} \\ & \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{aligned}$ | 10 | 10 | 50 | $n A$ Max |
| Input Offset Voltage (Note 4) | $\mathrm{R}_{\mathrm{S}} \leqslant 50 \mathrm{k}$ | 4.0 | 4.0 | 10 | $m \vee \mathrm{Max}$ |
| Input Offset Current (Note 4) |  | 20 | 20 | 70 | nA Max |
| Input Bias Current |  | 150 | 150 | 300 | nA Max |
| Input Voltage Range |  | $\pm 14$ | $\pm 14$ | $\pm 14$ | $\checkmark$ Typ |
| Saturation Voltage | $\begin{aligned} & \mathrm{V}^{+} \geqslant 4.5 \mathrm{~V}, \mathrm{~V}^{-}=0 \\ & \mathrm{~V}_{\mathrm{IN}} \leqslant-5 \mathrm{mV}, \operatorname{ISINK} \leqslant 8 \mathrm{~mA} \end{aligned}$ | 0.4 | 0.4 | 0.4 | $\checkmark$ Max |
| Positive Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 6.0 | 6.0 | 7.5 | mA Max |
| Negative Supply Current | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 5.0 | 5.0 | 5.0 | mA Max |

## NOTES:

1. This rating applies for $\pm 15 \mathrm{~V}$ supplies. The positive input voltage limit is 30 V above the negative supply. The negative input voltage limit is equal to the negative supply voltage or 30 V below the positive supply, whichever is less.
2. The maximum junction temperature is $150^{\circ} \mathrm{C}$. For operating at elevated temperatures, devices in the flat package, the derating is based on a thermal resistance of $185^{\circ} \mathrm{C} / \mathrm{W}$ when mounted on a $1 / 16$-inch-thick epoxy glass board with 0.03 -inch-wide, 2-ounce copper conductor. The thermal resistance of the dual-in-line package is $100^{\circ} \mathrm{C} / \mathrm{W}$, junction to ambient.
3. These specifications apply for $V_{S}= \pm 15 \mathrm{~V}$ and $-55^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 125^{\circ} \mathrm{C}$ for the $\mathrm{LH} 2111,-25^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 85^{\circ} \mathrm{C}$ for the LH 2211 , and $0^{\circ} \mathrm{C} \leqslant \mathrm{T}_{\mathrm{A}} \leqslant 70^{\circ} \mathrm{C}$ for the LH2311, unless otherwise stated. The offset voltage, offset current and bias current specifications apply for any supply voltage from a single 5 V supply up to $\pm 15 \mathrm{~V}$ supplies. For the $\mathrm{LH} 2311, \mathrm{~V}_{\text {IN }}= \pm 10 \mathrm{mV}$.
4. The offset voltages and offset currents given are the maximum values required to drive the output within a volt of either supply with a 1 mA load. Thus, these parameters define an error band and take into account the worst case effects of voltage gain and input impedance.
5. The response time specified is for a 100 mV input step with 5 mV overdrive.


## SECTION 6

Line Drivers and Receivers

## CONTENTS

1488 Quad Line Driver ..... 6-2
1489/1489A Quad Line Receivers ..... 6-4
9622 Dual Line Receiver ..... 6-6

## DESCRIPTION

The RC1488 is a monolithic quad line driver designed to interface data terminal equipment with data communications equipment in conformance with the specifications of EIA standard number RS-232-C. This standard specifies not only the number and type of interface leads, but also the voltage levels to be used.
The RC1488 and its companion circuit, the RC1489/RC1489A quad line receiver, provide a complete interface system between DTL and TTL logic levels and the RS-232-C defined levels.

## DESIGN FEATURES

- Current Limited Output 10 mA Typical
- Power-off Source Impedance 300 Ohms Minimum
- Simple Slew Rate Control With External Capacitor
- Flexible Operating Supply Range
- Compatible With All DTL and TTL Logic

LOGIC DIAGRAM




## CONNECTION INFORMATION

DB and DC Dual In-line

ABSOLUTE MAXIMUM RATINGS ( $T_{A}=+25^{\circ} \mathrm{C}$ unless otherwise noted)

| RATING | SYMBOL | VALUE | UNIT |
| :--- | :---: | :---: | :---: |
| Power Supply Voltage | $\mathrm{V}^{+}$ | +15 | V |
|  | $\mathrm{~V}^{-}$ | -15 |  |
| Input Signal Voltage | $\mathrm{V}_{\text {in }}$ | $-15 \leqslant \mathrm{~V}_{\text {in }} \leqslant 7.0$ | V |
| Output Signal Voltage | $\mathrm{V}_{\mathrm{O}}$ | $\pm 15$ | V |
| Power Derating (Package Limitation, Ceramic and Plastic Dual In-Line Packages) <br> Derate above $\mathrm{TA}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | $\mathrm{P}_{\mathrm{D}}$ | 1000 | mW |
|  | $1 / \theta_{\mathrm{JA}}$ | 6.7 | $\mathrm{~mW} /{ }^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $\mathrm{TA}_{\mathrm{A}}$ | 0 to +75 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $\mathrm{T}_{\text {stg }}$ | -65 to +175 | ${ }^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS $\quad \mathrm{V}^{+}=+9.0 \pm 1 \% \mathrm{Vdc}, \mathrm{V}^{-}=-9.0 \pm 1 \% \mathrm{Vdc}, \mathrm{T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ unless otherwise noted)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Forward Input Current | IF | $\mathrm{V}_{\text {in }}=0 \mathrm{~V}$ |  | 1.0 | 1.6 | mA |
| Reverse Input Current | $I_{R}$ | $\mathrm{V}_{\text {in }}=+5.0 \mathrm{~V}$ |  |  | 10 | $\mu \mathrm{A}$ |
| Output Voltage High | VOH | $\mathrm{V}_{\text {in }}=0.8 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=3.0 \mathrm{k} \Omega, \mathrm{V}^{+}=+9.0 \mathrm{~V}, \mathrm{~V}^{-=}=-9.0 \mathrm{~V}$ | +6.0 | +7.0 |  | V |
|  |  | $\mathrm{V}_{\text {in }}=0.8 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=3.0 \mathrm{k} \Omega, \mathrm{V}^{+}=+13.2 \mathrm{~V}, \mathrm{~V}-=-13.2 \mathrm{~V}$ | +9.0 | +10.5 |  |  |
| Output Voltage Low | $\mathrm{V}_{\mathrm{OL}}$ | $\mathrm{V}_{\text {in }}=1.9 \mathrm{Vdc}, \mathrm{R}_{\mathrm{L}}=3.0 \mathrm{k} \Omega, \mathrm{V}^{+}=+9.0 \mathrm{~V}, \mathrm{~V}-=-9.0 \mathrm{~V}$ | -6.0 | -7.0 |  | V |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{in}}=1.9 \mathrm{Vdc}, \mathrm{R}_{\mathrm{L}}=3.0 \mathrm{k} \Omega, \mathrm{~V}^{+}=+13.2 \mathrm{~V}, \\ & \mathrm{~V}^{-}=-13.2 \mathrm{~V} \end{aligned}$ | -9.0 | -10.5 |  |  |
| Positive Output Short-Circuit Current | ISC+ |  | $+6.0$ | +10 | +12 | mA |
| Negative Output Short-Circuit Current | ISC- |  | -6.0 | -10 | -12 | mA |
| Output Resistance | $\mathrm{R}_{\mathrm{O}}$ | $\mathrm{V}^{+}=\mathrm{V}^{-}=0,\left\|\mathrm{~V}_{\mathrm{O}}\right\|= \pm 2.0 \mathrm{~V}$ | 300 |  |  | $\Omega$ |
| Positive Supply Current$\left(R_{1}=\infty\right)$ | $1^{+}$ | $\mathrm{V}_{\text {in }}=1.9 \mathrm{Vdc}, \mathrm{V}^{+}=+9.0 \mathrm{~V}$ |  | +15 | +20 | mA |
|  |  | $\mathrm{V}_{\text {in }}=0.8 \mathrm{Vdc}, \mathrm{V}^{+}=+9.0 \mathrm{~V}$ |  | +4.5 | +6.0 |  |
|  |  | $\mathrm{V}_{\text {in }}=1.9 \mathrm{Vdc}, \mathrm{V}^{+}=+12 \mathrm{~V}$ |  | +19 | +25 |  |
|  |  | $\mathrm{V}_{\text {in }}=0.8 \mathrm{Vdc}, \mathrm{V}^{+}=+12 \mathrm{~V}$ |  | +5.5 | +7.0 |  |
|  |  | $\mathrm{V}_{\text {in }}=1.9 \mathrm{Vdc}, \mathrm{V}^{+}=+15 \mathrm{~V}$ |  |  | +34 |  |
|  |  | $\mathrm{V}_{\text {in }}=0.8 \mathrm{Vdc}, \mathrm{V}^{+}=+15 \mathrm{~V}$ |  |  | +12 |  |
| Negative Supply Current$\left(R_{L}=\infty\right)$ | $1-$ | $\mathrm{V}_{\text {in }} 1.9 \mathrm{Vdc}, \mathrm{V}^{-}=-9.0 \mathrm{~V}$ |  | -13 | -17 | mA |
|  |  | $\mathrm{V}_{\text {in }}=0.8 \mathrm{Vdc}, \mathrm{V}^{-}=-9.0 \mathrm{~V}$ |  | 0 | 0 |  |
|  |  | $\mathrm{V}_{\text {in }}=1.9 \mathrm{Vdc}, \mathrm{V}^{-}=-12 \mathrm{~V}$ |  | -18 | -23 |  |
|  |  | $\mathrm{V}_{\text {in }}=0.8 \mathrm{Vdc}, \mathrm{V}^{-}=-12 \mathrm{~V}$ |  | 0 | 0 |  |
|  |  | $\mathrm{V}_{\text {in }}=1.9 \mathrm{Vdc}, \mathrm{V}^{-}=-15 \mathrm{~V}$ |  |  | -34 |  |
|  |  | $\mathrm{V}_{\text {in }}=0.8 \mathrm{Vdc}, \mathrm{V}^{-}=-15 \mathrm{~V}$ |  |  | -2.5 |  |
| Power Dissipation | PD | $\mathrm{V}^{+}=9.0 \mathrm{Vdc}, \mathrm{V}^{-}=-9.0 \mathrm{~V}$ |  |  | 333 | mW |
|  |  | $\mathrm{V}^{+}=12 \mathrm{Vdc}, \mathrm{V}-=-12 \mathrm{~V}$ |  |  | 576 |  |

SWITCHING CHARACTERISTICS $\left(\mathrm{V}^{+}=+9.0 \pm 1 \% \mathrm{Vdc}, \mathrm{V}^{-}=-9.0 \pm 1 \% \mathrm{Vdc}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right)$

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| Porpagation Delay Time | $\mathrm{t}_{\mathrm{pd}}+$ | $\mathrm{Z}_{\mathrm{L}}=3.0 \mathrm{k}$ and 15 pF |  | 275 | 350 | ns |
| Fall Time | $\mathrm{tf}_{\mathrm{f}}$ | $\mathrm{Z}_{\mathrm{L}}=3.0 \mathrm{k}$ and 15 pF |  | 45 | 75 | ns |
| Propagation Delay Time | tpd | $\mathrm{Z}_{\mathrm{L}}=3.0 \mathrm{k}$ and 15 pF |  | 110 | 175 | ns |
| Rise Time | $\mathrm{t}_{\mathrm{r}}$ | $\mathrm{Z}_{\mathrm{L}}-3.0 \mathrm{k}$ and 15 pF |  | 55 | 100 | ns |

## GENERAL DESCRIPTION

The RC1489 and RC1489A are monolithic quad line receivers designed to interface data terminal equipment in conformance with the specifications of EIA standard number RS-232-C. This standard specifies not only the number and type of interface leads, but also the voltage levels to be used.
The RC1488 quad driver and its companion circuit, the RC1489/RC1489A quad receiver, provide a complete interface system between DTL or TTL logic levels and the RS-232-C defined levels.

## DESIGN FEATURES

- Input Resistance 3k to 7k
- Input Signal Range $\pm 30 \mathrm{~V}$
- Built-in Input Threshold Hysteresis
- Response Control: Logic Threshold Shifting and Input Noise Filtering


## LOGIC DIAGRAM

$\square$

## CONNECTION INFORMATION






$\square$ DB and DC
Dual In-line Package
(Top View)


Order Part Nos.:
RCi489DC, $\AA$ RCi489ADC,
RC1489DB, RC1489ADB

## ABSOLUTE MAXIMUM RATINGS ( $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ unless otherwise noted)

| RATING | SYMBOL | VALUE | UNIT |
| :--- | :---: | :---: | :---: |
| Power Supply Voltage | $\mathrm{V}^{+}$ | +10 | V |
| Input Signal Range | $\mathrm{V}_{\text {in }}$ | $\pm 30$ | V |
| Output Load Current | $\mathrm{I}_{\mathrm{L}}$ | 20 | mA |
| Power Dissipation (Package Limitation, Ceramic and Plastic Dual In-Line Packages) <br> Derate above $\mathrm{TA}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | $\mathrm{P}_{\mathrm{D}}$ | 1000 | mW |
| Operating Temperature Range | $1 / \theta_{\mathrm{JA}}$ | 6.7 | $\mathrm{~mW} /{ }^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $\mathrm{T}_{\mathrm{A}}$ | 0 to +75 | ${ }^{\circ} \mathrm{C}$ |

## ELECTRICAL CHARACTERISTICS

(Response control pin is open. $\mathrm{V}^{+}=+5.0 \mathrm{Vdc} \pm 1 \%, \mathrm{~T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ unless otherwise noted)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Positive Input Current | 1/H | $V_{\text {in }}=+25 \mathrm{~V}$ | 3.6 |  | 8.3 | mA |
|  |  | $\mathrm{V}_{\text {in }}=+3.0 \mathrm{~V}$ | 0.43 |  |  |  |
| Negative Input Current | IIL | $V_{\text {in }}=-25 \mathrm{~V}$ | -3.6 |  | -8.3 | mA |
|  |  | $\mathrm{V}_{\text {in }}=-3.0 \mathrm{~V}$ | -0.43 |  |  |  |
| Input Turn-On Threshold Voltage | $\mathrm{V}_{\text {IH }}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{OL}} \leqslant 0.45 \mathrm{~V}$ RC1489 | 1.0 |  | 1.5 | V |
|  |  | RC1489A | 1.75 | 1.95 | 2.25 |  |
| Input Turn-Off Threshold Voltage | VIL | $\begin{array}{r} \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{VOH}_{\mathrm{OH}} \geqslant 2.5 \mathrm{~V}, \mathrm{I}_{\mathrm{L}}=-0.5 \mathrm{~mA} \\ \mathrm{RC} 1489 \end{array}$ | 0.75 |  | 1.25 | V |
|  |  | RC1489A | 0.75 | 0.8 | 1.25 |  |
| Output Voltage High | VOH | $\mathrm{V}_{\text {in }}=0.75 \mathrm{~V}, \mathrm{I}_{\mathrm{L}}=-0.5 \mathrm{~mA}$ | 2.6 | 4.0 | 5.0 | V |
|  |  | Input Open Circuit, $\mathrm{I}_{\mathrm{L}}=-0.5 \mathrm{~mA}$ | 2.6 | 4.0 | 5.0 |  |
| Output Voltage Low | VOL | $\mathrm{V}_{\text {in }}=3.0 \mathrm{~V}, \mathrm{I}_{\mathrm{L}}=10 \mathrm{~mA}$ |  | 0.2 | 0.45 | V |
| Output Short-Cirucuit Current | ISC |  |  | 3.0 |  | mA |
| Power Supply Current | $1^{+}$ | $\mathrm{V}_{\text {in }}=+5.0 \mathrm{~V}$ |  | 20 | 26 | mA |
| Power Dissipation | PD | $\mathrm{V}_{\text {in }}=+5.0 \mathrm{~V}$ |  | 100 | 130 | mW |

## SWITCHING CHARACTERISTICS $\left(\mathrm{V}^{+}=+5.0 \mathrm{Vdc} \pm 1 \%, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right)$

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNIT |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| Propagation Delay Time | $\mathrm{t}_{\mathrm{pd}+}$ | $\mathrm{R}_{\mathrm{L}}=3.9 \Omega$ |  | 25 | 85 | ns |
| Rise Time | $\mathrm{t}_{\mathrm{r}}$ | $\mathrm{R}_{\mathrm{L}}=3.9 \Omega$ |  | 120 | 175 | ns |
| Propagation Delay Time | $\mathrm{t}_{\mathrm{pd}}-$ | $\mathrm{R}_{\mathrm{L}}=390 \Omega$ |  | 25 | 50 | ns |
| Fall Time | $\mathrm{t}_{\mathrm{f}}$ | $\mathrm{R}_{\mathrm{L}}=390 \Omega$ |  | 10 | 20 | ns |

## GENERAL DESCRIPTION

The RM9622 and RC9622 are dual line receivers designed to discriminate a worst-case logic swing of 2 V from a $\pm 10 \mathrm{~V}$ common-mode noise signal or ground shift. To provide a CCSLcompatible threshold voltage and maximum noise immunity, the differential amplifier has a built-in threshold of 1.5 V . The offset is obtained by use of current sources and matched resistors, and varies only $\pm 5 \%$ ( 75 mV ) over the military and commercial temperature ranges.
The RM9622 military version operates over a temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The RC9622 is the commercial type which operates from $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.
These dual line receivers offer a choice of output states with the inputs open, without affecting circuit performance by use of S3. At the input of each line receiver a 130 -ohm terminating resistor is provided. The output is CCSL-compatible. And the output high level can be increased to +12 V by connecting to a positive supply through a resistor. The outputs can be wired OR.

## DESIGN FEATURES

- CCSL-Compatible Threshold Voltage
- Input Terminating Resistors
- Choice of Output State With Inputs Open
- CCSL-Compatible Output
- High Common-Mode
- Wire-OR Capability
- Enable Inputs
- Full Military Temperature Range
- Logic Compatible Supply Voltages


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## LOGIC DIAGRAM



ABSOLUTE MAXIMUM RATINGS
VCC, Pin Potential to Ground Pin. . . . . . . -0.5 V to +7 V
Input Voltage . . . . . . . . . . . . . . . . . $\pm 15 \mathrm{~V}$
Voltage Applied to Outputs for . . . . . -0.5 V to +13.2 V
High Output State
VEE Pin Potential to Ground Pin . . . . . . -0.5 V to -12 V
Enable Pin Potential to Ground Pin. . . . -0.5 V to -15 V
Storage Temperature Range. . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

Operating Temperature Range


ELECTRICAL CHARACTERISTICS
$\left(-55^{\circ} \mathrm{C}\right.$ to $\left.+125^{\circ} \mathrm{C}, \mathrm{V}_{C C}=5.0 \mathrm{~V} \pm 10 \%, V_{E E}=-10 \mathrm{~V} \pm 10 \%\right)$

| SYMBOL | CHARACTERISTICS | CONDITIONS \& COMMENTS |  | LIMITS |  |  |  |  |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $-55^{\circ} \mathrm{C}$ |  | +250 ${ }^{\circ}$ |  |  | $+125^{\circ} \mathrm{C}$ |  |  |
|  |  |  |  | MIN | MAX | MIN | TYP | MAX | MIN | MAX |  |
| VOL | Output Low Voltage | $V_{C C}=4.5 \mathrm{~V}$ <br> ${ }^{*} V_{\text {DIF }}=2.0 \mathrm{~V}$ | $\begin{aligned} & \mathrm{VEE}=-11 \mathrm{~V} \\ & \mathrm{I} \mathrm{OL}=12.4 \mathrm{~mA} \end{aligned}$ |  | 0.40 |  | 0.25 | 0.40 |  | 0.40 | V |
| VOH | Output High Voltage | $V_{C C}=4.5 \mathrm{~V}$ <br> ${ }^{*} V_{\text {DIFF }}=1.0 \mathrm{~V}$ | $\begin{aligned} & \mathrm{VEE}=-9.0 \mathrm{~V} \\ & \mathrm{IOH}=-0.2 \mathrm{~mA} \end{aligned}$ | 2.8 |  | 3.0 | 3.3 |  | 2.9 |  | V |
| ICEX | Output Leakage Current | $V_{C C}=4.5 \mathrm{~V}$ <br> ${ }^{*} V_{\text {DIFF }}=1.0 \mathrm{~V}$ | $\begin{aligned} & V_{E E}=-11 \mathrm{~V} \\ & V_{C E X}=12 \mathrm{~V} \end{aligned}$ |  | 50 |  |  | 100 |  | 200 | $\mu \mathrm{A}$ |
| ISC | Output Shorted Current | $\begin{aligned} & V_{C C}=5.0 \mathrm{~V} \\ & { }^{*} V_{\text {DIFF }}=1.0 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & V_{E E}=-10 \mathrm{~V} \\ & V_{S C}=0 \mathrm{~V} \end{aligned}$ | -1.3 | -3.1 | -1.4 | -2.15 | -3.1 | -1.3 | -3.1 | mA |
| IR(ENABLE) | Enable Input Leakage Current | $\begin{aligned} & \mathrm{VCC}=4.5 \mathrm{~V} \\ & \mathrm{~S}_{3}=4.5 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & V_{E E}=-11 \mathrm{~V} \\ & V_{R}=4.0 \mathrm{~V} \end{aligned}$ |  |  |  |  | 2.0 |  | 5.0 | $\mu \mathrm{A}$ |
| IF(ENABLE) | Enable Input Forward Current | $\begin{aligned} & V_{C C} 5.5 V \\ & S_{3}=0 V \\ & \hline \end{aligned}$ | $\begin{aligned} & V_{E E}=-9.0 \mathrm{~V} \\ & V_{F}=0 \mathrm{~V} \end{aligned}$ |  | -1.5 |  | -0.96 | $-1.5$ |  | -1.5 | mA |
| $I F(+$ INPUT $)$ | + Input <br> Forward Current | $\left\lvert\, \begin{aligned} & V_{C C}=5.0 \mathrm{~V} \\ & - \text { Input }=\mathrm{Gnd} \end{aligned}\right.$ | $\begin{aligned} & V_{E E}=-10 V \\ & V F=0 V \end{aligned}$ |  | -2.3 |  | -1.67 | -2.1 |  | -2.0 | mA |
| IF(-INPUT) | - Input <br> Forward Current | $\begin{aligned} & V_{C C}, S_{3}=5.0 \mathrm{~V} \\ & + \text { Input }=\text { Gnd } \end{aligned}$ | $\begin{aligned} & V_{E E}=-10 \mathrm{~V} \\ & V_{F}=0 V \end{aligned}$ |  | -2.6 |  | -1.87 | -2.4 |  | -2.3 | mA |
| VIL(ENABLE) | Input Low Voltage | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V} \pm 1$ | $V_{E E}=-10 \mathrm{~V} \pm 10 \%$ |  | 1.3 |  | 1.4 | 1.0 |  | 0.7 | V |
| $\mathrm{V}_{\text {th }}$ | Differential Input Threshold Voltage | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V} \pm 10$ | $V_{E E}=-10 \mathrm{~V} \pm 10 \%$ | 1.0 | 2.0 | 1.0 | 1.5 | 2.0 | 1.0 | 2.0 | V |
| $\mathrm{V}_{\mathrm{CM}}$ | Common Mode Voltage | $\begin{aligned} & \mathrm{VCC}=5.0 \mathrm{~V} \\ & { }^{*} \mathrm{~V} \text { DIFF }=1.0 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & V_{E E}=-10 \mathrm{~V} \\ & 2.0 \mathrm{~V} \end{aligned}$ |  |  | -10 | $\pm 12$ | +10 |  |  | V |
| $\mathrm{R}_{130}$ / | Terminating Resistance | $V_{C C}=5.5 \mathrm{~V}$ | $V_{E E}=-11 \mathrm{~V}$ |  |  | 100 | 130 | 175 |  |  | $\Omega$ |
| ICC | 5 V Supply Current | $\mathrm{S}_{3},+$ Inputs $=5$ | $\mathrm{V},-$ Inputs $=0 \mathrm{~V}$ |  |  |  | 13.7 | 22.9 |  |  | mA |
| 'EE | -10V Supply Current | $\begin{aligned} & V_{C C}=5.5 V \\ & S_{3},+ \text { Inputs }=5 . \end{aligned}$ | $V_{E E}=-11 \mathrm{~V}$ <br> $\mathrm{V},-$ Inputs $=0 \mathrm{~V}$ |  |  |  | -6.5 | -11.1 |  |  | mA |
| tpd + | Turn-off Time | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{INO}} \rightarrow 3.0 \mathrm{~V}, \mathrm{R}_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & \mathrm{VEE}=-10 \mathrm{~V} \\ & 3.9 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{L}}=30 \mathrm{pF} \end{aligned}$ |  |  |  | 38 | 50 |  |  | ns |
| tpd- | Turn-on Time | $\begin{aligned} & V_{C C}=5.0 \mathrm{~V} \\ & V_{\text {INO }} \rightarrow 3.0 \mathrm{~V}, R_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & V E E=-10 V \\ & 0.39 \mathrm{k} \Omega, C_{L}=30 \mathrm{pF} \end{aligned}$ |  |  |  | 35 | 50 |  |  | ns |

* $V_{\text {DIFF }}$ is a differential input voltage referred from $A+$ to $A$ - and from $B+$ to $B-$.

NOTE:

1. Rating applies to ambient temperature up to $70^{\circ} \mathrm{C}$. Above $70^{\circ} \mathrm{C}$, derate linearly at $8.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for the ceramic DIP and $7.1 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for the Flatpak.

ELECTRICAL CHARACTERISTICS $10{ }^{\circ} \mathrm{C}$ to $+75{ }^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V} \pm 5 \%, \mathrm{~V}_{\mathrm{EE}}=-10 \mathrm{~V} \pm 5 \%$ )

| SYMBOL | CHARACTERISTICS | CONDITIONS \& COMMENTS | LIMITS |  |  |  |  |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $0{ }^{\circ} \mathrm{C}$ |  | +250C |  |  | +750C |  |  |
|  |  |  | MIN | MAX | MIN | TYP | MAX | MIN | MAX |  |
| VOL | Output Low Voltage | $\begin{array}{ll} V_{C C}=4.75 \mathrm{~V} & V_{E E}=-10.5 \mathrm{~V} \\ { }^{*} V_{\text {DIFF }}=2.0 \mathrm{~V} & 1 \mathrm{OL}-14.1 \mathrm{~mA} \end{array}$ |  | 0.45 |  | 0.25 | 0.45 |  | 0.45 | V |
| $\mathrm{V}_{\mathrm{OH}}$ | Output High Voltage | $\begin{array}{ll} \mathrm{V}_{\mathrm{CC}}=4.75 \mathrm{~V} & \mathrm{VEE}^{*}=-9.5 \mathrm{~V} \\ { }^{*} \mathrm{~V}_{\mathrm{DIFF}}=1.0 \mathrm{~V} & 1 \mathrm{OH}=-0.2 \mathrm{~mA} \end{array}$ | 2.9 |  | 3.0 | 3.3 |  | 2.9 |  | V |
| ICEX | Output Leakage Current | $V_{C C}=4.75 \mathrm{~V}$ $V_{E E}=-10.5 \mathrm{~V}$ <br> ${ }^{*} V_{\text {DIFF }}=1.0 \mathrm{~V}$ $\mathrm{~V}_{\text {CEX }}=5.25 \mathrm{~V}$ |  | 80 |  |  | 100 |  | 200 | $\mu \mathrm{A}$ |
| ISC | Output Shorted Current | $\begin{array}{ll} V C C=5.0 V & V E E=-10 \mathrm{~V} \\ { }^{*} V \text { VIFF }=1.0 V & V_{S C}=0 \mathrm{~V} \end{array}$ | -1.3 | -3.1 | -1.4 | -2.15 | -3.1 | -1.3 | -3.1 | mA |
| IR(ENABLE) | Enable Input Leakage Current | $V_{C C}=4.75 \mathrm{~V}$ $V_{E E}=-10.5 \mathrm{~V}$ <br> $\mathrm{~S}_{3}=4.75 \mathrm{~V}$ $V_{\mathrm{R}}=4.0 \mathrm{~V}$ |  |  |  |  | 5.0 |  | 10 | $\mu \mathrm{A}$ |
| IF(ENABLE) | Enable Input Forward Current | $V C C 5.25 V$ $V_{E E}=-9.5 V$ <br> $S_{3}=0 V$ $V F=0 V$ |  | -1.5 |  | -0.96 | $-1.5$ |  | -1.5 | mA |
| IF(+INPUT) | + Input <br> Forward Current | $V_{C C}=5.0 V$ $V_{E E}=-10 V$ <br> - Input $=G n d$ $V_{F}=0 V$ |  | -2.6 |  | -1.67 | -2.4 |  | -2.3 | mA |
| IF(-INPUT) | - Input <br> Forward Current | $\begin{array}{ll} V_{C C}, S_{3}=5.0 V & V_{E E}=-10 \mathrm{~V} \\ + \text { Input }=G n d & V_{F}=0 V \end{array}$ |  | -2.9 |  | -1.87 | -2.7 |  | -2.6 | mA |
| VIL(ENABLE) | Input Low Voltage | $V_{C C}=5.0 \mathrm{~V} \pm 5 \% \quad V_{E E}=-10 \mathrm{~V} \pm 5 \%$ |  | 1.2 |  | 1.4 | 1.0 |  | 0.85 | V |
| $\mathrm{V}_{\text {th }}$ | Differential Input Threshold Voltage | $V_{C C}=5.0 V \pm 5 \% \quad V_{E E}=-10 \mathrm{~V} \pm 5 \%$ | 1.0 | 2.0 | 1.0 | 1.5 | 2.0 | 1.0 | 2.0 | V |
| VCM | Common Mode Voltage | $\begin{aligned} & V C C=5.0 \mathrm{~V} \quad V_{E E}=-10 \mathrm{~V} \\ & { }^{*} V_{\text {DIFF }}=1.0 \mathrm{~V} \text { or } 2.0 \mathrm{~V} \end{aligned}$ |  |  | -7.5 | $\pm 12$ | +7.5 |  |  | V |
| R130 $\Omega$ | Terminating Resistance | $V_{C C}=5.25 \mathrm{~V} \quad V_{E E}=-10.5 \mathrm{~V}$ |  |  | 91 | 130 | 185 |  |  | $\Omega$ |
| ICC | 5 V Supply Current | $\mathrm{S}_{3},+$ Inputs $=5.25 \mathrm{~V},-$ Inputs $=0 \mathrm{~V}$ |  |  |  | 13.7 | 22.9 |  |  | mA |
| IEE | -10V Supply Current | $\begin{aligned} & V_{C C}=5.25 \mathrm{~V} \quad V_{E E}=-10.5 \mathrm{~V} \\ & \mathrm{~S}_{3},+ \text { Inputs }=5.25 \mathrm{~V},- \text { Inputs }=0 \mathrm{~V} \end{aligned}$ |  |  |  | -6.5 | -11.1 |  |  | mA |
| tpd+ | Turn-off Time | $\begin{aligned} & V_{C C}=5.0 \mathrm{~V} \quad V_{E E}=-10 \mathrm{~V} \\ & V_{I N O} \rightarrow 3.0 \mathrm{~V}, R_{L}=3.9 \mathrm{k} \Omega, C_{L}=30 \mathrm{pF} \end{aligned}$ |  |  |  | 38 | 100 |  |  | ns |
| $t_{\text {pd- }}$ | Turn-on Time | $\begin{aligned} & V_{C C}=5.0 \mathrm{~V} \quad V_{E E}=-10 \mathrm{~V} \\ & V_{I N O \rightarrow 3.0 V}, R_{L}=0.39 \mathrm{k} \Omega, C_{L}=30 \mathrm{pF} \end{aligned}$ |  |  |  | 35 | 100 |  |  | ns |

* $V_{\text {DIFF }}$ is a differential input voltage referred from $A+$ to $A$ - and from $B+$ to $B-$.


## TYPICAL APPLICATIONS



## TYPICAL ELECTRICAL DATA



## C. FUNCTIONAL OUAGRAM OF PCA2OO MULTIPLIER



## SECTION 7

Special Functions

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## GENERAL DESCRIPTION

The RC555 and RM555 monolithic timing circuits are highly stable controllers capable of producing accurate time delays or oscillation. In the time delay mode, delay time is precisely controlled by only two external parts: a resistor and a capacitor. For operation as an oscillator, both the free running frequency and the duty cycle are accurately controlled by two external resistors and a capacitor.
Terminals are provided for triggering and resetting. The circuit will trigger and reset on falling waveforms. The output can source or sink up to 200 mA or drive TTL circuits.

## DESIGN FEATURES

- Timing From Microseconds Through Hours
- Operates in Both Astable and Monostable Modes
- Adjustable Duty Cycle
- Output Drives TTL
- High Current Output Can Source or Sink 200mA
- Temperature Stability of $0.005 \% /{ }^{\circ} \mathrm{C}$
- Normally On and Normally Off Output


## SCHEMATIC DIAGRAM



CONNECTION INFORMATION

| TE Metal Can Package (Top View) | DE and NB Dual In-line Packages (Top View) | PIN | FUNCTION |
| :---: | :---: | :---: | :---: |
| - |  | 1 | GROUND |
| (1) (1) | $\square 1{ }^{\circ} 8^{\circ} \square$ | 2 | TRIGGER |
| (1) (1) | $\square 2$ | 3 | OUTPUT |
| (2) (6) |  | 4 | RESET |
| (3) | ${ }^{3}$ | 5 | CONTROL VOLTAGE |
| (3) (4) (5) | $\square 4$ | 6 | THRESHOLD |
| (4) |  | 7 | DISCHARGE |
|  | Order Part Nos.: | 8 | $V_{\text {cc }}$ |
| Order Part Nos : | PCSESND, RVSSENS |  |  |
| RC555T, RM555T | RC555DE, RV555DE, RM555DE |  |  |

## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage . . . . . . . . . . . . . . . . . . . . . . . +18V | Operating Temperature Range |  |
| :---: | :---: | :---: |
| Power Dissipation . . . . . . . . . . . . . . . . . . . . 600mW | RC555 | $0^{\circ} \mathrm{C}$ to +700 C |
| Storage Temperature Range . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ | RV555 | . $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 60s) . . . . . . . $+300^{\circ} \mathrm{C}$ | RM555 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS ( $V_{C C}=+5 \mathrm{~V}$ to $+15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM555 |  |  | RV/RC555 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Supply Voltage |  | 4.5 |  | 18 | 4.5 |  | 16 | V |
| Supply Current | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=\infty \\ & \mathrm{V}_{\mathrm{CC}}=15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=\infty \\ & \text { Low State, }(\text { Note 1) } \\ & \hline \end{aligned}$ |  | $\begin{gathered} 3 \\ 10 \end{gathered}$ | $\begin{gathered} 5 \\ 12 \end{gathered}$ |  | $\begin{gathered} 3 \\ 10 \end{gathered}$ | $\begin{gathered} 6 \\ 15 \end{gathered}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| Timing Error <br> Initial Accuracy Drift with Temperature Drift with Supply Voltage | $\begin{aligned} & \mathrm{R}_{\mathrm{A}}, \mathrm{R}_{\mathrm{B}}=1 \mathrm{k} \Omega \text { to } 100 \mathrm{k} \Omega \\ & \mathrm{C}=0.1 \mu \mathrm{~F} \text { (Note } 2) \end{aligned}$ |  | $\begin{gathered} 0.5 \\ 30 \\ 0.05 \end{gathered}$ | $\begin{gathered} 2 \\ 100 \\ 0.2 \end{gathered}$ |  | $\begin{gathered} 1 \\ 50.1 \\ 0.1 \end{gathered}$ |  | ppm/ ${ }^{\circ} \mathrm{C}$ <br> \%/Volt |
| Threshold Voltage |  |  | 2/3 |  |  | 2/3 |  | $\times \mathrm{V}_{\mathrm{CC}}$ |
| Trigger Voltage | $\begin{aligned} & \mathrm{VCC}=15 \mathrm{~V} \\ & \mathrm{VCC}=5 \mathrm{~V} \end{aligned}$ | $\begin{gathered} \hline 4.8 \\ 1.45 \\ \hline \end{gathered}$ | $\begin{gathered} 5 \\ 1.67 \end{gathered}$ | $\begin{aligned} & 5.2 \\ & 1.9 \end{aligned}$ |  | $\begin{gathered} 5 \\ 1.67 \end{gathered}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Trigger Current |  |  | 0.5 |  |  | 0.5 |  | $\mu \mathrm{A}$ |
| Reset Voltage |  | 0.4 | 0.7 | 1.0 | 0.4 | 0.7 | 1.0 | V |
| Reset Current |  |  | 0.1 |  |  | 0.1 |  | mA |
| Threshold Current | (Note 3) |  | 0.1 | 0.25 |  | 0.1 | 0.25 | $\mu \mathrm{A}$ |
| Control Voltage Level | $\begin{aligned} & V_{C C}=15 \mathrm{~V} \\ & V_{C C}=5 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 9.6 \\ & 2.9 \end{aligned}$ | $\begin{gathered} 10 \\ 3.33 \\ \hline \end{gathered}$ | $\begin{gathered} 10.4 \\ 3.8 \\ \hline \end{gathered}$ | $\begin{aligned} & 9.0 \\ & 2.6 \\ & \hline \end{aligned}$ | $\begin{gathered} 10 \\ 3.33 \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ 4 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Output Voltage Drop (low) | $\begin{aligned} & \mathrm{VCC}=15 \mathrm{~V} \\ & \mathrm{ISINK}=10 \mathrm{~mA} \\ & \text { ISINK }=50 \mathrm{~mA} \\ & \text { ISINK }=100 \mathrm{~mA} \\ & \text { ISINK }=200 \mathrm{~mA} \\ & \mathrm{VCC}=5 \mathrm{~V} \\ & \text { ISINK }=8 \mathrm{~mA} \\ & \text { ISINK }=5 \mathrm{~mA} \end{aligned}$ |  | $\begin{gathered} 0.1 \\ 0.4 \\ 2 \\ 2.5 \\ \\ 0.1 \end{gathered}$ | $\begin{gathered} 0.15 \\ 0.5 \\ 2.2 \\ \\ 0.25 \end{gathered}$ |  | $\begin{gathered} 0.1 \\ 0.4 \\ 2 \\ 2.5 \\ \\ 0.25 \\ \hline \end{gathered}$ | $\begin{gathered} 0.25 \\ 0.75 \\ 2.5 \\ \\ \\ 0.35 \\ \hline \end{gathered}$ | $\begin{aligned} & V \\ & V \\ & V \\ & V \end{aligned}$ |
| Output Voltage Drop (high) |  | $\begin{gathered} 13 \\ 3 \\ \hline \end{gathered}$ | $\begin{gathered} 12.5 \\ \\ 13.3 \\ 3.3 \\ \hline \end{gathered}$ |  | $\begin{gathered} 12.75 \\ 2.75 \end{gathered}$ | $\begin{gathered} 12.5 \\ 13.3 \\ 3.3 \\ \hline \end{gathered}$ |  | $\begin{aligned} & \text { V } \\ & \text { V } \\ & \text { V } \end{aligned}$ |
| Rise Time of Output |  |  | 100 |  |  | 100 |  | ns |
| Fall Time of Output |  |  | 100 |  |  | 100 |  | ns |

## NOTES:

1. Supply current when output high typically 1 mA less.
2. Tested at $V_{C C}=5 \mathrm{~V}$ and $V_{C C}=15 \mathrm{~V}$.
3. This will determine the maximum value of $R_{A}+R_{B}$. For $15 V$ operation, the max total $R=20 \mathrm{megohm}$.

## TYPICAL ELECTRICAL DATA



## TYPICAL APPLICATIONS

## Missing Pulse Detector

With the RC555/RM555 connected as shown, the timing cycle will be continuously reset by the input pulse train. A change in frequency, or a missing pulse, allows the timing cycle to go to completion and change the output level. For proper operation the time delay should be set slightly longer than the normal time between pulses.


## TYPICAL APPLICATIONS (Cont.)

## Monostable Operation

In this mode, the timer functions as a one-shot. The external capacitor is initially held discharged by a transistor internal to the timer. Applying a negative trigger pulse to Pin 2 sets the flip-flop, driving the output high and releasing the short-circuit across the external capacitor. The voltage across the capacitor increases with time constant $r=R_{A C}$ to $2 / 3 \mathrm{~V}_{\mathrm{CC}}$, where the comparator resets the flip-flop and discharges the external capacitor. The output is now in the low state.


## Free Running Operation

With the circuit connected as shown, it will trigger itself and free run as a multivibrator. The external capacitor charges through $R_{A}$ and $R_{B}$ and discharges through $R_{B}$ only. Thus the duty cycle is set by the ratio of these two resistors, and the capacitor charges and discharges between


Circuit triggering takes place when the negative-going trigger pulse reaches $1 / 3 V_{C C}$ and the circuit stays in the output high state until the set time elapses. The time the output remains in the high state is $1.1 R_{A} C$ and can be determined by the graph. A negative pulse applied to Pin 4 (reset) during the timing cycle will discharge the external capacitor and start the cycle over again beginning on the positive-going edge of the reset pulse. If reset function is not used, Pin 4 should be connected to VCC to avoid false resetting.

## Time Delay

vs $R_{A}, R_{B}$ and $C$

$1 / 3 V_{C C}$ and $2 / 3 V_{C C}$. Charge and discharge times, and therefore frequency, are independent of supply voltage. The free running frequency versus $R_{A}, R_{B}$, and $C$ is shown in the graph.

Free Running Frequency vs $R_{A}, R_{B}$ and $C$


## GENERAL DESCRIPTION

The RC556 and RM556 dual monolithic timing circuits are highly stable controllers capable of producing accurate time delays or oscillation. In the time delay mode, delay time is precisely controlled by only two external parts: a resistor and a capacitor. For operation as an oscillator, both the free running frequency and the duty cycle are accurately controlled by two external resistors and a capacitor.
Terminals are provided for triggering and resetting. The circuit will trigger and reset on falling waveforms. The output can source or sink up to 200 mA or drive TTL circuits.

## DESIGN FEATURES

- Timing From Microseconds Through Hours
- Operates in Both Astable and Monostable Modes
- Adjustable Duty Cycle
- Output Drives TTL
- High Current Output Can Source or Sink 200 mA
- Temperature Stability of $0.005 \% /{ }^{\circ} \mathrm{C}$
- Normally On and Normally Off Output


## SCHEMATIC DIAGRAM



## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage . . . . . . . . . . . . . . . . . . . . . . . +18 V | Operating Temperature Range |  |
| :---: | :---: | :---: |
| Power Dissipation . . . . . . . . . . . . . . . . . . . . 600 mW | RC556 . . . . . . . . . . . . | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Storage Temperature Range . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ | RM556 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 60s) . . . . . . . . . $+300^{\circ} \mathrm{C}$ | RV556 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS ( $\mathrm{V}_{\mathrm{CC}}=+5 \mathrm{~V}$ to $+15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise specified)

| PARAMETER | CONDITIONS | RM556 |  |  | RC556, RV556 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX | MIN | TYP | MAX |  |
| Supply Voltage |  | 4.5 |  | 18 | 4.5 |  | 16 | V |
| Supply Current (Each Side) | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=\infty \\ & \mathrm{V}_{\mathrm{CC}}=15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=\infty \\ & \text { Low State, ( Note 1) } \end{aligned}$ |  | $\begin{gathered} 3 \\ 10 \end{gathered}$ | $\begin{gathered} \hline 5 \\ 11 \end{gathered}$ |  | $\begin{gathered} 3 \\ 10 \end{gathered}$ | $\begin{gathered} \hline 6 \\ 14 \end{gathered}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| Timing Error (Free Running) <br> Initial Accuracy Drift with Temperature Drift with Supply Voltage | $\begin{aligned} & \mathrm{R}_{\mathrm{A}}, \mathrm{R}_{\mathrm{B}}=2 \mathrm{k} \Omega \text { to } 100 \mathrm{k} \Omega \\ & \mathrm{C}=0.1 \mu \mathrm{~F} \text { (Note } 2) \end{aligned}$ |  | $\begin{gathered} 1.5 \\ 90 \\ 0.15 \end{gathered}$ |  |  | $\begin{gathered} 2.25 \\ 150 \\ 0.3 \end{gathered}$ |  | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ <br> \%/Volt |
| Timing Error (Monostable) <br> Initial Accuracy Drift with Temperature Drift with Supply Voltage | $\begin{aligned} & \mathrm{R}_{\mathrm{A}}, \mathrm{R}_{\mathrm{B}}=2 \mathrm{k} \Omega \text { to } 100 \mathrm{k} \Omega \\ & \mathrm{C}=0.1 \mu \mathrm{~F} \text { (Note } 2 \text { ) } \end{aligned}$ |  | $\begin{gathered} 0.5 \\ 30 \\ 0.05 \end{gathered}$ | $\begin{gathered} 1.5 \\ 100 \\ 0.2 \end{gathered}$ |  | $\begin{gathered} 0.75 \\ 50 \\ 0.1 \end{gathered}$ |  | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ <br> \%/Volt |
| Threshold Voltage |  |  | 2/3 |  |  | 2/3 |  | $\times V_{\text {CC }}$ |
| Trigger Voltage | $\begin{aligned} & V_{C C}=15 \mathrm{~V} \\ & V_{C C}=5 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 4.8 \\ & 1.45 \\ & \hline \end{aligned}$ | $\begin{gathered} 5 \\ 1.67 \end{gathered}$ | $\begin{aligned} & 5.2 \\ & 1.9 \end{aligned}$ |  | $\begin{gathered} 5 \\ 1.67 \end{gathered}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Trigger Current |  |  | 0.5 |  |  | 0.5 |  | $\mu \mathrm{A}$ |
| Reset Voltage |  | 0.4 | 0.7 | 1.0 | 0.4 | 0.7 | 1.0 | V |
| Reset Current |  |  | 0.1 |  |  | 0.1 |  | mA |
| Threshold Current | (Note 3) |  | 0.03 | 0.1 |  | 0.03 | 0.1 | $\mu \mathrm{A}$ |
| Control Voltage Level | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=15 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{CC}}=5 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 9.6 \\ & 2.9 \end{aligned}$ | $\begin{gathered} 10 \\ 3.33 \end{gathered}$ | $\begin{gathered} 10.4 \\ 3.8 \end{gathered}$ | $\begin{aligned} & 9.0 \\ & 2.6 \end{aligned}$ | $\begin{gathered} 10 \\ 3.33 \end{gathered}$ | $\begin{gathered} 11 \\ 4 \end{gathered}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Output Voltage Drop (low) | $\begin{aligned} & \hline \mathrm{VCC}=15 \mathrm{~V} \\ & \mathrm{ISINK}=10 \mathrm{~mA} \\ & \mathrm{I} \text { SINK }=50 \mathrm{~mA} \\ & \mathrm{I} \text { SINK }=100 \mathrm{~mA} \\ & \mathrm{I} \text { SINK }=200 \mathrm{~mA} \\ & \mathrm{VCC}=5 \mathrm{~V} \\ & \mathrm{I} \text { SINK }=8 \mathrm{~mA} \\ & \text { ISINK }=5 \mathrm{~mA} \\ & \hline \end{aligned}$ |  | $\begin{gathered} 0.1 \\ 0.4 \\ 2 \\ 2.5 \\ 0.1 \end{gathered}$ | $\begin{gathered} 0.15 \\ 0.5 \\ 2.25 \\ \\ 0.25 \end{gathered}$ |  | $\begin{gathered} 0.1 \\ 0.4 \\ 2 \\ 2.5 \\ \\ \\ 0.25 \end{gathered}$ | $\begin{aligned} & 0.25 \\ & 0.75 \\ & 2.75 \\ & \\ & \\ & 0.35 \end{aligned}$ | $\begin{aligned} & V \\ & V \\ & V \\ & V \end{aligned}$ |
| Output Voltage Drop (high) | $\begin{aligned} & \text { ISOURCE }=200 \mathrm{~mA} \\ & V C C=15 \mathrm{~V} \\ & I_{C O U R C E}=100 \mathrm{~mA} \\ & V_{C C}=15 \mathrm{~V} \\ & V_{C C}=5 \mathrm{~V} \end{aligned}$ | $\begin{gathered} 13 \\ 3 \\ \hline \end{gathered}$ | $\begin{gathered} 12.5 \\ 13.3 \\ 3.3 \\ \hline \end{gathered}$ |  | $\begin{gathered} 12.75 \\ 2.75 \\ \hline \end{gathered}$ | $\begin{gathered} 12.5 \\ 13.3 \\ 3.3 \\ \hline \end{gathered}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
| Rise Time of Output |  |  | 100 |  |  | 100 |  | ns |
| Fall Time of Output |  |  | 100 |  |  | 100 |  | ns |
| Matching Characteristics Between Each Section <br> Initial Timing Accuracy <br> Timing Drift with Temperature Drift with Supply Voltage |  |  | $\begin{array}{r} 0.3 \\ \pm 10 \\ 0.1 \end{array}$ | $\begin{aligned} & 0.6 \\ & 0.2 \end{aligned}$ |  | $\begin{gathered} 0.5 \\ \pm 10 \\ 0.2 \end{gathered}$ | 1 0.5 | $\begin{gathered} \% \\ \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ \% / \mathrm{Volt} \end{gathered}$ |

[^5]
## TYPICAL ELECTRICAL DATA



## NOTES

1. Supply current when output high typically 2 mA less.
2. Tested at $\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}$ and $\mathrm{V}_{\mathrm{CC}}=15 \mathrm{~V}$.
3. This will determine the maximum value of $R_{A}+R_{B}$. For 15 V operation, the maximum total $R=20 \mathrm{M} \Omega$.

## BASIC OPERATIONAL MODES

## Monostable Operation

In this mode, the timer functions as a one-shot. The external capacitor is initially held discharged by a transistor internal to the timer. Applying a negative trigger pulse to Pin 2 sets the flip-flop, driving the output high and releasing the short-circuit across the external capacitor. The voltage across the capacitor increases with time constant $r=R_{A C}$ to $2 / 3 \mathrm{~V}_{\mathrm{CC}}$, where the comparator resets the flip-flop and discharges the external capacitor. The output is now in the low state.


## Free Running Operation (Astable)

With the circuit connected as shown, it will trigger itself and free run as a multivibrator. The external capacitor charges through $R_{A}$ and $R_{B}$ and discharges through $R_{B}$ only. Thus the duty cycle is set by the ratio of these two resistors, and the capacitor charges and discharges between


Circuit triggering takes place when the negative-going trigger pulse reaches $1 / 3 \vee_{C C}$ and the circuit stays in the output high state until the set time elapses. The time the output remains in the high state is $1.1 \mathrm{RAC}_{\mathrm{A}} \mathrm{and}$ can be determined by the graph. A negative pulse applied to Pin 4 (reset) during the timing cycle will discharge the external capacitor and start the cycle over again beginning on the positive-going edge of the reset pulse. If reset function is not used, Pin 4 should be connected to VCC to avoid false resetting.

$1 / 3 V_{C C}$ and $2 / 3 V_{C C}$. Charge and discharge times, and therefore frequency, are independent of supply voltage. The free running frequency versus $R_{A}, R_{B}$, and $C$ is shown in the graph.

Free Running Frequency vs $R_{A}, R_{B}$ and $C$


## DESCRIPTION

The XR-2207 is a monolithic voltage-controlled oscillator (VCO) integrated circuit featuring excellent frequency stability and a wide tuning range. The circuit provides simultaneous triangle and squarewave outputs over a frequency range of 0.01 Hz to 1 MHz . It is ideally suited for FM, FSK, and sweep or tone generation, as well as for phase-locked loop applications.

As shown in Figure 1, the circuit is comprised of four functional blocks: a variable-frequency oscillator which generates the basic periodic waveforms; four current switches actuated by binary keying inputs; and buffer amplifiers for both the triangle and squarewave outputs. The internal switches transfer the oscillator current to any of four external timing resistors to produce four discrete frequencies which are selected according to the binary logic levels at the keying terminals (pins 8 and 9 ).

The XR-2207 has a typical drift specification of $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. The oscillator frequency can be linearly swept over a 1000:1 range with an external control voltage; and the duty cycle of both the triangle and the squarewave outputs can be varied from $0.1 \%$ to $99.9 \%$ to generate stable pulse and sawtooth waveforms.

## FEATURES

- Excellent Temperature Stability ( $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ )
- Linear Frequency Sweep
- Adjustable Duty Cycle (0.1\% to 99.9\%)
- Two or Four Level FSK Capability
- Wide Sweep Range (1000:1 Min)
- Logic Compatible Input and Output Levels
- Wide Supply Voltage Range ( $\pm 4 \mathrm{~V}$ to $\pm 13 \mathrm{~V}$ )
- Low Supply Sensitivity (0.15\%/V)
- Wide Frequency Range $(0.01 \mathrm{~Hz}$ to 1 MHz$)$
- Simultaneous Triangle and Squarewave Outputs


## APPLICATIONS

- FSK Generation
- Voltage and Current-to-Frequency Conversion
- Stable Phase-Locked Loop
- Waveform Generation

Triangle, Sawtooth, Pulse, Squarewave

- FM and Sweep Generation


## SCHEMATIC DIAGRAM



CONNECTION INFORMATION


Figure 1. Functional Schematic Diagram

## ELECTRICAL CHARACTERISTICS

Test circuit of Figure 2, $\mathrm{V}^{+}=\mathrm{V}^{-}=6 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}=5000 \mathrm{pF}$,
$R_{1}=R_{2}=R_{3}=R_{4}=20 \mathrm{~K} \Omega, R_{L}=4.7 \mathrm{~K} \Omega$, Binary inputs grounded,
$S_{1}$ and $S_{2}$ closed unless otherwise specified.

| PARAMETERS | CONDITIONS | XR-2207 |  |  | XR-2207C |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN. | TYP. | MAX. | MIN. | TYP. | MAX. |  |
| GENERAL CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Supply Voltage <br> Single Supply <br> Split Supplies | See Typical Electrical Data | $\begin{array}{r} 8 \\ \pm 4 \\ \hline \end{array}$ | $\begin{array}{r} 12 \\ \pm 6 \\ \hline \end{array}$ | $\begin{array}{r} 26 \\ \pm 13 \\ \hline \end{array}$ | $\begin{array}{r} 8 \\ \pm 4 \\ \hline \end{array}$ | $\begin{array}{r} 12 \\ \pm 6 \\ \hline \end{array}$ | $\begin{array}{r} 26 \\ \pm 13 \\ \hline \end{array}$ | $\begin{aligned} & v \\ & v \end{aligned}$ |
| Supply Current <br> Single Supply <br> Split Supplies <br> Positive <br> Negative | Measured at pin $1, \mathrm{~S}_{1}$ open See Figure 2 <br> Measured at pin $1, \mathrm{~S}_{1}$ open Measured at pin $12, \mathrm{~S}_{1}, \mathrm{~S}_{2}$ open |  | 5 <br> 5 <br> 4 | 7 <br> 7 <br> 6 |  | 5 <br> 5 <br> 4 | 8 <br> 8 <br> 7 | mA <br> mA <br> mA |
| OSCILLATOR SECTION - FREQUENCY CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Upper Frequency Limit | $\mathrm{C}=500 \mathrm{pF}, \mathrm{R}_{3}=2 \mathrm{~K} \Omega$ | 0.5 | 1.0 |  | 0.5 | 1.0 |  | MHz |
| Lower Practical Frequency | $\mathrm{C}=50 \mu \mathrm{~F}, \mathrm{R}_{3}=2 \mathrm{M} \Omega$ |  | 0.01 |  |  | 0.01 |  | Hz |
| Frequency Accuracy |  |  | $\pm 1$ | $\pm 3$ |  | $\pm 1$ | $\pm 5$ | \% of $\mathrm{f}_{0}$ |
| Frequency Matching |  |  | 0.5 |  |  | 0.5 |  | $\%$ of $\mathrm{f}_{0}$ |
| Frequency Stability <br> Temperature <br> Power Supply | $0^{\circ}<\mathrm{T}_{\mathrm{A}}<75^{\circ} \mathrm{C}$ |  | $\begin{aligned} & 20 \\ & 0.15 \end{aligned}$ | 50 |  | $\begin{aligned} & 30 \\ & 0.15 \end{aligned}$ |  | $\begin{aligned} & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ & \% / \mathrm{V} \end{aligned}$ |
| Sweep Range | $\begin{aligned} & R_{3}=1.5 \mathrm{~K} \Omega \text { for } f_{H 1} \\ & R_{3}=2 \mathrm{M} \Omega \text { for } f_{L} \end{aligned}$ | 1000:1 | 1000:1 |  |  | 1000:1 |  | $\mathrm{fH} / \mathrm{fL}$ |
| Sweep Linearity <br> 10:1 sweep <br> 1000:1 Sweep | $\begin{aligned} & \mathrm{C}=5000 \mathrm{pF} \\ & \mathrm{f}_{\mathrm{H}}=10 \mathrm{kHz}, \mathrm{f}_{\mathrm{L}}=1 \mathrm{kHz} \\ & \mathrm{f}_{\mathrm{H}}=100 \mathrm{kHz}, \mathrm{f}_{\mathrm{L}}=100 \mathrm{kHz} \end{aligned}$ |  | $\begin{aligned} & 1 \\ & 5 \end{aligned}$ | 2 |  | $\begin{aligned} & 1.5 \\ & 5 \end{aligned}$ |  | \% |
| FM Distortion | $\pm 10 \%$ FM Deviation |  | 0.1 |  |  | 0.1 |  | \% |
| Recommended Range of Timing Resistors | See Characteristic Curves | 1.5 |  | 2000 | 1.5 |  | 2000 | $K \Omega$ |
| Impedance at Timing Pins | Measured at pins 4,5,6, or 7 |  | 75 |  |  | 75 |  | $\Omega$ |
| DC Level at Timing Terminals |  |  | 10 |  |  | 10 |  | mV |
| BINARY KEYING INPUTS |  |  |  |  |  |  |  |  |
| Switching Threshold | Measured at pins 8 and 9 . <br> Refer to pin 10 | 1.4 | 2.2 | 2.8 | 1.4 | 2.2 | 2.8 | V |
| Input Impedance |  |  | 5 |  |  | 5 |  | $\mathrm{K} \Omega$ |
| OUTPUT CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Triangle Output Amplitude Impedance DC Level Linearity | Measured at pin 13 <br> Referenced to pin 10 from 10\% to $90 \%$ of swing | 4 | $\begin{gathered} 6 \\ 10 \\ +100 \\ 0.1 \end{gathered}$ |  | 4 | $\begin{gathered} 6 \\ 10 \\ +100 \\ 0.1 \end{gathered}$ |  | Vpp <br> $\Omega$ <br> mV <br> \% |
| Squarewave Output <br> Amplitude <br> Saturation Voltage <br> Rise Time <br> Fall Time | Measured at pin 13, $\mathrm{S}_{5}$ closed <br> Referenced to pin 12 $\begin{aligned} & C_{L} \leqslant 10 p F \\ & C_{L} \leqslant 10 p F \end{aligned}$ | 11 | $\begin{gathered} 12 \\ 0.2 \\ 200 \\ 20 \end{gathered}$ | 0.4 | 11 | $\begin{gathered} 12 \\ 0.2 \\ 200 \\ 20 \end{gathered}$ | 0.4 | Vpp <br> V <br> nsec <br> nsec |

## ABSOLUTE MAXIMUM RATINGS



## DESCRIPTION OF CIRCUIT CONTROLS

## TIMING CAPACITOR (PINS 2 AND 3)

The oscillator frequency is inversely proportional to the timing capacitor, C . The minimum capacitance value is limited by stray capacitances and the maximum value by physical size and leakage current considerations. Recommended values range from 100 pF to $100 \mu \mathrm{~F}$. The capacitor should be non-polarized.

## TIMING RESISTORS (PINS 4, 5, 6, AND 7)

The tinıng resistors determine the total timing current, $I_{T}$, available to charge the timing capacitor. Values for timing resistors can range from $1.5 \mathrm{~K} \Omega$ to $2 \mathrm{M} \Omega$; however, for optimum temperature and power supply stability, recommended values are $4 \mathrm{~K} \Omega$ to $200 \mathrm{~K} \Omega$. To avoid parasitic pick up, timing resistor leads should be kept as short as possible. For noisy environments, unused or deactivated timing terminals should be bypassed to ground through $0.1 \mu \mathrm{~F}$ capacitors. Otherwise, they may be left open.

## SUPPLY VOLTAGE (PINS 1 AND 12)

The XR-2207 is designed to operate over a power supply range of $\pm 4 \mathrm{~V}$ to $\pm 13 \mathrm{~V}$ for split supplies, or 8 V to 26 V for single supplies. At high supply voltages, the frequency sweep range is reduced. Performance is optimum for $\pm 6 \mathrm{~V}$, or 12 V single supply operation.

## BINARY KEYING INPUTS (PINS 8 AND 9)

The internal impedance at these pins is approximately $5 \mathrm{~K} \Omega$. Keying levels are $<1.4 \mathrm{~V}$ for "zero" and $>3 \mathrm{~V}$ for "one" logic levels referenced to the de voltage at pin 10.

## BIAS FOR SINGLE SUPPLY (PIN 11)

For single supply operations, pin 11 should be externally biased to a potential between $\mathrm{V}^{+} / 3$ and $\mathrm{V}^{+} / 2$ volts (see Figure 2). The bias current at pin 11 is nominally $5 \%$ of the total oscillation timing current $\mathrm{I} T$.

## GROUND (PIN 10)

For split supply operation, this pin serves as circuit ground. For single supply operation, pin 10 should be ac grounded through a $1 \mu \mathrm{~F}$ bypass capacitor. During split supply operation, a ground current of $2 I_{\top}$ flows out of this terminal, where $I_{T}$ is the total timing current.

## SQUAREWAVE OUTPUT (PIN 13)

The squarewave output at pin 13 is a "open-collector" stage capable of sinking up to 20 mA of load current. $R_{L}$ serves as a pull-up load resistor for this output. Recommended values for $R_{L}$ range from $1 \mathrm{~K} \Omega$ to $100 \mathrm{~K} \Omega$.

## TRIANGLE OUTPUT (PIN 14)

The output at pin 14 is a triangle wave with a peak swing of approximately one-half of the total supply voltage. Pin 14 has a very low output impedance of $10 \Omega$ and is internally protected against short circuits.

Note: Triangle waveform linearity is sensitive to parasitic coupling between the square and the triangle-wave outputs (pins 13 and 14). In board layout or circuit wiring care should be taken to minimize stray wiring capacitance between these pins.

## OPERATING INSTRUCTIONS

## PRECAUTIONS

The following precautions should be observed when operating the XR-2207 family of integrated circuits:

1. Pulling excessive current from the timing terminals will adversely effect the temperature stability of the circuit. To minimize this disturbance, it is recommended that the totai cuirrent drawn from pins 4, 5, 6 , and 7 be limited to $\leqslant 6 \mathrm{~mA}$. In addition, permanent damage to the device may occur if the total timing current exceeds 10 mA .
2. Terminals $2,3,4,5,6$, and 7 have very low internal impedance and should, therefore, be protected from accidental shorting to ground or the supply voltages.
3. The keying logic pulse amplitude should not exceed the supply voltage.


Figure 2. Test Circuit for Split Supply Operation


Figure 3. Test Circuit for Single Supply Operation

## TYPICAL PERFORMANCE DATA

 for Split Supply Voltage


Frequency Accuracy vs.
Timing Resistance

Value vs Power Supply Voltage*


Frequency Drift vs. Supply Voltage


Pulse and Sawtooth Outputs


Normalized Frequency
Drift with Temperature
*Note: $R_{T}=$ Parallel Combination of Activated Timing Resistors

## SPLIT SUPPLY OPERATION

Figure 2 is the recommended circuit connection for split supply operation. The frequency of operation is determined by the timing capacitor, C , and the activated timing resistors ( $R_{1}$ through $R_{4}$ ). The timing resistors are activated by the logic signals at the binary keying inputs (pins 8 and 9 ), as shown in the logic table below. If a single timing resistor is activated, the frequency is $1 / R C$. Otherwise, the frequency is either $1 /\left(R_{1} \| R_{2}\right) C$ or $1 /\left(R_{1} \| R_{4}\right) C$.

The squarewave output is obtained at pin 13 and has a peak-to-peak voltage swing equal to the supply voltages. This output is an "open-collector" type and requires an external pull-up load resistor (nominally $5 \mathrm{~K} \Omega$ ) to the positive supply. The triangle waveform obtained at pin 14 is centered about ground and has a peak amplitude of $\mathrm{V}^{+} / 2$.

The circuit operates with supply voltages ranging from $\pm 4 \mathrm{~V}$ to $\pm 13 \mathrm{~V}$. Minimum drift occurs with $\pm 6$ volt supplies. For operation with unequal supply voltages, see page 4.


Figure 4. Frequency Sweep Operation

Table 1. Logic Table for Binary Keying Controls

| LOGIC <br> LEVEL |  | SELECTED <br> TIMING PINS | FREQUENCY | DEFINITIONS |
| :---: | :---: | :---: | :---: | :---: |
| 8 | 9 |  |  |  |
| 0 | 0 | 6 | $\mathrm{f}_{1}$ | $f_{1}=1 / R_{3} C, \Delta f_{1}=1 / R_{4} C$ |
| 0 | 1 | 6 and 7 | $\mathrm{f}_{1}+\Delta \mathrm{f}_{1}$ | $f_{2}=1 / R_{2} C, \Delta f_{2}=1 / R_{1} C$ |
| 1 | 0 | 5 | $\mathrm{f}_{2}$ | Logic Levels: $0=$ Ground |
| 1 | 1 | 4 and 5 | $\mathrm{f}_{2}+\triangle \mathrm{f}_{2}$ | $1=>3 V$ |

Note: For single-supply operation, logic levels are referenced to voltage at pin 10.

## SINGLE SUPPLY OPERATION

The circuit should be interconnected as shown in Figure 3 for singie-suppiy operation. Pin 12 should be grounded, and pin 11 biased from $\mathrm{V}^{+}$through a resistive divider to a value of bias voltage between $\mathrm{V}^{+} / 3$ and $\mathrm{V}^{+} / 2$. Pin 10 is bypassed to ground through a $0.1 \mu \mathrm{~F}$ capacitor.

For single-supply operation, the dc voltage at pin 10 and the timing terminals (pins 4 through 7) are equal and approximately 0.6 V above $\mathrm{V}_{\mathrm{B}}$, the bias voltage at pin 11. The logic levels at the binary keying terminals are referenced to the voltage at pin 10.

## ON - OFF KEYING

The XR-2207 can be keyed on and off by simply activating an open circuited timing pin. Under certain conditions, the circuit may exhibit very low frequency ( $<1 \mathrm{~Hz}$ ) residual oscillation in the "off" state due to internal bias current. If this effect is undesirable, it can be eliminated by connecting a $10 \mathrm{M} \Omega$ resistor from pin 3 to $\mathrm{V}^{+}$.

## FREQUENCY CONTROL (SWEEP AND FM)

The frequency of operation is controlled by varying the total timing current, $\mathrm{I}_{\mathrm{T}}$, drawn from the activated timing pins $4,5,6$, or 7 . The timing current can be modulated by applying a control voltage, $\mathrm{V}_{\mathrm{C}}$, to the activated timing pin through a series resistor $R_{C}$ as shown in Figure 4.

For split supply operation, a negative control voltage, $\mathrm{V}_{\mathrm{C}}$, applied to the circuits of Figure 4 causes the total timing current, IT, and the frequency, to increase.

As an example, in the circuit of Figure 4, the binary keying inputs are grounded. Therefore, only timing pin 6 is activated.

The frequency of operation is determined by:

$$
f=\frac{1}{R_{3} C_{B}}\left[1-\frac{V_{C} R_{3}}{R_{C^{-}} V^{-}}\right] H z
$$

## PULSE AND SAWTOOTH OPERATION

The duty cycle of the output waveforms can be controlled by frequency shift keying at the end of every half cycle of oscillator output. This is accomplished by connecting one or both of the binary keying inputs (pins 8 or 9 ) to the squarewave output at pin 13. The output waveforms can then be converted to positive or negative pulses and sawtooth waveforms.

Figure 5 is the recommended circuit connection for duty cycle control. Pin 8 is shorted to pin 13 so that the circuit switches between the " 0,0 " and the " 1,0 " logic states given in Table 1. Timing pin 5 is activated when the output is "high", and pin 6 is activated when the squarewave output goes to a "low" state.


Figure 5. Pulse and Sawtooth Generation

The duty cycle of the output waveforms is given as:

$$
\text { Duty Cycle }=\frac{R_{2}}{R_{2}+R_{3}}
$$

and can be varied from $0.1 \%$ to $99.9 \%$ by proper choice of timing resistors. The frequency of oscillation, $f$, is given as:

$$
f=\frac{2}{C}\left[\frac{1}{R_{2}+R_{3}}\right]
$$

AVAILABLE TYPES

| Part Number | Package | Operating Temperature |
| :--- | :--- | :---: |
| XR-2207M | Ceramic | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| XR-2207CN | Ceramic | $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ |
| XR-2207CP | Plastic | $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ |
| XR-2207N | Ceramic | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| XR-2207P | Plastic | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |

The frequency can be modulated or swept without changing the duty cycle by connecting $\mathrm{R}_{2}$ and $\mathrm{R}_{3}$ to a common control voltage $\mathrm{V}_{\mathrm{C}}$ instead of to $\mathrm{V}^{-}$. The sawtooth and the pulse output waveforms are shown in the Typical Electrical Data.

## DESCRIPTION

The XR-2211 is a monolithic phase-locked loop (PLL) system especially designed for data communications. It is particularly well suited for FSK modem applications. It operates over a wide supply voltage range of 4.5 to 20 V and a wide frequency range of 0.01 Hz to 300 kHz . It can accommodate analog signals between 2 mV and 3 V , and can interface with conventional DTL, TTL and ECL logic families. The circuit consists of a basic PLL for tracking an input signal frequency within the passband, a quadrature phase detector which provides carrier detection, and an FSK voltage comparator which provides FSK demodulation. External components are used to independently set carrier frequency, bandwidth, and output delay.


## FEATURES

- Wide Frequency Range ( 0.01 Hz to 300 kHz )
- Wide Supply Voltage Range (4.5V to 20V)
- DTL/TTL/ECL Logic Compatibility
- FSK Demodulation with Carrier-Detection
- Wide Dynamic Range ( 2 mV to 3 Vrms )
- Adjustable Tracking Range ( $\pm 1 \%$ to $\pm 80 \%$ )
- Excellent Temperature Stability ( $20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$, typical)


## APPLICATIONS

- FSK Demodulation
- Data Synchronization
- Tone Decoding
- FM Detection
- Carrier Detection


## SCHEMATIC DIAGRAM



ABSOLUTE MAXIMUM RATINGS

| Power Supply . | 20 V |
| :---: | :---: |
| Input Signal Level | 3 V rms |
| Power Dissipation |  |
| Ceramic Package . . . . . . . . . 750 mW |  |
| Derate above $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. . . . . $6 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ |  |
| Plastic Package | 625 mW |
| Derate above $\mathrm{TA}^{\prime}=+25^{\circ} \mathrm{C}$ | $5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ |

## ELECTRICAL CHARACTERISTICS

Test Conditions (see Figure 2):
$\mathrm{V}^{+}=+12 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{R}_{0}=30 \mathrm{~K} \Omega . \mathrm{C}_{0}=0.033 \mu \mathrm{~F}$.

CONNECTION INFORMATION


## GENERAL

| Supply Voltage |  | 4.5 |  | 20 | 4.5 |  | 20 | V |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- | :--- |
| Supply Current | $\mathrm{R}_{0} \geq 10 \mathrm{~K} \Omega$ See Fig. 4. |  | 4 | 7 |  | 5 | 9 | mA |


| OSCILLATOR |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency Accuracy | Deviation from $f_{0}=1 / R_{0} C_{0}$ |  | $\pm 1$ | $\pm 3$ |  | $\pm 1$ |  | \% |
| Frequency Stability Temperature Coefficient Power Supply Rejection | $R_{1}=\infty$ <br> See Fig. 8. <br> $V^{+}=12 \pm 1 \mathrm{~V}$. See Fig. 7 . $\mathrm{V}^{+}=5 \pm 0.5 \mathrm{~V} \text {. See Fig. } 7$ |  | $\begin{array}{r}  \pm 20 \\ 0.05 \\ 0.2 \end{array}$ | $\begin{array}{r}  \pm 50 \\ 0.5 \end{array}$ |  | $\begin{array}{r}  \pm 20 \\ 0.05 \\ 0.2 \end{array}$ |  | $\begin{aligned} & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ & \% / \mathrm{V} \\ & \% / \mathrm{V} \\ & \hline \end{aligned}$ |
| Upper Frequency Limit | $\mathrm{R}_{0}=8.2 \mathrm{~K} \Omega, \mathrm{C}_{0}=400 \mathrm{pF}$ | 100 | 300 |  |  | 300 |  | kHz |
| Lowest Practical Operating Frequency | $\mathrm{R}_{0}=2 \mathrm{M} \Omega, \mathrm{C}_{0}=50 \mu \mathrm{~F}$ |  |  | 0.01 |  | 0.01 |  | Hz |
| Timing Resistor, $\mathrm{R}_{0}$ Operating Range Recommended Range | See Fig. 5 <br> See Fig. 7 and 8. | 5 15 |  | $\begin{array}{r} 2000 \\ 100 \end{array}$ | 5 15 |  | $\begin{array}{r} 2000 \\ 100 \end{array}$ | $\begin{aligned} & \mathrm{K} \Omega \\ & \mathrm{~K} \Omega \end{aligned}$ |
| LOOP PHASE DETECTOR |  |  |  |  |  |  |  |  |
| Peak Output Current | Measured at pin 11. | $\pm 150$ | $\pm 200$ | $\pm 300$ | $\pm 100$ | $\pm 200$ | $\pm 300$ | $\mu \mathrm{A}$ |
| Output Offset Current |  |  | $\pm 1$ |  |  | $\pm 2$ |  | $\mu \mathrm{A}$ |
| Output Impedance |  |  | 1 |  |  | 1 |  | M $\Omega$ |
| Maximum Swing | Referenced to pin 10. | $\pm 4$ | $\pm 5$ |  | $\pm 4$ | $\pm 5$ |  | V |

QUADRATURE PHASE DETECTOR

| Peak Output Current | Measured at pin 3. | 100 | 150 |  |  | 150 |  | $\mu$ |
| :--- | :--- | ---: | ---: | :--- | :--- | ---: | :--- | :--- |
| Output Impedance |  |  | 1 |  |  | 1 |  | $\mathrm{M} \Omega$ |
| Maximum Swing |  |  | 11 |  |  | 11 |  | Vpp |

## INPUT PREAMP

| Input Impedance | Measured at pin 2. |  | 20 |  |  | 20 |  | $\mathrm{~K} \Omega$ |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Input Signal <br> Voltage Required to Cause Limiting |  |  |  |  |  |  |  | mV |

## VOLTAGE COMPARATOR

| Input Impedance | Measured at pins 3 and 8. |  | 2 |  |  | 2 |  | $\mathrm{M} \Omega$ |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | :--- | :--- |
| Input Bias Current |  |  | 100 |  |  | 100 |  | nA |
| Voltage Gain | $\mathrm{R}_{\mathrm{L}}=5.1 \mathrm{~K} \Omega$ | 55 | 70 |  | 55 | 70 |  | dB |
| Output Voltage Low | $\mathrm{I}_{\mathrm{C}}=3 \mathrm{~mA}$ |  | 300 |  |  | 300 |  | mV |
| Output Leakage Current | $\mathrm{V}_{0}=12 \mathrm{~V}$ |  | .01 |  |  | .01 |  | $\mu \mathrm{~A}$ |
| INTERNAL REFERENCE |  |  |  |  |  |  |  |  |
| Voltage Level | Measured at pin 10. | 4.9 | 5.3 | 5.7 | 4.75 | 5.3 | 5.85 | V |
| Output Impedance |  | 100 |  |  | 100 |  | $\Omega$ |  |

## TYPICAL PERFORMANCE DATA




Figure 1. Functional Block Diagram of a Tone and FSK Decoding System Using XR-2211.

## DESCRIPTION OF CIRCUIT CONTROLS

SIGNAL INPUT (PIN 2)
Signal is ac coupled to this terminal. The internal impedance at pin 2 is $20 \mathrm{~K} \Omega$. Recommended input signal level is in the range of 10 mV rms to 3 V rms .

## QUADRATURE PHASE DETECTOR OUTPUT (PIN 3)

This is the high-impedance output of quadrature phase detector, and is internally connected to the input of lockdetect voltage-comparator. In tone-detection applications, pin 3 is connected to ground through a parallel combination of $R_{D}$ and $C_{D}$ (see Figure 2) to eliminate the chatter at lock-detect outputs. If this tone-detect section is not used, pin 3 can be left open circuited.


Figure 2. Generalized Circuit Connection for FSK and Tone Detection

## LOCK-DETECT OUTPUT, Q (PIN 5)

The output at pin 5 is at "high" state when the PLL is out of lock and goes to "low" or conducting state when the PLL is locked. It is an open-collector type output and requires a pull-up resistor, $\mathrm{R}_{\mathrm{L}}$, to $\mathrm{V}^{+}$for proper operation. At "low" state, it can sink up to 5 mA of load current.

## LOCK-DETECT COMPLEMENT, $\overline{\mathrm{O}}$ (PIN 6)

The output at pin 6 is the logic complement of the lockdetect output at pin 5 . This output is also an open-collector type stage which can sink 5 mA of load current at low or "on" state.

## FSK DATA OUTPUT (PIN 7)

This output is an open-collector logic stage which requires a pull-up resistor, $\mathrm{R}_{\mathrm{L}}$, to $\mathrm{V}^{+}$for proper operation. It can sink 5 mA of load current. When decoding FSK signals, FSK data output is at "high" or off state for low input frequency; and at "low" or on state for high input frequency. If no input signal is present, the logic state at pin 7 is indeterminate.

## FSK COMPARATOR INPUT (PIN 8)

This is the high-impedance input to the FSK voltage comparator. Normally, an FSK post-detection or data filter is connected between this terminal and the PLL phasedetector output (pin 11). This data filter is formed by $R_{F}$ and $C_{F}$ of Figure 2. The threshold voltage of the comparator is set by the internal reference voltage, $\mathrm{V}_{\mathrm{R}}$, available for pin 10.

## REFERENCE VOLTAGE, $\mathbf{V R}_{\mathrm{R}}$ (PIN 10)

This pin is internally biased at the reference voltage level, $V_{R} ; V_{R}=V^{+} / 2-650 \mathrm{mV}$. The dc voltage level at this pin forms an internal reference for the voltage levels at pins $3,8,11$ and 12 . Pin 10 must be bypassed to ground with a $0.1 \mu \mathrm{~F}$ capacitor, for proper operation of the circuit.

LOOP PHASE DETECTOR OUTPUT (PIN 11)
This terminal provides a high-impedance output for the loop phase-detector. The PLL loop filter is formed by $\mathrm{R}_{1}$ and $\mathrm{C}_{1}$ connected to pin 11 (see Figure 2). With no input signal, or with no phase-error within the PLL, the dc level at pin 11 is very nearly equal to $V_{R}$. The peak voltage swing available at the phase detector output is equal to $\pm \mathrm{V}_{\mathrm{R}}$.

## VCO CONTROL INPUT (PIN 12)

VCO free-running frequency is determined by external timing resistor, $\mathrm{R}_{0}$, connected from this terminal to ground. The VCO free-running frequency, $\mathrm{f}_{\mathrm{O}}$, is:

$$
\mathrm{f}_{0}=\frac{1}{\mathrm{R}_{0} \mathrm{C}_{0}} \mathrm{~Hz}
$$

where $C_{0}$ is the timing capacitor across pins 13 and 14. For optimum temperature stability, $\mathrm{R}_{0}$ must be in the range of $10 \mathrm{~K} \Omega$ to $100 \mathrm{~K} \Omega$ (see Typical Electrical Data).

This terminal is a low-impedance point, and is internally biased at a dc level equal to $\mathrm{V}_{\mathrm{R}}$. The maximum timing current drawn from pin 12 must be limited to $\leqslant 3 \mathrm{~mA}$ for proper operation of the circuit.

## VCO TIMING CAPACITOR (PINS 13 AND 14)

VCO frequency is inversely proportional to the external timing capacitor, $\mathrm{C}_{0}$, connected across these terminals. $\mathrm{C}_{0}$ must be non-polar, and in the range of 200 pF to $10 \mu \mathrm{~F}$

## VCO FREQUENCY ADJUSTMENT

VCO can be fine-tuned by connecting a potentiometer, $R_{X}$, in series with $R_{0}$ at pin 12 (see Figure 3 ).

## VCO FREE-RUNNING FREQUENCY, $\mathrm{f}_{\mathrm{o}}$.

The XR-2211 does not have a separate VCO output terminal. Instead, the VCO outputs are internally connected to the phase-detector sections of the circuit. However, for set-up or adjustment purposes, VCO free-running frequency can be measured at pin 3 (with $C_{D}$ disconnected), with no input and with pin 2 shorted to pin 10.

## DESIGN EQUATIONS

See Figure 2 for Definitions of Components.

1. VCO Center Frequency, $\mathrm{f}_{\mathrm{O}}$ :
$\mathrm{f}_{0}=1 / \mathrm{R}_{0} \mathrm{C}_{0} \mathrm{~Hz}$
2. Internal Reference Voltage, $\mathrm{V}_{\mathrm{R}}$ (measured at pin 10)
$V_{R}=V^{+} / 2-650 \mathrm{mV}$
3. Loop Lowpass Filter Time Constant, $\tau$ :
$\tau=\mathrm{R}_{1} \mathrm{C}_{1}$
4. Loop Damping, $\zeta$ :
$\zeta=\sqrt[1 / 4]{\frac{c_{0}}{c_{1}}}$
5. Loop Tracking Bandwidth, $\pm \Delta f / f_{0}$ :

$$
\Delta f / f_{0}=R_{0} / R_{1}
$$


6. FSK Data Filter Time Constant, $\tau_{F}$ :

$$
\tau_{F}=R_{F} C_{F}
$$

7. Loop Phase Detector Conversion Gain, $\mathrm{K}_{\phi}$ : $\mathrm{K}_{\phi}$ is the differential dc voltage across pins 10 and 11, per unit of phase error at phase-detector input):
$\mathrm{K}_{\phi}=-2 \mathrm{~V}_{\mathrm{R}} / \pi$ volts $/$ radian
8. VCO Conversion Gain, $K_{0}$ : $\left\langle K_{0}\right.$ is the amount of change in VCO frequency, per unit of dc voltage change at pin 11):
$K_{0}=-1 / V_{R} C_{0} R_{1} H z /$ volt
9. Total Loop Gain, $\mathrm{K}_{\mathrm{T}}$ :
$\mathrm{K}_{\mathrm{T}}=2 \pi \mathrm{~K}_{\phi} \mathrm{K}_{0}=4 / \mathrm{C}_{0} \mathrm{R}_{1} \mathrm{rad} / \mathrm{sec} /$ volt
10. Peak Phase-Detector Current, IA:
$I_{A}=V_{R}($ volts $) / 25 m A$

## APPLICATIONS

## FSK DECODING

Figure 3 shows the basic circuit connection for FSK decoding. With reference to Figures 2 and 3, the functions of external components are defined as follows: $\mathrm{R}_{0}$ and $\mathrm{C}_{0}$ set the PLL center frequency, $\mathrm{R}_{1}$ sets the system bandwidth, and $\mathrm{C}_{1}$ sets the loop-filter-time-constant and the loop damping factor. $C_{F}$ and $R_{F}$ form a one-pole post-detection filter for the FSK data output. The resistor $\mathrm{R}_{\mathrm{B}}(=510 \mathrm{~K} \Omega)$ from pin 7 to pin 8 introduces positive feedback across FSK comparator to facilitate rapid transition between output logic states.

Recommended component values for some of the most commonly used FSK bands are given in Table 1.


Figure 3. Circuit Connection for FSK Decoding

## Design Instructions

The circuit of Figure 3 can be tailored for any FSK decoding application by the choice of five key circuit components; $R_{0}, R_{1}, C_{0}, C_{1}$ and $C_{F}$. For a given set of FSK mark and space frequencies, $f_{1}$ and $f_{2}$, these parameters can be calculated as follows:

1. Calculate PLL center frequency, $\mathrm{f}_{\mathrm{O}}$ :

$$
f_{0}=\frac{f_{1}+f_{2}}{2}
$$

2. Choose value of timing resistor $R_{O}$ to be in the range of $10 \mathrm{~K} \Omega$ to $100 \mathrm{~K} \Omega$. This choice is arbitrary. The recommended value is $R_{0} \cong 20 \mathrm{~K} \Omega$. The final value of $R_{0}$ is normally fine-tuned with the series potentiometer, RX.
3. Calculate value of $\mathrm{C}_{0}$ from Design Equation No. 1 or from Typical Performance Data:
$C_{0}=1 / R_{0} f_{0}$
RAYTHEON
4. Calculate $R_{1}$ to give a $\Delta f$ equal to the mark-space deviation:
$\left.R_{1}=R_{0}\left[f_{0} / f_{1}-f_{2}\right)\right]$
5. Calculate $\mathrm{C}_{1}$ to set loop damping. (See Design Equation No. 4.)

Normally, $\zeta \approx 1 / 2$ is recommended.

Then: $C_{1}=C_{0} / 4$ for $\zeta=1 / 2$
6. Calculate Data Filter Capacitance, $\mathrm{C}_{\mathrm{F}}$ :

For $R_{F}=100 \mathrm{~K} \Omega, R_{B}=510 \mathrm{~K} \Omega$, the recommended value of $\mathrm{C}_{\mathrm{F}}$ is:
$C_{F} \approx 3 /$ Baud Rate) $\mu \mathrm{F}$
Note: All calculated component values except RO can be rounded-off to the nearest standard value, and $R_{O}$ can be varied to fine-tune center frequency through a series potentiometer, $R_{X}$. (See Figure 3.)

## Design Example:

75 Baud FSK demodulator with mark/space frequencies of $1110 / 1170 \mathrm{~Hz}$ :

Step 1: Calculate $\mathrm{f}_{0}: \mathrm{f}_{0}=(1110+1170)(1 / 2)=1140 \mathrm{~Hz}$
Step 2: Choose $\mathrm{R}_{0}=20 \mathrm{~K} \Omega$ ( $18 \mathrm{~K} \Omega$ fixed resistor in series with $5 \mathrm{~K} \Omega$ potentiometer)

Step 3: Calculate $\mathrm{C}_{0}$ from VCO Frequency vs Timing Capacitor: $\mathrm{C}_{0}=0.044 \mu \mathrm{~F}$

Step 4: Calculate $\mathrm{R}_{1}: \mathrm{R}_{1}=\mathrm{R}_{0}(2240 / 60)=380 \mathrm{~K} \Omega$
Step 5: Calculate $\mathrm{C}_{1}: \mathrm{C}_{1}=\mathrm{C}_{0} / 4=0.011 \mu \mathrm{~F}$
Note: All values except $R_{O}$ can be rounded-off to nearest standard value.

Table 1. Recommended Component Values for Commonly Used FSK Bands (See Circuit of Figure 3)

| FSK BAND | COMPONENT VALUES |  |
| :--- | :--- | :--- |
| 300 Baud | $\mathrm{C}_{0}=0.039 \mu \mathrm{~F}$ | $\mathrm{C}_{\mathrm{F}}=0.005 \mu \mathrm{~F}$ |
| $\mathrm{f}_{1}=1070 \mathrm{~Hz}$ | $\mathrm{C}_{1}=0.01 \mu \mathrm{~F}$ | $\mathrm{R}_{0}=18 \mathrm{~K} \Omega$ |
| $\mathrm{f}_{2}=1270 \mathrm{~Hz}$ | $\mathrm{R}_{1}=100 \mathrm{~K} \Omega$ |  |
| 300 Baud | $\mathrm{C}_{0}=0.022 \mu \mathrm{~F}$ | $\mathrm{C}_{\mathrm{F}}=0.005 \mu \mathrm{~F}$ |
| $\mathrm{f}_{1}=2025 \mathrm{~Hz}$ | $\mathrm{C}_{1}=0.0047 \mu \mathrm{~F}$ | $\mathrm{R}_{0}=18 \mathrm{~K} \Omega$ |
| $\mathrm{f}_{2}=2225 \mathrm{~Hz}$ | $\mathrm{R}_{1}=200 \mathrm{~K} \Omega$ |  |



## Figure 4. External Connectors for FSK Demodulation with Carrier-Detect Capability <br> FSK DECODING WITH CARRIER-DETECT

The lock-detect section of the XR-2211 can be used as a carrier-detect option for FSK decoding. The recommended circuit connection for this application is shown in Figure 4. The open-collector lock-detect output, pin 6, is shorted to data output (pin 7). Thus, data output will be disabled at "low" state until there is a carrier within the detection band of the PLL and the pin 6 output goes "high" to enable the data output.

The minimum value of the lock-detect filter capacitance $C_{D}$ is inversely proportional to the capture range, $\pm \Delta f_{\mathrm{c}}$. This is the range of incoming frequencies over which the loop can acquire lock and is always less than the tracking range. It is further limited by $\mathrm{C}_{1}$. For most applications, $\Delta \mathrm{f}_{\mathrm{C}}>\Delta \mathrm{f} / 2$. For $R_{D}=470 \mathrm{~K} \Omega$, the approximate minimum value of $C_{D}$ can be determined by:

$$
C_{D}(\mu F) \geqslant 16 / \text { capture range in } \mathrm{Hz}
$$

With values of $C_{D}$ that are too small, chatter can be observed on the lock-detect output as an incoming signal frequency approaches the capture bandwidth. Excessively-large values of $C_{D}$ will slow the response time of the lock-detect output.

## TONE DETECTION

Figure 5 shows the generalized circuit connection for tone detection. The logic outputs, Q and $\overline{\mathrm{Q}}$ at pins 5 and 6 are normally at "high" and "low" logic states, respectively. When a tone is present within the detection band of the PLL, the logic state at these outputs become reversed for the duration of the input tone. Each logic output can sink 5 mA of load current.

Both logic outputs at pins 5 and 6 are open-collector type stages, and require external pull-up resistors $\mathrm{R}_{\mathrm{L} 1}$ and $\mathrm{R}_{\mathrm{L} 2}$. as shown in Figure 5.


Figure 5. Circuit Connection for Tone Detection

With reference to Figures 2 and 5, the function of the external circuit components can be explained as follows: $R_{0}$ and $C_{0}$ set VCO center frequency; $R_{1}$ sets the detection bandwidth; $\mathrm{C}_{1}$ sets the lowpass-loop filter time constant and the loop damping factor, $R_{L 1}$ and $R_{L 2}$ are the respective pull-up resistors for the $Q$ and $\bar{Q}$ logic outputs.

## Design Instructions

The circuit of Figure 5 can be optimized for any tonedetection application by the choice of the 5 key circuit components: $R_{0}, R_{1}, C_{0}, C_{1}$ and $C_{D}$. For a given input tone frequency, fs, these parameters are calculated as follows:

1. Choose $R_{0}$ to be in the range of $15 \mathrm{~K} \Omega$ to $100 \mathrm{~K} \Omega$. This choice is arbitrary.
2. Calculate $C_{0}$ to set center frequency, $f_{0}$ equal to ${ }^{f} S$ : $C_{0}=1 / R_{0} f$.
3. Calculate $R_{1}$ to set bandwidth $\pm \Delta f$; (see Design Equation No. 5):
$R_{1}=R_{0}\left(f_{0} / \Delta f\right)$
Note: The total detection bandwidth covers the frequency range of $f 0 \pm \Delta f$.
4. Calculate value of $\mathrm{C}_{1}$ for a given loop damping factor:

$$
C_{1}=C_{0} / 16 \zeta^{2}
$$

Normally $\zeta \approx 1 / 2$ is optimum for most tone-detector applications, giving $\mathrm{C}_{1}=0.25 \mathrm{C}_{0}$.

Increasing $\mathrm{C}_{1}$ improves the out-of-band signal rejection, but increases the PLL capture time.
5. Calculate value of filter capacitor $C_{D}$. To avoid chatter at the logic output, with $R_{D}=470 \mathrm{~K} \Omega$, $C_{D}$ must be:
$C_{D}(\mu \mathrm{~F}) \geqslant(16 /$ capture range in Hz$)$
Increasing $C_{D}$ slows the logic output response time.

## Design Examples:

Tone detector with a detection band of $1 \mathrm{kHz} \pm 20 \mathrm{~Hz}$ :
Step 1: Choose $R_{0}=20 \mathrm{~K} \Omega(18 \mathrm{~K} \Omega$ in series with $5 \mathrm{~K} \Omega$ potentiometer).

Step 2: Choose $C_{0}$ for $f_{0}=1 \mathrm{kHz}$ :
$\mathrm{C}_{0}=0.05 \mu \mathrm{~F}$.
Step 3: Calculate $R_{1}: R_{1}=\left(R_{0}\right)(1000 / 20)=1 \mathrm{M} \Omega$.
Step 4: Calculate $\mathrm{C}_{1}$ : for $\zeta=1 / 2, \mathrm{C}_{1}=0.25 \mu \mathrm{~F}$, $\mathrm{C}_{0}=0.013 \mu \mathrm{~F}$.

Step 5: Calculate $C_{D}: C_{D}=16 / 38=0.42 \mu \mathrm{~F}$.
Step 6: Fine-tune center frequency with $5 \mathrm{~K} \Omega$ potentiometer, RX.

## LINEAR FM DETECTION



Note: See section on Design Equations for Component Values.
Figure 6. Linear FM Detector Using XR-2211 and an External Op Amp

## LINEAR FM DETECTION

The XR-2211 can be used as a linear FM detector for a wide range of analog communications and telemetry applications. The recommended circuit connection for the application is shown in Figure 6. The demodulated output is taken from the loop phase detector output (pin 11), through a post detection filter made up of $R_{F}$ and $C_{F}$, and an external buffer amplifier. This buffer amplifier is necessary because of the high impedance output at pin 11. Normally, a noninverting unity gain op amp can be used as a buffer amplifier, as shown in Figure 6.

The FM detector gain, i.e., the output voltage change per unit of FM deviation, can be given as:

$$
V_{\text {out }}=R_{1} V_{R} / 100 R_{0} \text { Volts/\%deviation }
$$

where $\mathrm{V}_{\mathrm{R}}$ is the internal reference voltage. $\left(\mathrm{V}_{\mathrm{R}}=\mathrm{V}^{+} / 2\right.$ 650 mV ). For the choice of external components $\mathrm{R}_{1}, \mathrm{R}_{0}$, $C_{D}, C_{1}$ and $C_{F}$, see section on Design Equations.

## AVAILABLE TYPES

| Part Number | Package | Operating Temperature |
| :--- | :--- | :---: |
| XR-2211M | Ceramic | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| XR-2211N | Ceramic | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| XR-2211P | Plastic | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| XR-2211CN | Ceramic | $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ |
| XR-2211CP | Plastic | $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ |

## DESCRIPTION

The XR-2567 is a dual monolithic tone decoder of the 567-type that is ideally suited for tone or frequency decoding in multiple-tone communication systems. Each decoder of the XR-2567 can be used independently or both sections can be interconnected for dual operation. The matching and temperature tracking characteristics between decoders on this monolithic chip are superior to those available from two separate tone-decoder packages.

The XR-2567 operates over a frequency range of 0.01 Hz to 500 kHz . Supply voltages can vary from 4.5 V to 12 V , with internal voltage regulation provided for supplies between 7 V and 12 V . A functional block diagram of the complete monolithic system is shown below. Each decoder consists of a phase-locked loop (PLL), a quadrature AM detector, a voltage comparator, and a logic compatible output that can sink more than 100 mA of load current.

The center frequency of each decoder is set by an external resistor and capacitor which determine the free-running frequency of each PLL. When an input tone is present within the passband of the circuit, the PLL "locks" on the input signal. The logic output, which is normally "high", then switches to a "low" state during this "lock" condition.

## FEATURES

- Replaces two 567-type decoders
- Excellent temperature tracking between decoders
- Bandwidth adjustable from 0 to $14 \%$
- Logic compatible outputs with 100 mA sink capability
- Center frequency matching (1\% typical)
- Center frequency adjustable from 0.01 Hz to 500 kHz
- Inherent immunity to false triggering
- Frequency range adjustable over 20:1 range by external resistor


## APPLICATIONS

- Touch-Tone ${ }^{\circledR}$ Decoding
- Sequential Tone Decoding
- Dual-Tone Decoding/Encoding
- Communications Paging
- Ultrasonic Remote-Control and Monitoring
- Full-Duplex Carrier-Tone Transceiver
- Wireless Intercom
- Dual Precision Oscillator
- FSK Generation and Detection


## SCHEMATIC DIAGRAM



## ELECTRICAL CHARACTERISTICS

Test Conditions: $\mathrm{V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise specified.
Test circuit of Figure 1, $\mathrm{S}_{1}$ closed unless otherwise specified.

| PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| GENERAL |  |  |  |  |  |
| Supply Voltage Range Without Regulator With Internal Regulator | See Figure 1, $\mathrm{S}_{1}$ closed See Figure 1, $\mathrm{S}_{1}$ open | $\begin{aligned} & 4.75 \\ & 6.5 \\ & \hline \end{aligned}$ |  | $\begin{array}{r} 7 \\ 12 \\ \hline \end{array}$ | Vdc <br> Vdc |
| Supply Current (both decoders) Quiescent $\times R-2567 \mathrm{M}$ XR-2567C Activated XR-2567M XR-2567C | See Typical Performance Data $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=20 \mathrm{~K} \Omega \\ & \mathrm{R}_{\mathrm{L}}=20 \mathrm{~K} \Omega \\ & \mathrm{R}_{\mathrm{L}}=20 \mathrm{~K} \Omega \\ & \mathrm{R}_{\mathrm{L}} \quad 20 \mathrm{~K} \Omega \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 12 \\ & 14 \\ & 22 \\ & 24 \\ & \hline \end{aligned}$ | $\begin{aligned} & 16 \\ & 20 \\ & 26 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \\ & \hline \end{aligned}$ |
| Output Voltage |  |  |  | 15 | V |
| Negative Voltage at Input |  |  |  | -10 | V |
| Positive Voltage at Input |  |  |  | $\mathrm{V}_{\mathrm{cc}}+0.5$ | V |
| CENTER FREQUENCY* |  |  |  |  |  |
| Highest Center Frequency |  | 100 | 500 |  | kHz |
| $\begin{aligned} & \text { Center Frequency Stability } \\ & \text { Temperature } \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \\ & 0<\mathrm{T}_{\mathrm{A}}<+75^{\circ} \mathrm{C} \\ & -55^{\circ}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C} \end{aligned}$ | See Typical Performance Data See Typical Performance Data See Typical Performance Data |  | $\begin{array}{r} 35 \\ \pm 60 \\ \pm 140 \end{array}$ |  |  |
|  | $\begin{aligned} \mathrm{f}_{\mathrm{O}} & =100 \mathrm{kHz} \\ \mathrm{f}_{\mathrm{O}} & =100 \mathrm{kHz} \\ \mathrm{f}_{\mathrm{O}} & =100 \mathrm{kHz}, \mathrm{~V}+=9 \mathrm{~V} \\ \mathrm{f}_{\mathrm{O}} & =100 \mathrm{kHz}, \mathrm{~V}+=9 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 0.5 \\ & 0.7 \\ & 0.05 \\ & 0.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0 \\ & 2.0 \end{aligned}$ | $\begin{aligned} & \% / V \\ & \% / V \\ & \% / V \\ & \% / V \end{aligned}$ |
| DETECTION BANDWIDTH* |  |  |  |  |  |
| Largest Detection Bandwidth XR-2567M <br> XR-2567C | $\begin{aligned} & \mathrm{f}_{\mathrm{O}}=100 \mathrm{kHz} \\ & \mathrm{f}_{\mathrm{O}}=100 \mathrm{kHz} \end{aligned}$ | $\begin{aligned} & 12 \\ & 10 \\ & \hline \end{aligned}$ | $\begin{aligned} & 14 \\ & 14 \end{aligned}$ | $\begin{aligned} & 16 \\ & 18 \\ & \hline \end{aligned}$ | $\begin{aligned} & \% \text { of } \mathrm{f}_{\mathrm{o}} \\ & \% \text { of } \mathrm{f}_{\mathrm{O}} \end{aligned}$ |
| Largest Detection Bandwidth Skew <br> XR-2567M <br> XR-2567C |  |  | 1 1 | 2 <br> 3 | $\begin{aligned} & \% \text { of } \mathrm{f}_{\mathrm{o}} \\ & \% \text { of } \mathrm{f}_{\mathrm{O}} \\ & \hline \end{aligned}$ |
| Largest Detection Bandwidth Variation Temperature Supply Voltage | $\begin{aligned} & V_{\text {in }}=300 \mathrm{mV} \mathrm{rms} \\ & V_{\text {in }}=300 \mathrm{mV} \mathrm{rms} \end{aligned}$ |  | $\begin{aligned} & \pm 0.1 \\ & \pm 2 \end{aligned}$ |  | $\begin{aligned} & \% /{ }^{\circ} \mathrm{C} \\ & \% / \mathrm{V} \end{aligned}$ |
| INPUT* |  |  |  |  |  |
| Input Resistance |  |  | 20 |  | k $\Omega$ |
| Smallest Detectable Input Voltage | $\mathrm{I}_{\mathrm{L}}=100 \mathrm{~mA}, \mathrm{f}_{\mathrm{i}}=\mathrm{f}_{\mathrm{O}}$ |  | 20 | 25 | mV rms |
| Largest No-Output Input Voltage | $\mathrm{I}_{\mathrm{L}}=100 \mathrm{~mA}, \mathrm{f}_{\mathrm{i}}=\mathrm{f}_{\mathrm{O}}$ | 10 | 15 |  | mV rms |
| Greatest Simultaneous Outband Signal to Inband Signal Ratio |  |  | +6 |  | dB |
| Minimum Input Signal to Wideband Noise Ratio | Noise Bw $=140 \mathrm{kHz}$ |  | -6 |  | dB |
| OUTPUT* |  |  |  |  |  |
| Output Saturation Voltage | $\begin{aligned} & I_{\mathrm{L}}=30 \mathrm{~mA}, \mathrm{~V}_{\text {in }}=25 \mathrm{mV} \mathrm{rms} \\ & \mathrm{I}_{\mathrm{L}}=100 \mathrm{~mA}, \mathrm{~V}_{\text {in }}=25 \mathrm{mV} \mathrm{rms} \end{aligned}$ |  | $\begin{aligned} & 0.2 \\ & 0.6 \end{aligned}$ | $\begin{aligned} & 0.4 \\ & 1.0 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| Output Leakage Current |  |  | 0.01 | 25 | $\mu \mathrm{A}$ |
| Fastest ON-OFF Cycling Rate |  |  | fo/20 |  |  |
| Output Rise Time | $\mathrm{R}_{\mathrm{L}}=50 \Omega$ |  | 150 |  | ns |
| Output Fall Time | $\mathrm{R}_{\mathrm{L}}=50 \Omega$ |  | 30 |  | ns |
| MATCHING CHARACTERISTICS |  |  |  |  |  |
| Center Frequency Matching | $\mathrm{f}_{\mathrm{O}}=10 \mathrm{kHz}$ |  | 1 |  | \% |
| Temperature Drift Matching | $\begin{aligned} & 0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<75^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C}<\mathrm{T}_{A}<125^{\circ} \mathrm{C} \end{aligned}$ |  | $\begin{aligned} & \pm 20 \\ & \pm 50 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \\ & \mathrm{ppm} /{ }^{\circ} \mathrm{C} \end{aligned}$ |

[^6]
## ABSOLUTE MAXIMUM RATINGS

| Power Supply |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| With Internal Regulator . . . . . . . . 14 V |  |  |  |  |
| Without Regulator (Pins 12 and 13 shorted) . . 10V |  |  |  |  |
| Power Dissipation |  |  |  |  |
| Ceramic Package . . . . . . . . . . 750 mW |  |  |  |  |
| Derate above $+25^{\circ} \mathrm{C}$. . . . . . . $6 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ |  |  |  |  |
| Plastic Package |  |  |  |  |
| Derate above $+25^{\circ} \mathrm{C}$. . . . . . . $5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ |  |  |  |  |
| Temperature |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
| Storage . . . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |  |  |  |  |

CONNECTION INFORMATION


## TYPICAL PERFORMANCE DATA



Internal Power Dissipation vs Supply Voltage. Both Units Activated, $R_{L}=20 \mathrm{~K}$


Total Supply Current vs Supply Voltage for Operation with Internal Regulator (Pins 12 and 13 Not Connected)


Power Supply Dependence of Center Frequency


Largest Detection Bandwidth vs Operating Frequency


Total Supply Current vs Supply Voltage for Operation Without Internal Regulator (Pins 12 and 13 Shorted)


Bandwidth vs Input Signal Amplitude ( $C_{2}$ in $\mu F$ )

## TYPICAL PERFORMANCE DATA (Cont)



Greatest Number of Cycles Before Output


Detection Bandwidth as a Function of $C_{2}$ and $C_{3}$


Bandwidth Variation With Temperature


Frequency Drift With
Temperature


Temperature Coefficient of Center Frequency (Mean and S.D.)


Figure 1. Test Circuit


Figure 2. XR-2567 Typical Response

## DEFINITIONS OF THE XR-2567 PARAMETERS

The center frequency, $\mathrm{f}_{0}$, is the free-running frequency of the current-controlled oscillator of the PLL with no input signal. It is determined by resistor $\mathrm{R}_{1}$ and capacitor $\mathrm{C}_{1}$; $f_{0}$ can be approximateed by

$$
\mathrm{f}_{0} \approx \frac{1}{R_{1} C_{1}} \mathrm{~Hz}
$$

where $R_{1}$ is in ohms and $C_{1}$ is in farads.

The detection bandwidth is the frequency range centered about $\mathrm{f}_{0}$, within which an input signal larger than the threshold voltage (typically 20 mV rms ) will cause a "logic zero" state at the output. The detection bandwidth corresponds to the capture range of the PLL and is determined by the lowpass bandwidth filter. The bandwidth of the filter, as a percent of $\mathrm{f}_{\mathrm{O}}$, can be determined by the approximation

where $V_{i}$ is the input signal in volts, rms, and $C_{2}$ is the capacitance in $\mu \mathrm{F}$ at pins 10 or 15 .
The largest detection bandwidth is the largest frequency range within which an input signal above the threshold voltage will cause a logical zero state at the output. The maximum detection bandwidth corresponds to the lock range of the PLL.

The detection band skew is a measure of how accurately the largest detection band is centered about the center frequency $f_{0}$. It is defined as ( $f_{\max }+f_{\min }-2 f_{0}$ )/fo, where $f_{\text {max }}$ and $f_{\text {min }}$ are the frequencies corresponding to the edges of the detection band. If necessary, the detection band skew can be reduced to zero by an optional centering adjustment. (See Optional Controls.)

## DESCRIPTION OF CIRCUIT CONTROLS

## INPUT (PINS 11 AND 14)

The input signal is applied to pins 14 and/or 11 through a coupling capacitor, $\mathrm{C}_{\mathrm{C}}$. These terminals are internally biased at a dc level 2 volts above ground and they have an input impedance level of approximately $20 \mathrm{~K} \Omega$.

TIMING RESISTOR R1 AND CAPACITOR $\mathbf{C}_{1}$
(PINS 1, 8, 9, and 16)
The center frequency, $f 0$, of each decoder section is set by a resistor $R_{1}$ and a capacitor $C_{1} . R_{1 A}$ is connected between pins 1 and 16 in decoder section $A$, and $R_{1 B}$ between pins 8 and 9 of decoder section $\mathrm{B} . \mathrm{C}_{1 \mathrm{~A}}$ is connected from pin 1 to ground, and $\mathrm{C}_{1 \mathrm{~B}}$ from pin 8 to ground, as shown in Figure 3. $\mathrm{R}_{1}$ and $\mathrm{C}_{1}$ should be selected for the desired center frequency by the expression $f_{0} \approx 1 / R_{1} C_{1}$. For optimum temperature stability, $\mathrm{R}_{1}$ should be selected such that $2 K \Omega \leqslant R_{1} \leqslant 20 K \Omega$, and the $R_{1} C_{1}$ product should have sufficient stability over the projected operating temperature range.

For decoder section $A$, the oscillator output can be obtained at either pin 1 or 16 . Pin 16 is the oscillator squarewave output which has a magnitude of approximately $\mathrm{V}_{\mathrm{CC}}-1.4 \mathrm{~V}$ and an average dc level of $\mathrm{V}_{\mathrm{CC}} / 2$. A $1 \mathrm{~K} \Omega$ load may be driven from this point. The voltage at pin 1 is an exponential triangle waveform with a peak-to-peak amplitude of 1 volt and an average dc level of $\mathrm{V}_{\mathrm{CC}} / 2$. Only high impedance loads should be connected to pin 1 to avoid disturbing the temperature stability or duty cycle of the oscillator. For section B, pin 9 is the squarewave output and pin 8 the exponential triangle waveform output.


Figure 3. Circuit Connection Diagram

## LOOP FILTER, $\mathrm{C}_{2}$ (PINS 10 and 15)

Capacitors $C_{2 A}$ and $C_{2 B}$ connected from pins 15 and 10 to ground are the single-pole, lowpass filters for the PLL portion of decoder sections A and B . The filter time constant is given by $T_{2}=R_{2} C_{2}$, where $R_{2}(10 \mathrm{~K} \Omega)$ is the impedance at pins 10 or 15 . The selection of $\mathrm{C}_{2}$ is determined by the detection bandwidth requirements and input signal amplitude as shown in the Curves. One approach is to select an area of operation from the graph and then adjust the input level and value of $\mathrm{C}_{2}$ accordingiy. Or, if the input amplitude variation is known, the required $\mathrm{f}_{0} \mathrm{C}_{2}$ product can be found to give the desired bandwidth. Constant bandwidth operation requires $\mathrm{V}_{\mathrm{i}}>200 \mathrm{mV}$ rms. Then, as noted in the Curves, bandwidth will be controlled solely by the $\mathrm{f}_{0} \mathrm{C}_{2}$ product. (For additional information, see Optional Controls Section, "Speed of Response" and "Bandwidth Reduction".)

Pins 10 and 15 correspond to the PLL phase detector outputs of sections A and B, respectively. The voltage level at these pins is a linear function of frequency over the range of 0.95 to $1.05 \mathrm{f}_{0}$, with a slope of approximately $20 \mathrm{mV} / \%$ frequency deviation.

## OUTPUT FILTER, $\mathrm{C}_{3}$ (PINS 2 AND 7)

Capacitors $C_{3 A}$ and $C_{3 B}$ connected from pins 2 and 7 to ground form lowpass post detection filters for sections $A$ and $B$ respectively. The function of the post detection filter is to eliminate spurious outputs caused by out-of-band signals. The time constant of the filter can be expressed as $T_{3}=R_{3} C_{3}$, where $R_{3}(4.7 K)$ is the internal impedance at pins 2 or 7 .

The precise value of $\mathrm{C}_{3}$ is not critical for most applications. To eliminate the possibility of false triggering by spurious signals, a minimum value for $\mathrm{C}_{3}$ is $2 \mathrm{C}_{2}$, where $\mathrm{C}_{2}$ is the loop filter capacitance for the corresponding decoder section. If $\mathrm{C}_{3}$ is smaller than $2 \mathrm{C}_{2}$, then frequencies adjacent to the detection band may switch the output stage "off" and "on" at the beat frequency, or the output may pulse "off" and "on" during the turn-on transient.

If the value of $C_{3}$ becomes too large, the turn-on or turn-off time of the output stage will be delayed until the voltage change across $C_{3}$ reaches the threshold voltage. In certain applications, this delay may be desirable as a means of suppressing spurious outputs. (For additional information, see Optional Controls Section, "Speed of Response" and "Chatter".)

## LOGIC OUTPUT (PINS 3 AND 6)

Output terminals 3 and 6 provide a binary logic output when an input signal tone is present within the detectionband of each respective decoder section. The logic outputs are uncommitted "bare-collector" power transistors capable of switching high current loads. The current level at the output is determined by an external load resistor, $R_{L}$, connected from $V_{C C}$ to pins 3 and 6.

When an in-band signal is present, the output transistor at pins 3 or 6 saturates with a collector voltage less than 1 volt (typically 0.6 V ) at full rated current of 100 mA . If large output voltage swings are needed, $\mathrm{R}_{\mathrm{L}}$ can be connected to a supply voltage, $\mathrm{V}^{+}$higher than the $\mathrm{V}_{\mathrm{CC}}$ supply. For safe operation, $\mathrm{V}^{+} \leqslant 15$ volts.

## REGULATOR BYPASS (PIN 12)

This pin corresponds to the output of the voltage regulator section. For circuit operation with a supply voltage greater than 7 V , pin 12 should be ac grounded with a bypass capacitor $\geqslant 1 \mu \mathrm{~F}$. For circuit operation over a supply voltage range of 4.5 to 7 V , the voltage regulator section is not required; pin 12 should be shorted to $\mathrm{V}_{\mathrm{CC}}$.

## GROUND TERMINALS (PINS 4 AND 5)

To eliminate parasitic interaction, each decoder section has a separate ground terminal. The internal regulator shares a common ground with decoder section A (pin 4).

Independent ground terminals also allow additional flexibility for split supply operation. Pin 4 can be used as $\mathrm{V}^{-}$, and pin 5 as ground, as shown in Figure 4. When the circuit is operated with split supplies, the positive supply should always be $>6 \mathrm{~V}$, and the dc potential across pins 13 and 14 should not exceed 15 volts.


Figure 4. Split-Supply Operation Using Independent Ground Terminals of Units $A$ and $B$. Unit $A$ Operates Between $V^{+}$and $V^{-}$, Unit B Operates Between $V^{+}$and Ground

## OPTIONAL CONTROLS

## SPEED OF RESPONSE

The minimum lock-up time is inversely related to the loop frequency. As the natural loop frequency is lowered, the turn-on transient becomes greater. Thus, maximum operating speed is obtained when the value of capacitor $\mathrm{C}_{2}$ is minimum. At the instant an input signal is applied, its phase may drive the oscillator away from the incoming frequency rather than toward it. Under this condition, the lock-up transient is in a worst case situation, and the minimum theoretical lock-up time will not be achievable.

The following expressions yield the values of $C_{2}$ and $C_{3}$, in microfarads, which allow the maximum operating speeds for various center frequencies. The minimum rate that digital information may be detected without losing information due to turn-on transient or output chatter is about 10 cycles/ bit, which corresponds to an information transfer rate of $\mathrm{f}_{0} / 10$ Baud.

$$
c_{2}=\frac{130}{f_{0}}, \quad c_{3}=\frac{260}{f_{0}}
$$

In situations where minimum turn-off time is of less importance than fast turn-on, the optional sensitivity adjustment circuit of Figure 5 can be used to bring the quiescent C3 voltage closer to the threshold voltage. Sensitivity to beat frequencies, noise, and extraneous signals, however, will be increased.

## CHATTER

When the value of $\mathrm{C}_{3}$ is small, the lock transient and ac components at the lock detector output may cause the output stage to move through its threshold more than once, resulting in output chatter.


Figure 5. Optional Connections for Sensitivity Control

Although some loads, such as lamps and relays will not respond to chatter, "logic" may interpret chatter as a series of output signals. Chatter can be eliminated by feeding a portion of the output back to the input or by increasing the size of capacitor $C_{3}$. Generally, the feedback method is preferred since keeping $\mathrm{C}_{3}$ small will enable faster operation. Three alternate schemes for chatter prevention are shown in Figure 6. Generally, it is only necessary to assure that the feedback time constant does not get so large that it prevents operation at the highest anticipated speed.


Figure 6. Methods of Reducing Chatter

## SKEW ADJUSTMENT

The circuits shown in Figure 7 can be used to change the position of the detection band (capture range) within the largest detection band (or loop range). By moving the detection band to either edge of the lock range, input signal variations will expand the detection band in one direction only. Since $\mathrm{R}_{3}$ also has a slight effect on the duty cycle, this approach may be useful to obtain a precise duty cycle when the circuit is used as an oscillator.


Figure 7. Connections to Reposition Detection Band

## OUTPUT LATCHING

After a signal is received, the output of either decoder section can be latched "on" by connecting a $20 \mathrm{~K} \Omega$ resistor and diode from the "output" terminal to the "output filter" terminal as shown in Figure 8. The output stage can be unlatched by raising the voltage level at the output filter terminal.


Figure 8. Output Latching

## POSITIONING OF DETECTION BANDS

Figure 9 defines the respective band-edge and band-center frequencies for sections $A$ and $B$ of the dual tone decoder. Frequencies $f_{L}$ and $f_{H}$ with appropriate subscripts refer to the low and the high band-edge frequencies for decoder section $A$ and $B$, and $f_{0}$ is the center frequency.


Figure 9. Positioning of Detection Bands

The two sections can be interconnected to form a single-tone detector with an overall detection bandwidth equal to the sum of the difference of the detection bands for the two individual detector sections. For example, if the individual decoder sections are interconnected as shown in Figure 13, then the total detection bandwidth would be approximately equal to the sum of the respective bandwidths as shown in Figure 9 (b). Similarly, if the decoders are interconnected as shown in Figure 11, then the overall detection band would be equal to the difference, or the overlap, between the respective bandwidths as shown in Figure 9 (c).

## BANDWIDTH REDUCTION

The bandwidth of each decoder can be reduced by either increasing the loop filter capacitor $\mathrm{C}_{2}$ or reducing the loop gain. Increasing $\mathrm{C}_{2}$ may be an undesirable solution since this will also reduce the damping of the loop and thus slow the circuit response time.


Figure 10. Bandwidth Reduction

Figure 10 shows the proper method of reducing the loop gain for reduced bandwidth. This technique will improve damping and permit faster performance under narrow band operation.

Bandwidth reduction can also be obtained by subtracting over-lapping bandwidths of the two decoder sections (see Figures 9 (c) and 11).

## APPLICATIONS

## DUAL-TONE DETECTION

In most dual-tone detection systems, the decoder output is required to change state only when both input tones are present simultaneously. This can be implemented by setting the detection bandwidth of each of the XR-2567 decoder sections to cover one of the input tones; and then connecting the respective outputs through a NOR gate, as shown in Figure 11. In this case, the output of the NOR gate will be "high" only when both input tones are present simultaneously.

Figure 12 shows additional circuit configurations which can be used for decoding multiple-tone input signals. In Figure 12 (a), the output of Unit $A$ is connected to the output filter (pin 7) of Unit B through the diode $D_{1}$. If no input tone is present within the detection-band of Unit $A$, then its output ( $\operatorname{pin} 3$ ) is "high", which keeps diode $D_{1}$ conducting and "disables" Unit B by keeping its output (pin 6) "high". If an input tone is present within the detectionband of Unit A, pin 3 is low, diode $\mathrm{D}_{1}$ is reverse biased, and decoder $B$ is no longer disabled. If under these conditions an input signal is present within the detection-band of Unit B, then its output at pin 6 would be "low". Thus, the output at pin 6 is "low" only when input tones within the detection-band of $A$ and $B$ are present simultaneously.

The dual-tone decoder circuit of Figure 12 (b) makes use of the split-ground feature of the XR-2567. The output terminal of Unit A is used as a "switch" in series with the ground terminal (pin 5) of Unit B. If the input tone A is not present, pin 3 is at its high-impedance state, and the ground terminal of Unit $B$ is open-circuited. When the input tone $A$ is present, pin 3 goes to a low-impedance state and Unit B is activated. In this manner, the output of Unit $B$ will be "low" only when both tones A and B are present.

In the circuit connection of Figure 12 (b), Unit B does not draw any current until it is activated. Therefore, its power dissipation in a stand-by condition is lower than other dual-tone decoder configurations. However, due to finite series resistance between pin 3 and ground when Unit B is activated, the output current sink capability is limited to $\leqslant 10 \mathrm{~mA}$.


Figure 11. Connections for Decoding Dual-Tone Encoded Input Signals.


Figure 12. Additional Dual-Tone Decoding Circuits

## SEQUENTIAL TONE DECODING

Dual-tone detector circuits can also be used for sequential tone decoding where one tone must be present before the other for the circuit to operate. This can be achieved by making the output filter capacitance, $\mathrm{C}_{3}$, of one of the sections larger with respect to the other. For example, in the circuits of Figure 12 (a) and 13 (b), if $C_{3 A}$ is chosen to be much larger than $\mathrm{C}_{3} \mathrm{~B}\left(\mathrm{C}_{3} \mathrm{~A} \geqslant \mathrm{C}_{3} \mathrm{~B}\right)$, then Unit A will remain "on" and activate $B$ for a finite time duration after tone $A$ is terminated. Thus, the circuit wiil be abie to detect the two tones only if they are present sequentially, with tone $A$ preceding tone $B$.

The circuit of Figure 12 (a) can also be modified for sequential tone decoding by addition of a diode, $\mathrm{D}_{2}$, between pins 3 and 6. Once activated by Unit A, Unit B will stay "on" as long as tone B is present, even though tone A may terminate. Once tone B disappears, the circuit is reset to its original state and would require tone $A$ to be present for activation.

## HIGH-SPEED NARROW-BAND TONE DECODER

The circuit of Figure 11 can be used as a narrow-band tone decoder by overlapping the detection bands of Units $A$ and $B$ (see Figure 9 (c)). The output of the NOR gate will be high only when an input signal is present within the overlapping portions of the detection band. To maintain uniform response within the passband, the input signal amplitude should be $\geqslant 80 \mathrm{mV}$ rms. For minimum response time, PLL filter capacitors $\mathrm{C}_{2} A$ and $\mathrm{C}_{2} \mathrm{~B}$ should be:

$$
C_{2 A}=C_{2 B} \cong \frac{130}{f_{0}(H z)} \mu F
$$

Under this condition, the worst-case output delay is $\approx 10$ to 14 cycles of the input tone.

The practical matching and tracking tolerances of individual units limit the minimum bandwidth to $\approx 4 \%$ of fo .

## WIDEBAND DECODER

Figure 13 is a circuit configuration for increasing the detection bandwidth of the XR-2567 by combining the respective bandwidths of individual decoder sections. If the detection bands of each section are located adjacent to each other as shown in Figure 9 (b), and if the two outputs (pins 3 and 6) are shorted together, then the resulting bandwidth is the sum of individual bandwidths. In this manner, the total detection bandwidth can be increased to $24 \%$ of center frequency. To maintain uniform response throughout the passband, the input signal level should be $\geqslant 80 \mathrm{mV} \mathrm{rms}$, and the respective passbands of each section should have $\approx 3 \%$ overlap at center frequency.


Figure 13. Wide-Band Tone Detection

## TONE TRANSCEIVER

The XR-2567 can be used as a full-duplex tone transceiver by using one section of the unit as a tone detector and the remaining section as a tone generator. Since both sections operate independently, the circuit can transmit and receive simultaneously. A recommended circuti connection for transceiver applications is shown in Figure 14. In this case, Unit A is utilized as the receiver and Unit B is used as the transmitter. The transmitter section can be keyed "on" and "off" by applying a pulse to pin 8 through a disconnect diode $\mathrm{D}_{1}$. The oscillator section of Unit B will be keyed "off' when the keying logic level at pin 8 is at a "low" state.

The output of the transmitter section (Unit B) can also be frequency modulated over a $+6 \%$ deviation range by applying a modulation signal to pin 10.


Figure 14. Tone Transceiver

## HIGH CURRENT OSCILLATOR

The oscillator output of each section of XR-2567 can be amplified using the high current logic driver sections of the circuit. In this manner, each section of the circuit can switch 100 mA loads, without sacrificing oscillator stability. A recommended circuit connection for this application is shown in Figure 15. The oscillator frequency can be modulated over $\pm 6 \%$ of $f 0$ by applying a control voltage to pins 15 or 10.


## AVAILABLE TYPES

| Part Number | Package | Operating Temperature |
| :--- | :--- | :---: |
| $X R-2567 \mathrm{M}$ | Ceramic | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| $X R-2567 \mathrm{CN}$ | Ceramic | $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ |
| $X R-2567 \mathrm{CP}$ | Plastic | $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ |

Figure 15. Precision Oscillator with High Current Output Capability

## GENERAL DESCRIPTION

The RC4151 and RM4151 provide a simple low-cost method of $A / D$ conversion. They have all the inherent advantages of the voltage-to-frequency conversion technique. The output of RC4151/RM4151 is a series of pulses of constant duration. The frequency of the pulses is proportional to the applied input voltage. These converters are designed for use in a wide range of data conversion and remote sensing applications.

## DESIGN FEATURES

- Single Supply Operation ( +8 V to +22 V )
- Pulse Output Compatible With All Logic Forms
- Programmable Scale Factor (K)
- Linearity $\pm 0.05 \%$ typical - precision mode
- Temperature stability $\pm 100 \% \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ typical
- High Noise Rejection
- Inherent Monotonicity
- Easily Transmittable Output
- Simple Full Scale Trim
- Single-Ended Input, Referenced to Ground
- Also Provides Frequency-to-Voltage Conversion

SCHEMATIC DIAGRAM


## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Supply Voltages . . . . . . . . . . . . . . . . . . . . . . . . . +22 V | Storage Temperature Range |  |
| :---: | :---: | :---: |
| Output Sink Current . . . . . . . . . . . . . . . . . . . . 20 mA | RM4151 | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Internal Power Dissipation . . . . . . . . . . . . . . 500mW | RV4151 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Input Voltage : . . . . . . . . . . . . . . -0.2 V to $+\mathrm{V}_{\mathrm{CC}}$ | RC4151 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Output Short Circuit to Ground . . . . . . . . Continuous | Operating Temperature Range |  |
|  | RM4151 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
|  | RV4151 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
|  | RC4151 | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS ( $\mathrm{V}_{\mathrm{CC}}=+15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified)

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Supply Current | $8 \mathrm{~V}<\mathrm{V}_{\mathrm{CC}}<15 \mathrm{~V}$ |  | 3.5 | 6.0 | mA |
|  | $15 \mathrm{~V}<\mathrm{V}_{\mathrm{CC}}<22 \mathrm{~V}$ | 2.0 | 4.5 | 7.5 | mA |
| Conversion Accuracy Scale Factor | Circuit Figure 3, $\mathrm{V}_{\mathrm{I}}=10 \mathrm{~V}$ $\mathrm{R}_{\mathrm{S}}=14.0 \mathrm{k}$ | 0.90 | 1.00 | 1.10 | kHz/V |
| Drift with Temperature | Circuit Figure 3, $\mathrm{V}_{1}=10 \mathrm{~V}$ | - | $\pm 100$ | - | ppM/oC |
| Drift with VCC | Circuit Figure 3, $\mathrm{V}_{1}=1.0 \mathrm{~V}$ $8 V<V_{C C}<18 V$ | - | 0.2 | 1.0 | \%/V |
| Input Comparator Offset Voltage |  | - | 5 | 10 | mV |
| Offset Current |  | - | $\pm 50$ | $\pm 100$ | nA |
| Input Bias Current |  | - | -100 | -300 | nA |
| Common Mode Range (Note 1) |  | 0 | 0toVCC-2 | VCC-3.0 | V |
| One-Shot Threshold Voltage, Pin 5 |  | 0.63 | . 667 | 0.70 | $\times \mathrm{VCC}$ |
| Input Bias Current, Pin 5 |  | - | -100 | -500 | nA |
| Reset V ${ }_{\text {SAT }}$ | $\operatorname{Pin} 5,1=2.2 \mathrm{~mA}$ | - | 0.15 | 0.50 | V |
| Current Source Output Current ( $\mathrm{RS}=14.0 \mathrm{k} \Omega$ ) | Pin 1, Figure 2, $\mathrm{V}=0$ | - | 138.7 | - | $\mu \mathrm{A}$ |
| Change with Voltage | Pin $1, V=0 \mathrm{~V}$ to $\mathrm{V}=10 \mathrm{~V}$ | - | 1.0 | 2.5 | $\mu \mathrm{A}$ |
| Off Leakage | Pin 1, V $=0 \mathrm{~V}$ | - | 1 | 50.0 | nA |
| Reference Voltage | Pin 2, Figure 2 | 1.70 | 1.9 | 2.08 | V |
| Logic Output VSAT | $\operatorname{Pin} 3,1=3.0 \mathrm{~mA}$ | - | 0.15 | 0.50 | V |
| $\mathrm{V}_{\text {SAT }}$ | $\operatorname{Pin} 3,1=2.0 \mathrm{~mA}$ | - | 0.10 | 0.30 | V |
| Off Leakage |  | - | . 1 | 1.0 | $\mu \mathrm{A}$ |

Note 1: Input Common Mode Range includes ground

## PRINCIPLE OF OPERATION

## Single Supply Mode Voltage-to-Frequency Conversion

In this application the RC4151/RM4151 functions as a standalone voltage to frequency converter operating on a single positive power supply. Refer to Figure 2, the simplified block diagram. The RC/RM4151 contains a voltage comparator, a one-shot, and a precision switched current source. The voltage comparator compares a positive input voltage applied at pin 7 to the voltage at pin 6 . If the input voltage is higher, the comparator will fire the one-shot. The output of the one-shot is connected to both the logic output and the precision switched current source. During the one-shot period, T, the logic output will go low and the current source will turn on with current $I$. At the end of the one-shot period the logic output will go high and the current source will shut off. At this time the current source has injected an amount of charge $\mathrm{Q}=\mathrm{I}_{\mathrm{O}} \mathrm{O}^{\top}$ into the network $R_{B}-C_{B}$. If this charge has not increased the voltage $V_{B}$ such that $V_{B}>V_{1}$, the comparator again fires the one-shot and the current source injects another lump of charge, Q , into the $R_{B}-C_{B}$ network. This process continues until $V_{B}>V_{1}$. When this condition is achieved the current source remains off and the voltage $\mathrm{V}_{\mathrm{B}}$ decays until $\mathrm{V}_{\mathrm{B}}$ is again equal to $\mathrm{V}_{\mathrm{I}}$. This completes one cycle. The VFC will now run in a steady state mode. The current source dumps lumps of charge into the capacitor $C_{B}$ at a rate fast enough to keep $V_{B} \geqslant V_{1}$. Since the discharge rate of capacitor $C_{B}$ is proportional to $V_{B} / R_{B}$, the frequency at which the system runs will be proportional to the input voltage.

The 4151 VFC is easy to use and apply if you understand the operation of it through the block diagram, Figure 2. Many users, though, have expressed the desire to understand the workings of the internal circuitry. Figure 1 shows the schematic of the 4151. The circuit can be divided into five sections: the internal biasing network, input comparator, one-shot, voltage reference, and the output current source.

The internal biasing network is composed of Q39-043. The Nchannel FET Q43 supplies the initial current for zener diode Q39. The NPN transistor Q38 senses the zener voltage to derive the current reference for the multiple collector current source Q41. This special PNP transistor provides active pull-up for all of the other sections of the 4151.


Figure 2. Simplified Block Diagram, Single Supply Mode

The input comparator section is composed of Q1-Q7. Lateral PNP transistors Q1-O4 form the special ground-sensing input which is necessary for VFC operation at low input voltages. NPN transistors Q 5 and Q 6 convert the differential signal to drive the second gain stage Q7. If the voltage on input pin 7 is less than that on threshold pin 6, the comparator will be off and the collector of $Q 7$ will be in the high state. As soon as the voltage on pin 7 exceeds the voltage on pin 6 , the collector of 07 will go low and trigger the one-shot.
The one-shot is made from a voltage comparator and an R-S latch. Transistors Q12-Q15 and Q18-Q20 form the comparator, while Q8-Q11 and Q16-Q17 make up the R-S latch. One latch output, open-collector reset transistor Q16, is connected to a comparator input and to the terminal, pin 5 . Timing resistor $\mathrm{R}_{\mathrm{O}}$ is tied externally from pin 5 to $+\mathrm{V}_{\mathrm{CC}}$ and timing capacitor $\mathrm{C}_{\mathrm{O}}$ is tied from pin 5 to ground. The other comparator input is tied to a voltage divider $\mathrm{R}_{3}-\mathrm{R}_{5}$ which sets the comparator threshold voltage at 0.667 VCC. One-shot operation is initiated when the collector of Q 7 goes low and sets the latch. This causes Q16 to turn off, releasing the voltage at pin 5 to charge exponentially towards $+\mathrm{V}_{\mathrm{CC}}$ through $\mathrm{R}_{\mathrm{O}}$. As soon as this voltage reaches $0.667 \mathrm{~V}_{\mathrm{CC}}$, comparator output Q 20 will go high causing Q10 to reset the latch. When the latch is reset, Q 16 will discharge $\mathrm{C}_{\mathrm{O}}$ to ground. The one-shot has now completed its function of creating a pulse of period $T=1.1$ $\mathrm{R}_{\mathrm{O}} \mathrm{C}_{\mathrm{O}}$ at the latch output, Q21. This pulse is buffered through Q23 to drive the open-collector logic circuit transistor Q32. During the one-shot period the logic output will be in the low state. The one-shot output is also used to switch the reference voltage by Q 22 and Q 24 . The low T.C. reference voltage is derived from the combination of a 5.5 V zener diode with resistor and diode level shift networks. A stable 1.89 volts is developed at pin 2, the emitter of Q33.

Connecting the external current-setting resistor $\mathrm{R}_{\mathrm{S}}=14.0 \Omega$ from pin 2 to ground gives $135 \mu \mathrm{~A}$ from the collectors of Q 33 and Q34. This current is reflected in the precision current mirror $\mathrm{Q} 35-\mathrm{Q} 37$ and produces the output current $\mathrm{I}_{\mathrm{O}}$ at pin 1. When the R-S latch is reset, Q22 and Q24 will hold the reference voltage off, pin 2 will be at 0 V , and the current will be off. During the one-shot period T , the latch will be set, the voltage of pin 2 will go to 1.89 V , and the output current will be switched on.

## TYPICAL APPLICATIONS

## Single Supply Voltage-to-Frequency Converter

Figure 3 shows the simplest type of VFC that can be made with the 4151 . Input voltage range is from 0 to +10 V , and output frequency is from 0 to 10 kHz . Full scale frequency can be tuned by adjusting RS, the output current set resistor. This circuit has the advantage of being simple and low in cost, but it suffers from inaccuracy due to a number of error sources. Linearity error is typically $1 \%$. A frequency offset will also be introduced by the input comparator offset voltage. Also, response time for this circuit is limited by the passive integration network $R_{B} C_{B}$. For the component values shown in Figure 3, response time for a step change input from 0 to +10 V will be 135 msec . For applications which require fast response time and high accuracy, use the circuits of Figure 4 and 5.


Figure 3. Single Supply Voltage-to-Frequency Converter

## Precision VFC with Single Supply Voltage

For applications which requrie a VFC which will operate from a single positive supply with positive input voltage, the circuit of Figure 4 will give greatly improved linearity, frequency offset, and response time. Here, an active integrator using one section of the RC3403A quad ground-sensing op-amp has replaced the $R_{B}-C_{B}$ network in Figure 3. Linearity error for this circuit is due only to the 4151 current source output conductance. Frequency offset is due only to the op-amp input offset and can be nulled to zero by adjusting $\mathrm{R}_{\mathrm{B}}$. This technique uses the op-amp bias current to develop the null voltage, so an opamp with stable bias current, like the RC3403A, is required.


Figure 4. Precision Voltage-to-Frequency Converter Single Supply

## Precision Voltage-to-Frequency Converter

In this application (Figure 5) the 4151 VFC is used with an operational amplifier integrator to provide typical linearity of $0.05 \%$ over the range of 0 to -10 V . Offset is adjustable to zero. Unlike many VFC designs which lose linearity below 10 mV , this circuit retains linearity over the full range of input voltage, all the way to 0 V .
Trim the full scale adjust pot at $\mathrm{V}_{\mathrm{I}}=-10 \mathrm{~V}$ for an output frequency of 10 kHz . The offset adjust pot should be set for 10 Hz with an input voltage of -10 mV .


Figure 5. Precision Voltage-to-Frequency Converter

The 4131 operational amplifier integrator improves linearity of this circuit over that of Figure 3 by holding the output of the source, Pin 1, at a constant OV . Therefore linearity error due to the current source output conductance is eliminated. The diode connected around the op-amp prevents the voltage at 4151 pin 7 from going below 0 . Use a low-leakage diode here, since any leakage will degrade the accuracy. This circuit can be operated from a single positive supply if an RC3403A ground-sensing op-amp is used for the integrator. In this case, the diode can be left out. Note that even though the circuit itself will operate from a single supply, the input voltage is necessarily negative. For operation above 10 kHz , bypass 4151 pin 6 with $0.01 \mu \mathrm{f}$.

## Comparison of Voltage-to-Frequency Applications Circuits

Table 1 compares the VFC applications circuits for typical linearity, frequency offset, response time for a step input from 0 to 10 volts, sign of input voltage, and whether the circuit will operate from a single positive supply or split supplies.

Table 1

|  | Figure 3 | Figure 4 | Figure 5 |
| :--- | :---: | :---: | :---: |
| Linearity | $1 \%$ | $0.2 \%$ | $0.05 \%$ |
| Frequency Offset | +10 Hz | 0 | 0 |
| Response Time | 135 msec | $10 \mu \mathrm{sec}$ | $10 \mu \mathrm{sec}$ |
| Input Voltage | + | + | - |
| Single Supply | yes | yes | yes |
| Split Supply | - | - | yes |

## Frequency-to-Voltage Conversion

The 4151 can be used as a frequency-to-voltage converter. Figure 6 shows the single-supply FVC configuration. With no signal applied, the resistor bias networks tied to pins 6 and 7 hold the input comparator in the off state. A negative going pulse applied to pin 6 (or positive pulse to pin 7) will cause the comparator to fire the one-shot. For proper operation, pulse width must be less than the period of the one-shot, $\mathrm{T}=$ 1.1 $\mathrm{R}_{\mathrm{O}} \mathrm{C}_{\mathrm{O}}$. For a 5 V p-p square-wave input the differentiator network formed by the input coupling capacitor and the resistor bias network will provide pulses which correctly trigger the one-shot. An external voltage comparator such as the 311 or 339 can be used to "square-up" sinusoidal input signals before they are applied to the 4151. Also, the component values for the input signal differentiator and bias network can be altered to accommodate square waves with different amplitudes and frequencies. The passive integrator network $R_{B} C_{B}$ filters the current pulses from the pin 1 output. For less output ripple, increase the value of $C_{B}$.


Figure 6. Single Supply Frequency-to-Voltage Converter
For increased accuracy and linearity, use an operational amplifier integrator as shown in Figure 7, the precision FVC configuration. Trim the offset to give -10 mV out with 10 Hz in and trim the full scale adjust for -10 V out with 10 kHz in. Input signal conditioning for this circuit is necessary just as for the single supply mode, and scale factor can be programmed by the choice of component values. A tradeoff exists between output ripple and response time, through the choice of integration capacitor $\mathrm{C}_{\mathrm{l}}$. If $\mathrm{C}_{1}=0.1 \mu \mathrm{f}$ the ripple will be about 100 mV . Response time constant $\tau_{\mathrm{R}}=\mathrm{R}_{\mathrm{B}} \mathrm{C}_{\mathrm{I}}$. For $\mathrm{R}_{\mathrm{B}}=$ $100 \mathrm{k} \Omega$ and $\mathrm{C}_{\mathrm{I}}=0.1 \mu \mathrm{f}, \tau_{\mathrm{R}}=10 \mathrm{msec}$.


Figure 7. Precision Frequency-to-Voltage Converter

## PRECAUTIONS

1. The voltage applied to comparator input pins 6 and 7 should not be allowed to go below ground by more than 0.3 volt.
2. Pins 3 and 5 are open-collector outputs. Shorts between these pins and $+V_{C C}$ can cause overheating and eventual destruction.
3. Reference voltage terminal pin 2 is connected to the emitter of an NPN transistor and is held at approximately 1.9 volts. This terminal should be protected from accidental shorts to ground or supply voltages. Permanent damage may occur if current in pin 2 exceeds 5 mA .
4. Avoid stray coupling between 4151 pins 5 and 7, which could cause false triggering. For the circuit of Figure 3, bypass pin 7 to ground with at least $0.01 \mu \mathrm{f}$. If false triggering is experienced with the precision mode circuits, bypass pin 6 to ground with at least $0.01 \mu \mathrm{f}$. This is necessary for operation above 10 kHz .

## PROGRAMMING THE 4151

The 4151 can be programmed to operate with a full scale frequency anywhere from 1.0 Hz to 100 kHz . In the case of the VFC configuration, nearly any full scale input voltage from 1.0 V and up can be tolerated if proper scaling is employed. Here is how to determine component values for any desired full scale frequency.

1. Set $R \mathrm{~S}=14 \mathrm{k} \Omega$ or use a 12 k resistor and 5 k pot as shown in the figures. (The only exception to this is Figure 5.)
2. Set $T=1.1 \mathrm{ROC}_{\mathrm{O}}=0.75\left[\frac{1}{\mathrm{fo}}\right]$ where fo is the desired full scale frequency. For optimum performance make $6.8 \mathrm{k} \Omega$ $<\mathrm{RO}_{\mathrm{O}}<680 \mathrm{k} \Omega$ and $0.001 \mu \mathrm{f}<\mathrm{C}_{\mathrm{O}}<1.0 \mu \mathrm{f}$.
3. a) For the circuit of Figure 3 make $C_{B}=10^{-2}\left[\frac{1}{\text { fo }}\right]$ Farads. Smaller values of $\mathrm{C}_{\mathrm{B}}$ will give faster response time, but will also increase frequency offset and nonlinearity.
b) For the active integrator circuits make

$$
C_{1}=5 \times 10^{-5}\left[\frac{1}{\text { fo }}\right] \text { Farads. }
$$

The op-amp integrator must have a slew rate of at least $135 \times 10^{-6}\left[\frac{1}{C_{I}}\right]$ volts per second where the value of $C_{l}$ is again give in Farads.
4. a) For the circuits of Figure 3 and 4 keep the values of $R_{B}$ and $R_{B}{ }^{\prime}$ as shown and use an input attenuator to give the desired full scale input voltage.
b) For the precision mode circuit of Figure 5 , set $\mathrm{R}_{\mathrm{B}}=$ $\frac{V_{10}}{100 \mu \mathrm{~A}}$ where $\mathrm{V}_{10}$ is the full scale input voltage. Alternately the op-amp inverting input (summing node) can be used as a current input with full scale input current $110=-100 \mu \mathrm{~A}$.
5. For the FVCs, pick the value of $\mathrm{C}_{\mathrm{B}}$ or $\mathrm{C}_{\boldsymbol{\prime}}$ to give the optimum tradeoff between response time and output ripple for the particular application.

## DESIGN EXAMPLE

I. Design a precision VFC (from Figure 5) with fo $=$ 100 kHz and $\mathrm{V}_{10}=-10 \mathrm{~V}$.

1. Set $R_{S}=14.0 \mathrm{k} \Omega$.
2. $T=0.75\left[\frac{1}{10^{-5}}\right]=7.5 \mu \mathrm{sec}$

Let $\mathrm{R}_{\mathrm{O}}=6.8 \mathrm{k} \Omega$ and $\mathrm{C}_{\mathrm{O}}=0.001 \mu \mathrm{f}$.
3. $C_{1}=5 \times 10^{-5}\left[\frac{1}{10^{-5}}\right]=500 \mathrm{pf}$.

Op-amp slew rate must be at least
$S R=135 \times 10^{-6}\left[\frac{1}{500 \mathrm{pf}}\right]=0.27 \mu \mathrm{sec}$
4. $R_{B}=\frac{10 \mathrm{~V}}{100 \mu \mathrm{~A}}=100 \mathrm{k} \Omega$.
II. Design a precision VFC with $f 0=1 \mathrm{~Hz}$ and $\mathrm{V}_{1 \mathrm{O}}=-10 \mathrm{~V}$.

1. Let $R_{S}=14.0 \mathrm{k} \Omega$.
2. $T=0.75\left[\frac{1}{1}\right]=0.75 \mathrm{sec}$.

$$
\text { Let } \mathrm{R}_{\mathrm{O}}=680 \mathrm{k} \Omega \text { and } \mathrm{C}_{\mathrm{O}}=1.0 \mu \mathrm{f}
$$

3. $C_{1}=5 \times 10^{-5}\left[\frac{1}{1}\right] F=50 \mu \mathrm{f}$.
4. $R_{B}=100 \mathrm{k} \Omega$.
III. Design a single supply FVC to operate with a supply voltage of 9 V and full scale input frequency fo $=83.3 \mathrm{~Hz}$. The output voltage must reach at least 0.63 of its final value in 200 msec . Determine the output ripple.
5. Set $R_{S}=14.0 \mathrm{k} \Omega$.
6. $\mathrm{T}=0.75\left[\frac{1}{83.3}\right]=9 \mathrm{msec}$

$$
\text { Let } \mathrm{R}_{\mathrm{O}}=82 \mathrm{k} \Omega \text { and } \mathrm{C}_{\mathrm{O}}=0.1 \mu \mathrm{f}
$$

3. Since this FVC must operate from 8.0 V , we shall make the full scale output voltage at pin 6 equal to 5.0 V .
4. $R_{B}=\frac{5 V}{100 \mu A}=50 k \Omega$.
5. Output response time constant is $\tau_{R} \leqslant 200 \mathrm{msec}$ Therefore $\mathrm{C}_{\mathrm{B}} \leqslant \frac{\tau_{\mathrm{R}}}{\mathrm{R}_{\mathrm{B}}}=\frac{200 \times 10^{-3}}{50 \times 10^{3}}=4 \mu \mathrm{f}$.
Worst case ripple voltage is:

$$
V_{R}=\frac{9 \mathrm{mS} \times 135 \mu \mathrm{~A}}{4 \mu \mathrm{f}}=304 \mathrm{mV}
$$

IV. Design an opto-isolated VFC with high linearity which accepts a full scale input voltage of +10 V . See Figure 8 for the final design. This circuit uses the precision mode

VFC configuration for maximum linearity. The RC3403A quad op-amp provides the functions of inverter, integrator, regulator, and LED driver.


Figure 8. Opto-Isolated VFC

## DESCRIPTION

The Raytheon 4152 consists of a comparator, a one-shot, a precise gated current-source output, an internal voltage reference, and an open-collector output . . . all on a single monolithic IC chip. These elements can be combined via external pin connections to perform a wide variety of circuit functions.
The versatility of this unique IC makes it easy to tailor the circuit operation to your needs. Pulse width, scale factor, and output drive are set by external resistors as shown in Figure 1. Combine the versatile 4152 with an op amp or two, some digital circuits, and the range of cost-effective applications becomes even greater.
The Raytheon 4152 provides a versatile, low-cost means of accurately converting an analog signal to a pulse train of proportional frequency, and vice versa. It can be imaginatively applied to a broad range of signal conditioning applications once the various functional blocks within the IC are understood.

The 4152 is directly interchangeable with the 4151 , thereby allowing an upgrading of system accuracy at minimal cost.


Figure 1. Functional Diagram of Raytheon 4152.

## FEATURES

- Single supply operation ( +7 V to +18 V )
- Pulse output compatible with all logic forms (DTL/TTL/ CMOS)
- Programmable scale factor (K)
- High linearity $\pm 0.05 \%$ max
- Temperature stability $\pm 150 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max
- Direct replacement for RM/RC4151
- High noise rejection
- Inherent monotonicity
- Easily transmittable output
- Simple full scale trim
- Single-ended input, referenced to ground
- V/F or F/V conversion
- Voltage or current input
- Wide dynamic range


## APPLICATIONS

- Precision voltage-to-frequency-converters
- Pulse-width modulators
- Programmable pulse generators
- Frequency-to-voltage converters
- Integrating analog-to-digital converter
- Long-term analog integrator
- Signal conversion -

Current-to-frequency
Temperature-to-frequency
Pressure-to-frequency
Capacitance-to-frequency
Frequency-to-current

- Signal isolation

VFC $\rightarrow$ opto-isolation $\rightarrow$ FVC
ADC with opto-isolation

- Signal encoding

FSK modulation/demodulation
Pulse-width modulation

- Frequency scaling
- DC motor speed control


## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Supply Voltages | +22V | Storage Temperature Range |  |
| :---: | :---: | :---: | :---: |
| Output Sink Current | 20 mA | RM4152 | $-65{ }^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Internal Power Dissipation | 500 mW | RV4152 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Input Voltage | -0.2 V to + V CC | RC4152 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Output Short Circuit to Ground | . . Continuous | Operating Temperature Range |  |
|  |  | RM4152 | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
|  |  | RV4152 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
|  |  | RC4152 | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |



| CIRCUIT CHARACTERISTICS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: |
| Input Comparator |  |  |  |  |
| Input Offset Voltage @ $25^{\circ} \mathrm{C}$ vs. Temperature | $0.65 V_{\text {CC }}$ | $\begin{gathered} \pm 2 \\ \pm 20 \end{gathered}$ | $\pm 10$ | $\underset{\mu \mathrm{V} /{ }^{\circ} \mathrm{C}}{ }$ |
| Input Offset Current |  | $\pm 30$ | $\pm 100$ | nA |
| Bias Current (Either Input) |  | -50 | -300 | nA |
| Input Voltage Range (Either Input) |  | $0 \text { to } V_{C C}-3.0 \text { Volts }$ |  | V |
|  |  | $10,000$ |  | - |
| One-Shot Pulse Circuit |  |  |  |  |
| Pulse Width (See Fig. 1) |  | $1.1 \mathrm{R}_{0} \mathrm{C}_{0} \pm 3 \%$ |  | sec |
| Threshold Voltage (Pin 5) Input Bias Current (Pin 5) |  | $0.67 V^{\prime} C C$ -100 | $\begin{gathered} 0.69 V_{C C} \\ -500 \end{gathered}$ | V |
| $\mathrm{V}_{\text {sat }}$ at Pin 5, I $=2.2 \mathrm{~mA}$ |  | 0.10 | -500 | V |
| Pulse Width Stability ( $\mathrm{T}_{\mathrm{p}}=75 \mu \mathrm{~s}$ ) <br> vs. Temperature <br> vs. Supply |  | $\begin{gathered} \pm 30 \\ \pm 100 \end{gathered}$ | $\pm 50$ | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ ppm/V |
| Gated Current Source |  |  |  |  |
| Output of Gated Current Source vs. Temperature (1) |  |  | $\underset{\substack{\mathrm{V}_{\mathrm{R}} / \mathrm{R}_{\mathrm{S}} \pm 1 \% \\ \pm 50}}{ }$ | 100 | $\stackrel{-}{\text { apm }} /{ }^{\circ} \mathrm{C}$ |
| vs. Supply |  | 0.10 | $\pm 100$ | $\% / V$ |
| Compliance (Change with Voltage) |  | 0.10 | 0.25 | $\mu \mathrm{A} / \mathrm{V}$ |
| Leakage in OFF State |  | 10 | 50 | nA |
| Rise Time |  | 100 |  | nsec |
| Fall Time |  | 100 |  | nsec |
| Reference Voltage |  |  |  |  |
| Voltage $\mathrm{V}_{\mathrm{R}}($ Pin 2 ) |  | 2.25 | 2.5 | $\checkmark$ |
| Temperature Coefficient |  | $\pm 50$ | $\pm 100$ | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Logic Output (Pin 3) |  |  |  |  |
| $V_{\text {sat }} @ 1=3 \mathrm{~mA}$ |  | 0.1 | 0.5 | V |
| @I= 10 mA |  | 0.8 |  | V |
| Power Supply |  |  |  |  |
| Voltage, Operating Range | +7 | +15 | +18 | V |
| Quiescent Current Drain |  | 2.5 | 6 | mA |

[^7]
## Input Comparator

The input comparator section consists of transistors Q1 through Q7 (see Figure 2). A PNP ground-sensing input stage provides capability of operating down to low input voltages, thus the input range on either input is from zero up to $+\mathrm{V}_{\mathrm{CC}}-3 \mathrm{~V}$ (power supply voltage less three volts). This is particularly important for single-supply operation. Input comparator gain is approximately 10,000 . The output of the comparator, transistor 07, switches from OFF to ON when the input voltage applied to pin 7 becomes more positive than the input voltage on pin 6. The output transistor Q7 going into saturation is used to trigger the one-shot.

One important precaution: The voltage applied to the input comparator (pins 6 and 7) must not be more negative than 0.3 V relative to the ground terminal (pin 4) unless there is protective current limiting. Negative input voltages will saturate the input PNP transistors and cause excessive input base current. This input-base current must not be allowed to exceed 25 mA over an extended period of time or the IC could be damaged. If there is a possibility of continuous excessive negative voltage on the input, then a resistor in series with the input should be added to limit the input current.

## One-Shot Circuit

Pulse-width of the one-shot is determined by the external components $\mathrm{R}_{\mathrm{o}}, \mathrm{C}_{\mathrm{O}}$ that are connected to pin 5 . The capacitor $\mathrm{C}_{\mathrm{O}}$ is normally discharged through the saturated transistor Q16. When the one-shot timing cycle is initiated, capacitor $\mathrm{C}_{\mathrm{O}}$ is released by Q16 turning OFF and allowed to charge towards $+V_{C C}$ through $R_{0}$. At $2 / 3$ of $+V_{C C}$, transistor Q 16 is switched ON and the capacitor $\mathrm{C}_{\mathrm{O}}$ is discharged. The pulse width will therefore be determined by the following equation:

$$
\begin{gathered}
1-\epsilon^{-\frac{T_{p}}{R_{o} C_{o}}=0.667} \\
T_{p}=1.1 R_{o} C_{o}
\end{gathered}
$$

Pulse width $T_{p}$ is independent of supply voltage $+V_{C C}$. For best linearity and stability, $\mathrm{R}_{\mathrm{O}}$ and $\mathrm{C}_{\mathrm{O}}$ should be selected within a range of $5 \mathrm{~K} \Omega$ to $500 \mathrm{~K} \Omega$ and $0.001 \mu \mathrm{~F}$ to $1.0 \mu \mathrm{~F}$.

A latching action by the RS flip-flop comprised of Q9 and Q11 assures that the timing cycle will be completed regardless of input voltage. The flip-flop is set by Q 7 going into the ON state. Q9 is normally OFF and Q11 normally ON; so Q7 going low will cause Q11 to switch OFF and Q9 to switch ON. Since Q9 and Q7 collectors are tied together, Q 9 will keep the collectors low regardless of Q 7 state. At the end of the timing cycle, Q10 is switched ON and this will make Q9 go OFF. If Q7 is OFF, then the flip-flop can reset to the normal state where Q9 is OFF and Q11 ON. The input state overides this reset action. In FVC applications, it is very important to make the input pulses narrower than the output pulse width $T_{p}$ to assure proper resetting of the Q9-011 flip-flop.
The output pulse of the one-shot performs three functions during the timing interval:

1. The open-collector output transistor Q32 is switched into saturation. The output pulse at pin 3 is in the low state during the $T_{p}$ timing interval.
2. A reference voltage $V_{R}$ is switched $O N$ at pin 2.
3. The output current source is gated ON. A current pulse of width $T_{p}$ and amplitude $V_{R} / R_{S}$ wiil come out of pin 1.


Figure 2. Raytheon 4152 Schematic Diagram

## Gated Current Source

During the pulse timing interval $T_{p}$, a reference voltage $V_{R}$ is switched to the ON state at pin 2. External resistor $R_{S}$ at pin 2 sets up a current $V_{R} / R_{S}$ that is reflected in precision current source $\mathrm{Q} 35-\mathrm{Q} 37$. This causes a current pulse of magnitude $\mathrm{V}_{\mathrm{R}} / \mathrm{R}_{\mathrm{S}}$ from Q 35 at pin 1. The output pulse $\mathrm{I}_{\mathrm{O}}$ at pin 1 has pulse width $T_{p}$ and amplitude of $V_{R} / R_{S}$.

## Reference

The reference voltage $\mathrm{V}_{\mathrm{R}}$ is derived from a very stable, low tempco, buried-zener diode. The zener voltage is level shifted to provide a stable 2.3 V at pin 2 during the timing interval $T_{p}$. This internal reference provides excellent power-supply rejection over a wide operating range. Low-cost unregulated power supplies can often be used without degrading accuracy (see characteristic curves).

## VOLTAGE-TO-FREQUENCY CONVERSION

## Single-Supply VFC Circuit

The simplest type of VFC that can be made with the Raytheon 4152 is shown in Figure 3. The circuit will operate from a single power supply voltage that can vary from +7 V to +18 V . The input voltage $V_{I N}$ is positive and can range from zero up to within 3 V of positive supply.
The input voltage $\mathrm{V}_{\text {IN }}$ is applied to the input comparator through a low-pass filter ( $100 \mathrm{~K} \Omega, 0.01 \mu \mathrm{~F}$ ). The one-shot will fire repetitively and pump out current pulses of amplitude ${ }^{\prime} O$ into the external low-pass filter comprised of $R_{B}, C_{B}$. This sets up a feedback loop and the pulse repetition rate will rise until the average voltage at pin 6 equals the DC input voltage at pin 7. At null, the duty cycle $T_{p} / T$ must be sufficient to keep integrating capacitor $C_{B}$ charged up to $V_{I N}$. Assuming $C_{B}$ is relatively large, then in the steady-state condition:

SPECIFICATIONS AS SINGLE-SUPPLY VFC (Figure 3) Typical performance at $25^{\circ} \mathrm{C}$ when connected as shown in Fig. 3. $\mathrm{R}_{\mathrm{O}}=6.8 \mathrm{~K} \Omega, \mathrm{C}_{\mathrm{O}}=0.01 \mu \mathrm{~F}, \mathrm{~V}_{\mathrm{CC}}=+15.0 \mathrm{~V}, \mathrm{R}_{\mathrm{B}}=$ $100 \mathrm{~K} \Omega, \mathrm{C}_{\mathrm{B}}=1.0 \mu \mathrm{~F}$.

Input

| Input Voltage Range | 10 mV to +10 V |
| :--- | :--- |
| Input Overrange | $+10 \% \min$ |
| Input Impedance | $100 \mathrm{~K} \Omega$ |

Output
Frequency Range
Frequency Overrange
Scale Factor
Response Time to Step Input
Pulse Width
Rise and Fall Time
Output Voltage
HIGH State
LOW State
Accuracy

| Nonlinearity | $\pm 1 \% \mathrm{max}$ |
| :--- | :--- |
| Offset Voltage | $\pm 15 \mathrm{mV}$ max |
| Gain Accuracy |  |
| $\quad$ vs. Temperature | $\pm 300 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max |
| $\quad$ vs. Supply | $\pm 0.3 \% / \mathrm{Volt}$ |
| Offset Stability |  |
| $\quad$ vs. Temperature | $\pm 50 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| $\quad$ vs. Supply | $\pm 20 \mu \mathrm{~V} / \mathrm{V}$ of $\Delta \mathrm{V}_{\mathrm{S}}$ |

## Power Requirement

Supply Voltage

| Rated Performance | +15 V |
| :--- | :--- |
| Operating Range | +7 V to +18 V |
| iescent Current Drain | +6.0 mA max |

10 Hz to 10 kHz
$+10 \%$ min $1 \mathrm{kHz} / \mathrm{V} \pm 10 \%$ 135 msec $75 \mu \mathrm{sec} \pm 10 \%$
500 nsec
$+V_{C C}$
$3.0 \mathrm{~mA} @ \mathrm{~V}_{\text {sat }}=0.15 \mathrm{~V}$
$10 \mathrm{~mA} @ \mathrm{~V}_{\text {sat }}=0.8 \mathrm{~V}$
$\pm 1 \%$ max
$\pm 15 \mathrm{mV}$ max
$\pm 300 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max
$\pm 0.3 \% /$ Volt
$\pm 50 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$
$\pm 20 \mu \mathrm{~V} / \mathrm{V}$ of $\Delta \mathrm{V}_{\mathrm{S}}$

Operating Range
+7 V to +18 V
+6.0 mA max


Figure 3. Single-Supply Voltage-to-Frequency Converter

$$
\frac{V_{I N}}{R_{B}}=I_{O} \frac{T_{p}}{T}
$$

Since $I_{O}$ is $V_{R} / R_{S}$ and $T_{p}$ is $1.1 R_{0} C_{0}$, then the output frequency $F_{O}$ will be:

$$
F_{O}=\frac{1}{T}=\frac{R_{S}}{1.1 R_{o} C_{o} R_{B}} \frac{V_{I N}}{V_{R}}
$$

The external passive components set the scale factor. For best linearity, $R_{S}$ should be limited to a range of $15 \mathrm{~K} \Omega$ to $20 \mathrm{~K} \Omega$. Reference voltage $\mathrm{V}_{\mathrm{R}}$ is nominally 2.3 V . Recommended values for various operating ranges are given in the table below:

| $\quad$Operating <br> Range | $\mathbf{R}_{\mathbf{o}}$ | $\mathbf{C}_{\mathbf{o}}$ | $\mathbf{R}_{\mathbf{B}}$ | $\mathbf{C}_{\mathbf{B}}$ |
| :--- | :---: | :--- | :---: | :---: |
|  |  |  |  |  |
| DC to 1 kHz | $6.8 \mathrm{~K} \Omega$ | $0.1 \mu \mathrm{~F}$ | $100 \mathrm{~K} \Omega$ | $10 \mu \mathrm{~F}$ |
| DC to 10 kHz | $6.8 \mathrm{~K} \Omega$ | $0.01 \mu \mathrm{~F}$ | $100 \mathrm{~K} \Omega$ | $1.0 \mu \mathrm{~F}$ |
| DC to 100 kHz | $6.8 \mathrm{~K} \Omega$ | $0.001 \mu \mathrm{~F}$ | $100 \mathrm{~K} \Omega$ | $0.1 \mu \mathrm{~F}$ |

This simple, single-supply VFC circuit is recommended for applications where the input dynamic range is limited and does not go to zero, and response time is not critical. When scaled for 10 kHz full-scale output, the nonlinearity will be less than $1 \%$ over an input range of 10 mV to 10 V . Response time to a step input will be approximately 135 msec .
Linearity, offset, and response time are all improved by adding an external op amp as shown in Figure 4. The active integrator is used to make a precision VFC circuit.

SPECIFICATIONS AS PRECISION, DUAL-SUPPLY VFC (Figure 4) - Typical performance when connected as shown in Fig. 4. $\mathrm{R}_{\mathrm{O}}=6.8 \mathrm{~K} \Omega, \mathrm{C}_{\mathrm{O}}=0.01 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{I}}=0.005 \mu \mathrm{~F}, \mathrm{~V}_{\mathrm{CC}}=$ $\pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{B}}=100 \mathrm{~K} \Omega$.

Input

| Input Voltage Range | 0 to -10 V |
| :--- | :--- |
| Input Overrange | $+10 \% \mathrm{~min}$ |
| Input Impedance | $100 \mathrm{~K} \Omega$ |

Output

| Frequency Range | 0 to 10 kHz |
| :--- | :--- |
| Frequency Overrange | $+10 \% \mathrm{~min}$ |
| Scale Factor | $1 \mathrm{kHz/V} \pm 10 \%$ |
| Response Time to Step Input ${ }^{(1)}$ | $10 \mu \mathrm{sec}$ |
| Pulse Width | $75 \mu \mathrm{sec} \pm 10 \%$ |
| Rise and Fall Time | 500 nsec |
| Output Voltage |  |
| $\quad$ HIGH State | +V CC |
| $\quad$ LOW State | +0.5 V max at 3 mA |

## Accuracy

| Nonlinearity | $\pm 0.05 \% \max$ |
| :--- | :--- |
| Offset Voltage | $\pm 1 \mathrm{mV}$, Adj to Zero |
| Gain Accuracy |  |
| $\quad$ vs. Temperature | $\pm 150 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max |
| $\quad$ vs. Supply | $\pm 0.02 \% / \mathrm{V}$ |
| Offset Stability |  |
| $\quad$ vs. Temperature | $\pm 20 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| vs. Supply | $\pm 20 \mu \mathrm{~V} / \mathrm{V}$ |

Power Requirement
Supply Voltage $\pm 15 \mathrm{~V}$
Quiescent Current Drain (4152 only) +6 mA
${ }^{(1)}$ Two pulses of new frequency plus $10 \mu \mathrm{sec}$.


Figure 4. Precision Voltage-to-Frequency Converter

## Precision VFC Circuit, Dual-Supply

In the precision VFC circuit of Figure 4, a negative input voltage is summed with positive output current pulses $V_{R} / R_{S}$ into an integrator circuit. The integrator output is applied to the 4152 input comparator. This forms a charge-balancing loop and the pulse-repetition frequency will be such that the average value of output current pulses will equal the average value of input current. In the steady-state condition,

$$
\frac{V_{I N}}{R_{B}}=\frac{V_{R}}{R_{S}} \frac{T_{p}}{T}
$$

As before, pulse width $T_{p}$ is $1.1 R_{o} C_{0}$. The reference voltage $\mathrm{V}_{\mathrm{R}}$ is nominally 2.3 V , therefore:

$$
F_{O}=0.395 \frac{R_{S}}{R_{B} R_{o} C_{o}} V_{I N}
$$

For best linearity, $\mathrm{R}_{\mathrm{S}}$ should be limited to a range of $15 \mathrm{~K} \Omega$ to $20 \mathrm{~K} \Omega$. The current pulses will have a magnitude of approximately $134 \mu \mathrm{~A}$ with $\mathrm{V}_{\mathrm{R}}$ of 2.3 V and $\mathrm{R}_{\mathrm{S}}$ of $17.2 \mathrm{~K} \Omega$. A choice of $100 \mathrm{~K} \Omega$ for $R_{B}$ provides a high input impedance to $V_{\text {IN }}$. If we choose $R_{0}$ of $6.8 \mathrm{~K} \Omega$, then the table below indicates the VFC scaling for various capacitor values using the circuit of Fig. 4 and $\mathrm{R}_{\mathrm{S}}$ of $17.2 \mathrm{~K} \Omega$ :

|  |  | Scale | Range |  |
| :--- | :---: | :---: | :---: | :---: |
| $\mathbf{C}_{\mathbf{o}}$ | $\mathbf{C}_{\mathbf{I}}$ | Factor | Input $\mathrm{V}_{\text {IN }}$ | Output $\mathrm{F}_{\mathbf{O}}$ |
| $0.1 \mu \mathrm{~F}$ | $0.05 \mu \mathrm{~F}$ | $0.1 \mathrm{kHz} / \mathrm{V}$ | 0 to -10 V | 0 to 1 kHz |
| $0.01 \mu \mathrm{~F}$ | $0.005 \mu \mathrm{~F}$ | $1 \mathrm{kHz} / \mathrm{V}$ | 0 to -10 V | 0 to 10 kHz |
| 1000 pF | 500 pF | $10 \mathrm{kHz} / \mathrm{V}$ | 0 to -10 V | 0 to 100 kHz |

Scale factor can be easily trimmed by varying $R_{S}$. The offset adjustment shown in Fig. 4 compensates for offset in the op amp. Best linearity is obtained with op amps having greater than $1 \mathrm{~V} / \mu \mathrm{sec}$ slew rate, but any op amp can be used.

## FREQUENCY-TO-VOLTAGE CONVERSION

## Single-Supply FVC Circuit

A basic, single-supply frequency-to-voltage converter can be designed as shown in Figure 5 if the input frequency is in the form of a pulse or square wave. If the input is in the form of a sine wave, then a comparator should be used ahead of this circuit. The incoming pulses shaped by $\mathrm{C}_{\text {IN }}$ trigger the 4152 input comparator and fire the one-shot. For proper operation, the input pulse width must be less than the one-shot period $T_{p}$, which is $1.1 R_{o} C_{o}$. A differentiator and biasing network on the input ( $C_{1}, 5.1 \mathrm{~K} \Omega$, and $10 \mathrm{~K} \Omega$ ) is used to shape the trigger input. Pin 7 is biased at $1 / 2 \vee_{\mathrm{CC}}$ and $\operatorname{Pin} 6$ is biased at $2 / 3 \mathrm{~V}_{\mathrm{CC}}$, therefore the input comparator is in the OFF state between input pulses. A negative-going pulse applied to Pin 6, or a positive-going pulse to Pin 7, will cause the input comparator to fire the one-shot. The input pulse amplitude must be large enough to trip the comparator, but not so
large as to exceed the input voltage ratings. For the component values shown in Fig. 5, the input pulse amplitude should be 5 V peak-to-peak when operating from $\pm 15 \mathrm{~V}$ supplies.
Output current pulses of precise amplitude and width are low-pass filtered by $R_{B}, C_{B}$ to provide a $D C$ output voltage. Output ripple voltage can be minimized by increasing $C_{B}$, but at the expense of increased response time. The DC output voltage will be directly proportional to the input frequency $\mathrm{F}_{\text {IN }}$. The average value of the output is given by:

$$
\begin{gathered}
V_{0}=\frac{F_{I N} H z}{0.395 \frac{R_{S}}{R_{B} R_{0} C_{0}} \frac{H z}{\text { Volt }}} \\
V_{0}=2.53 \frac{R_{B} R_{0} C_{0}}{R_{S}} F_{I N} \text { Volts }
\end{gathered}
$$

Recommended values for various operating ranges are given below:

| Input <br> Operating <br> Range | $\mathbf{C}_{\mathbf{I N}}$ | $\mathbf{R}_{\mathbf{o}}$ | $\mathbf{C}_{\mathbf{o}}$ | $\mathbf{R}_{\mathbf{B}}$ | $\mathbf{C}_{\mathbf{B}}$ | Ripple |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 to 1 kHz | $0.02 \mu \mathrm{~F}$ | $6.8 \mathrm{~K} \Omega$ | $0.1 \mu \mathrm{~F}$ | $100 \mathrm{~K} \Omega$ | $100 \mu \mathrm{~F}$ | 1 mV |
| 0 to 10 kHz | $0.002 \mu \mathrm{~F}$ | $6.8 \mathrm{~K} \Omega$ | $0.01 \mu \mathrm{~F}$ | $100 \mathrm{~K} \Omega$ | $10 \mu \mathrm{~F}$ | 1 mV |
| 0 to 100 kHz | 200 pF | $6.8 \mathrm{~K} \Omega$ | $0.001 \mu \mathrm{~F}$ | $100 \mathrm{~K} \Omega$ | $1 \mu \mathrm{~F}$ | 1 mV |

To estimate worst-case ripple voltage, assume that the current pulse ${ }^{\mathrm{O}}$ of width $\mathrm{T}_{\mathrm{p}}$ causes a step change in output voltage across $C_{B}$. From $i=C d V / d t$,

$$
\Delta v_{o}=\frac{I_{0} T_{p}}{C_{B}} \text {, where } T_{p}=1.1 R_{o} C_{o}
$$



Figure 5. Single Supply Frequency-to-Voltage Converter

For example; if the output pulse width $T_{p}$ were 9 msec , the pulse amplitude were $2.3 \mathrm{~V} / 17 \mathrm{~K} \Omega=135 \mu \mathrm{~A}$, and $\mathrm{C}_{\mathrm{B}}$ were chosen to be $10 \mu \mathrm{~F}$, then the output ripple would be approximately 121 mV peak-to-peak.

## Precision Frequency-to-Voltage Circuits

Linearity and offset can be improved by adding one or more op amps to form an active low-pass filter at the output. A circuit using a single op amp filter is shown in Figure 6. The output current pulses of amplitude $\mathrm{V}_{\mathrm{R}} / \mathrm{R}_{\mathrm{S}}$ are injected into the summing junction of an op amp integrator.
The positive output pulses are averaged by the low-pass filter and the output voltage will be negative. In the steady-state condition,

$$
\begin{aligned}
& v_{{ }_{\text {Avg }}}=\frac{F_{I N} H z^{0.395} \frac{R_{S}}{R_{B} R_{o} C_{o}} \frac{H z}{\text { Volt }}}{} \\
& v_{{ }_{\text {Avg }}}=-2.53 \frac{R_{B} R_{o} C_{o}}{R_{S}} F_{I N} \text { Volts }
\end{aligned}
$$

The worst-case ripple can be estimated as in the single-supply case. As before, there is a design trade-off between ripple voltage and response time.
A two-pole low-pass filter is recommended for applications requiring wide dynamic range and fast response time. The double pole filter shown in Figure 7 is an excellent choice for FVC operation. The filter response can be calculated from the following equations:

$$
\mathrm{I}_{\mathrm{O}}+\frac{\mathrm{V}_{0}}{R_{1}}=-\mathrm{C}_{1} \frac{\mathrm{~d} V_{1}}{d t}
$$



Figure 6. Frequency-to-Voltage Converter with Single-Pole Low-Pass Filter
and

$$
\frac{V_{1}-V_{0}}{R_{2}}=c_{2} \frac{d V_{0}}{d t}
$$

These combine into the single differential equation:

$$
I_{O}=-C_{1} R_{2} C_{2} \frac{d^{2} V_{0}}{d t^{2}}-C_{1} \frac{d V_{0}}{d t}-\frac{V_{0}}{R_{1}}
$$

On the input side; $I_{O}$ is a pulse train of frequency $F_{I N}$, pulsewidth $T_{p}$, and amplitude $\mathrm{V}_{\mathrm{R}} / \mathrm{R}_{\mathrm{S}}$. As before, the input amplitude should be 5 V peak-to-peak for the component values shown. When FIN is constant, the output voltage will be:

$$
\begin{gathered}
\frac{V_{o}{ }_{\text {Avg }}}{R_{1}}=\frac{V_{R}}{R_{S}} \frac{T_{p}}{T} \\
V_{o_{\text {Avg }}}=-1.1 \frac{R_{1}}{R_{S}} R_{o} C_{o} V_{R} F_{I N}
\end{gathered}
$$

Response to a step-change in input frequency is determined by the ratio of the two time constants, $\mathrm{R}_{1} \mathrm{C}_{1}$ and $\mathrm{R}_{2} \mathrm{C}_{2}$. Step response to input frequency change will be critically damped for $R_{1} C_{1}=4 R_{2} C_{2}$. A more optimum relationship is $R_{1} C_{1}$ equal to $\mathrm{R}_{2} \mathrm{C}_{2}$ which provides a damping factor of 0.5 . The capacitors $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$, as well as $\mathrm{R}_{0} \mathrm{C}_{0}$, should be chosen for minimum ripple over the desired range of operation. Scaled for 1 V per kHz and $\mathrm{T}_{\mathrm{p}}$ of 6.8 msec , this filter has less than 0.1 V peak-to-peak ripple over the range of 10 Hz to 10 kHz $\left(R_{1}=100 \mathrm{~K}\right.$ and $\left.C_{1}=0.1 \mu \mathrm{~F}\right)$. The ripple is less than 0.02 V peak-to-peak above 100 Hz .


Figure 7. Frequency-to-Voltage Converter with Two-Pole Low-Pass Filter

## TYPICAL ELECTRICAL DATA



## PRODUCT DESCRIPTION

The Raytheon RC4200 is the industry's first integrated circuit multiplier to have complete compensation for nonlinearity, the primary source of error and distortion. This is also the first IC multiplier to have three on-board operational amplifiers designed specifically for use in multiplier logging circuits. These specially-designed amplifiers are frequency compensated for optimum AC response in a logging circuit; the heart of a multiplier, and can therefore provide superior AC response in comparison to other analog multipliers.

Versatility is unprecedented; this is the first IC multiplier that can be used in a wide variety of applications without sacrificing accuracy. Four-quadrant multiplication, onequadrant division or square-rooting, and RMS-to-DC conversion can all be easily implemented with predictable accuracy. The nonlinearity compensation is not just trimmed at a single temperature, it is designed to provide compensation over the full temperature range. This nonlinearity compensation combined with the low gain and offset drift inherent in a well-designed monolithic chip provides a very low tempco on accuracy.

The excellent linearity and versatility were achieved through circuit design rather than special grading or tweaking, therefore unit cost is very low. Analog multipliers can now be used in applications where price was previously an inhibiting factor.

The Raytheon RC4200 is ideal for use in low-distortion audio modulation circuits, voltage-controlled active tilters. and precision oscillators.


Figure 1. 4200 Multiplier Functional Diagram

## FEATURES

- High accuracy

Non-linearity - $0.1 \%$ maximum
Temperature coefficient $=0.005 \% /{ }^{\circ} \mathrm{C}$ maximum

- Multiple functions

Multiply, divide, square, square root, RMS-to-DC conversion, AGC, and modulate/demodulate

- Wide bandwidth -4 MHz


## THERMAL SYMMETRY

The scale factor is sensitive to temperature gradients across the chip in the lateral direction. Where possible, the package should be oriented such that sources generating temperature gradients are located physically on the line of thermal symmetry. This will minimize scale-factor error due to thermal gradients.

## CONNECTION INFORMATION



## FUNCTIONAL DESCRIPTION

The RC4200 multiplier is designed to multiply two input currents ( $I_{1}$ and $I_{2}$ ) and to divide by a third input current ( $1_{4}$ ). The output is also in the form of a current $\left(I_{3}\right)$. A simplified circuit diagram is shown in Figure 1. The nominal relationship between the three inputs and the output is:

$$
\begin{equation*}
I_{3}=\frac{i_{1} i_{2}}{i_{4}} \tag{1}
\end{equation*}
$$

All four currents must be positive and restricted to a range of $1 \mu \mathrm{~A}$ to 1 mA . The three input currents go into the multiplier chip at op-amp summing junctions which are nominally at zero volts. Therefore, an input voltage can be easily

ABSOLUTE MAXIMUM RATINGS (above which the useful life may be impaired)


ELECTRICAL CHARACTERISTICS (Over operating temperature range, $\mathrm{V}_{\mathbf{S}}=-15 \mathrm{~V}$ unless otherwise noted)

| PARAMETER | CONDITIONS | RC4200A |  |  | RC4200 |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN. | TYP | MAX | MIN | TYP | MAX |  |
| Input range $\left(I_{1}, I_{2}\right.$ and $\left.I_{4}\right)$ |  | 1.0 | - | 1000 | 1.0 |  | 1000 | $\mu \mathrm{A}$ |
| Total error as multiplier <br> Untrimmed | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | $\cdots$ | $\pm 2.0$ |  |  | $\pm 3.0$ | \% |
| With external trim |  |  |  | $\pm 0.2$ |  |  | $\pm 0.5$ | \% |
| Vs temperature |  |  | $\pm 0.005$ |  |  | $\pm 0.005$ |  | $\% /{ }^{\circ} \mathrm{C}$ |
| Vs supply (-9 to -18V) |  |  | $\pm 0.1$ |  |  | $\pm 0.1$ |  | \%/V |
| Nonlinearity | $50 \mu \mathrm{~A}<1<250 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  |  | $\pm 0.1$ |  |  | $\pm 0.3$ | \% |
| Input offset voltage | $I_{1}=I_{2}=I_{4}=150 \mu \mathrm{~A}, \mathrm{~T}_{A}=25^{\circ} \mathrm{C}$ |  |  | $\pm 5$ |  |  | $\pm 10$ | mV |
| Input bias current | $\mathrm{I}_{1}=I_{2}=\mathrm{I}_{4}=150 \mathrm{AA}, T_{A}=25^{\circ} \mathrm{C}$ |  |  | 300 |  |  | 500 | nA |
| Average temperature coefficient of input offset voltage | $I_{1}=I_{2}=I_{4}=150 \mu \mathrm{~A}$ |  |  | $\pm 50$ |  |  | $\pm 100$ | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Output current range ( $\mathrm{I}_{3}$ ) | (Notel) 1 ) | 1.0 |  | 1000 | 1.0 |  | 1000 | $\mu \mathrm{A}$ |
| Frequency response, -3 dB | \% |  | 4 MHz |  |  | 4 MHz |  | MHz |
| Supply voltage range | \# $\%$ | -9 | -15 | -18 | -9 | -15 | -18 | V |
| Quiescent current | $I_{1}=I_{2}=I_{4}=150 \mu \mathrm{~A}, \mathrm{~T}_{A}=25^{\circ} \mathrm{C}$ |  |  | 4 |  |  | 4 | mA |

Note 1: These specifications apply with output $\left(I_{3}\right)$ connected to an op amp summing junction. If desired, the output ( $1_{3}$ ) at pin (4) can be used to drive a resistive load directly. The resistive load should be less than 700 ohms and must be pulled up to a positive supply such that the voltage on pin (3) stays within a range of 0 to +5 V .
converted to an input current by a series resistor. Any number of currents may be summed at the inputs. Depending on the application, the output current can be converted to a voltage by an external op amp or used directly. This capability of combining input currents and voltages in various combinations provides great versatility in application.

Inside the multiplier chip, the three op amps make the collector currents of transistors Q1, Q2, and Q4 equal to their respective input currents $\left(I_{1}, I_{2}\right.$, and $\left.I_{4}\right)$. These op amps are designed with current-source outputs and are phase-compensated for optimum frequency response as a multiplier. Power drain of the op amps was minimized to prevent the introduction of undesired thermal gradients on the chip. The three op amps operate on a single-supply voltage (nominally -15 V ) and total quiescent current drain is less than 4 mA . These special op amps provide significantly improved performance in comparison to 741-type op amps.

The actual multiplication is done within the log-antilog configuration of the Q1-Q4 transistor array. These four transistors, with associated proprietary circuitry, were specially designed to precisely implement the relationship

$$
\begin{equation*}
V_{B E N}=\frac{k T}{q} \ln \frac{I^{\prime} C N}{I_{S N}} \tag{2}
\end{equation*}
$$

Previous multiplier designs have suffered from an additional undesired linear term in the above equation; the collector current times the emitter resistance. This IC re term can cause significant linearity error. In four-quadrant multiplier circuits, this added IC re term introduces a parabolic nonlinearity even with matched transistors. Raytheon has developed a unique and proprietary means of inherently compensating for this undesired IC re term. Furthermore, this Raytheon-developed circuit technique compensates linearity error over temperature changes. The nonlinearity-versus-temperature is significantly improved over earlier designs.

From equation (2) and by assuming equal transistor junction temperatures, summing base-to-emitter voltage drops around the transistor array yields:
$\frac{k T}{q}\left[\ln \frac{I_{1}}{I_{S 1}}+\ln \frac{I_{2}}{I_{S 2}}-\ln \frac{I_{3}}{I_{S 3}}-\ln \frac{I_{4}}{I_{S 4}}\right]=0$

This equation reduces to:

$$
\begin{equation*}
\frac{I_{1} I_{2}}{I_{3} I_{4}}=\frac{I_{S 1}{ }^{\prime} S 2}{I_{S 3} I_{S 4}} \tag{4}
\end{equation*}
$$

The ratio of reverse saturation currents, IS1 IS2 / IS3 IS4, depends on the transistor matching. In a monolithic multi-
plier this matching is easily achieved and the ratio is very close to unity, typically $1.0 \pm 1 \%$. The final result is the desired relationship:

$$
\begin{equation*}
I_{3}=\frac{I_{1} I_{2}}{I_{4}} \tag{5}
\end{equation*}
$$

The inherent linearity and gain stability combined with low cost and versatility makes this new circuit ideal for a wide range of nonlinear functions.

## APPLICATIONS

FOUR-QUADRANT, GENERAL-PURPOSE MULTIPLIER


Figure 2. Four-Quadrant General Purpose Multiplier Using the RC4200
The general schematic for a four-quadrant multiplier using the RC4200 IC is shown in Figure 2. A positive reference voltage, $\mathrm{V}_{\mathrm{R}}$, is used to offset the multiplier chip. To stay within the most linear operating range, it is necessary that $V_{R} / R_{2}$ plus $V_{X} / R_{1}$ be limited to a range of $50 \mu \mathrm{~A}$ to $250 \mu \mathrm{~A}$. Within the operating range, input and output currents are given by the following equations:

$$
\begin{array}{ll}
I_{1}=\frac{V_{X}}{R_{1}}+\frac{V_{R}}{R_{2}} & I_{3}=\frac{V_{X}}{R_{1}}+\frac{V_{Y}}{R_{1}}+\frac{V_{R}}{R_{2}}+\frac{V_{0}}{R_{0}} \\
I_{2}=\frac{V_{Y}}{R_{1}}+\frac{V_{R}}{R_{2}} & I_{4}=\frac{V_{R}}{R_{2}}
\end{array}
$$

Combining these relationships through the equation $1_{3}=$ I 1 I2/l4 yields:

$$
V_{0}=\frac{R_{0} R_{2}}{R_{1}^{2}} \frac{V_{X} V_{Y}}{V_{R}}
$$

The reference voltage $V_{R}$ must be positive, but $V_{X}$ and $V_{Y}$ can be $A C$ voltages. The positive supply voltage can be used as the reference in many applications where a well-regulated +15 V is available. Some typical values for a multiplier scaled at $V_{X} \vee_{Y} / 10$ are calculated below:

Given: $\quad V_{X}$ and $V_{Y}$ have range of $-10 V$ to +10 V .
Desired scaling is $V_{0}=V_{X} V_{Y} / 10$
Reference voltage $\mathrm{V}_{\mathrm{R}}$ is +15 V

## Calculation:

(1) Choose $\mathrm{R}_{1}=100 \mathrm{~K} \Omega$

From requirement of $+50 \mu \mathrm{~A}$ minimum

$$
\frac{-10 \mathrm{~V}}{100 \mathrm{~K}}+\frac{15 \mathrm{~V}}{\mathrm{R}_{2}}=50 \mu \mathrm{~A}
$$

Thus, $\mathrm{R}_{2}$ would also need to be $100 \mathrm{~K} \Omega$
(2) Calculate $R_{0}$ from $\frac{R_{0} R_{2}}{R_{1}{ }^{2}} \frac{1}{V_{R}}=\frac{1}{10}$,

$$
\begin{aligned}
& R_{0}=\frac{R_{1}^{2}}{R_{2}} \frac{V_{R}}{10} \\
& R_{0}=(100 K \Omega) \frac{15}{10} \\
& R_{0}=150 \mathrm{~K} \Omega
\end{aligned}
$$

Results:

$$
\begin{gathered}
V_{0}=\frac{V_{X} V_{Y}}{10} \text { with } V_{R}=+15 \mathrm{~V} \\
R_{1}, R_{2}=100 \mathrm{~K} \Omega \\
R_{0}=150 \mathrm{~K} \Omega
\end{gathered}
$$

These values cause a range on $I_{1}$ and $I_{2}$ of $50 \mu \mathrm{~A}$ to $250 \mu \mathrm{~A}$ for $V_{X}$ and $V_{Y}$ of -10 V to +10 V .

While the choice of values for $R_{1}, R_{2}$ and $R_{0}$ are arbitrary, best results are obtained by operating $I_{1}$ and $I_{2}$ over a range of approximately $50 \mu \mathrm{~A}$ to $250 \mu \mathrm{~A}$.

Accuracy of the four-quadrant multiplier is dependent upon both the RC4200 chip and the external components. AC feedthrough, which is the undesired output when multiplying one $A C$ input by zero on the other input, is dependent on op amp offsets and on the matching of the $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ resistor sets. Gain accuracy depends on the external reference voltage $V_{R}$, the resistor ratio $R_{0} R_{2} / R_{1}{ }^{2}$, and the multiplier chip. Linearity depends almost entirely upon the multiplier IC. The linear error terms can all be nulled externally by trimming resistor ratios or offsets. A four-quadrant multiplier with provision for external trimming of linear error components is shown in Figure 3. The optimum mix of component tolerances, trimming range, and cost is very application dependent. With moderate-cost components and no external trimming, the RC4200 is more accurate than many of the complete IC multipliers. With precision components and external trimming as shown in Figure 3, the RC4200 is capable of performance comparable to the best hybrid or modular multipliers.

The error analysis is most easily done by separately considering resistor match, offsets, and gain; then superimposing the results.

## Resistor Matching

Assuming no op amp offsets and no error due to the multiplier chip, then the output would be the sum of the terms given below:

$$
\begin{aligned}
\text { Desired Output } & =\frac{R_{0} R_{2 d}}{R_{1 a} R_{1 c}} \frac{V_{X} V_{Y}}{V_{R}} \\
V_{Y} \text { Feedthrough } & =\frac{R_{0}}{R_{1 a}}\left(\frac{R_{2 d}}{R_{2 a}}-\frac{R_{1 c}}{R_{1 d}}\right) V_{Y} \\
V_{X} \text { Feedthrough } & =\frac{R_{0}}{R_{1 a}}\left(\frac{R_{2 d}}{R_{2 b}}-\frac{R_{1 a}}{R_{1 b}}\right) V_{X} \\
\text { Output Offset } & =\frac{R_{0}}{R_{2 a}}\left(\frac{R_{2 d}}{R_{2 b}}-\frac{R_{2 a}}{R_{2 c}}\right) V_{R}^{2}
\end{aligned}
$$

The AC feedthrough is directly proportional to the matching of the $R_{2}$ resistor set and the $R_{1}$ resistor set. AC feedthrough on the X or Y input is related to resistor tolerance as:

$$
A C \text { Feedthrough } \sim \frac{R_{0}}{R_{1}} \times 2 \times \text { Res. Tol. } \times V_{I N}
$$



Figure 3. Four-Quadrant, General-Purpose Multiplier with Offset Adjustments

For example, if $R_{0} / R_{1}$ were 1.5 as in the example given previously and the resistors were matched to within $1 \%$, then the maximum $A C$ feedthrough due to resistor mismatch would be $3 \%$ of the $V_{X}$ or $V_{Y}$ input voltage. This AC feedthrough can be nulled directly by trimming the resistor sets or indirectly by trimming offsets.

## Effect of Op Amp Offsets

In a multiplier, the offsets are cross multiplied and can thus cause AC feedthrough. When one input is zero and the other is a large AC signal, then the output will be the offset of the "zero" input times the AC signal. To quantify this effect, consider the circuit as shown in Figure 3. The offsets of each amplifier are due to both input offset voitage for the op amp and the input offset current times the source resistance.

These offsets can be lumped together into a single $\mathrm{V}_{\mathrm{OS}}$ term. For this analysis, assume that the external resistors are perfectly matched ( $\mathrm{R}_{1}$ 's and $\mathrm{R}_{2}$ 's all matched). The set of equations below must be combined to see their interaction:

$$
\begin{aligned}
& I_{1}=\frac{V_{X}-V_{0 S 1}}{R_{1}}+\frac{V_{R}-V_{0 S 1}}{R_{2}} \\
& I_{2}=\frac{V_{Y}-V_{O S 2}}{R_{1}}+\frac{V_{R}-V_{0 S 2}}{R_{2}} \\
& I_{3}=\frac{V_{X}-V_{O S 3}}{R_{1}}+\frac{V_{Y}-V_{0 S 3}}{R_{1}}+\frac{V_{R}-V_{0 S 3}}{R_{2}}+\frac{V_{0}-V_{0 S 3}}{R_{0}} \\
& I_{4}=\frac{V_{R}-V_{0 S 4}}{R_{2}}
\end{aligned}
$$

For simplicity, $\mathrm{V}_{\mathrm{OS}}{ }^{2}$ terms and gain-error factors on error terms can be dropped. The output voltage would then be the sum of the terms given below:

$$
\begin{aligned}
& \text { Desired Output }=\frac{R_{0} R_{2}}{R_{1}^{2}} \frac{V_{X} V_{Y}}{V_{R}} \\
& V_{Y} \text { Feedthrough }=\frac{R_{0}}{R_{1}} \frac{1}{V_{R}}\left[V_{O S 4}-\left(\frac{R_{2}}{R_{1}}+1\right) V_{O S 1}\right] V_{Y} \\
& V_{X} \text { Feedthrough }=\frac{R_{0}}{R_{1}} \frac{1}{V_{R}}\left[V_{O S 4}-\left(\frac{R_{2}}{R_{1}}+1\right) V_{O S 2}\right] V_{X}
\end{aligned}
$$

Output Offset =

$$
\left(\frac{2 R_{0}}{R_{1}}+\frac{R_{0}}{R_{2}}+1\right) v_{0 S 3}-\left(\frac{R_{0}}{R_{1}}+\frac{R_{0}}{R_{2}}\right)\left(v_{0 S 1}+v_{0 S 2}\right)
$$

To estimate magnitudes, consider the previous example where $R_{0}=150 \mathrm{k} \Omega, R_{1}$ and $R_{2}$ were $100 \mathrm{k} \Omega$, and $V_{R}=15 \mathrm{~V}$. Then,

$$
\begin{aligned}
V_{Y} \text { Feedthrough } & =\frac{1}{10}\left(V_{O S 4}-2 V_{O S 1}\right) V_{Y} \\
V_{X} \text { Feedthrough } & =\frac{1}{10}\left(V_{O S 4}-2 V_{O S 2}\right) V_{X} \\
\text { Output Offset } & =5.5 V_{0 S 3}-3\left(V_{O S 1}+V_{O S 2}\right)
\end{aligned}
$$

To carry this example further, let each $\mathrm{V}_{\mathrm{OS}}$ term have a maximum value of $\pm 10 \mathrm{mV}$. The worst-case combination would then be a feedthrough of 0.003 V Y and 0.003 V X . Output offset could be as high as 115 mV , but would generally be less.

The trimming procedure is straight-forward when done in the following recommended sequence:

1. Apply a full-scale $A C$ voltage to $V_{Y}$ and make $V_{X}$ zero. Trim $\mathrm{V}_{\mathrm{OS} 1}$ for output null $\left(\mathrm{V}_{\mathrm{O}}=0\right)$.
2. Apply the same full scale $A C$ voltage to $V_{X}$ and make $V_{Y}$ zero. Trim $V_{O S}$ for output null $V_{O}=0$ ).
3. Apply zero to both inputs $\left(V_{X}=0\right.$ and $\left.V_{Y}=0\right)$. Trim $\mathrm{V}_{\mathrm{OS} 3}$ for output null $\left(\mathrm{V}_{\mathrm{O}}=0\right)$.
4. Adjust scale factor with $R_{0}$. Always adjust the input offsets before setting the scale factor.

In most applications, the offset adjustments are used to compensate for the $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ resistor network mismatch as well as the op amp offsets. Thus, the range of offset adjustment is usually chosen to encompass both error terms. For example, the $V_{Y}$ feedthrough is:

$$
\left\{\frac{R_{0}}{R_{1}}\left(\frac{R_{2 d}}{R_{2 b}}-\frac{R_{1 a}}{R_{1 b}}\right)+\frac{R_{0}}{R_{1}} \frac{1}{V_{R}}\left[v_{0 S 4}-\left(\frac{R_{2}}{R_{1}}+1\right) v_{0 S 1}\right]\right\} v_{Y}
$$

Varying $\mathrm{V}_{\text {OS1 }}$ over sufficient range can compensate for both offset and resistor mismatch.

## ONE-QUADRANT DIVIDER

Division is very easily implemented with the RC4200 multiplier when the inputs are all positive. The circuit for one-quadrant division is shown in Figure 4. The inputs $V_{\mathrm{X}}, \mathrm{V}_{\mathrm{Z}}$, and $\mathrm{V}_{\mathrm{R}}$ must be positive and the input currents $I_{1}, I_{2}$ and $I_{4}$ must be restricted in range. Within the rated range, $I_{1} I_{2}$ will equal $I_{3} I_{4}$ and therefore:

$$
\begin{aligned}
& \left(\frac{v_{X}}{R_{1}}\right)\left(\frac{v_{R}}{R_{2}}\right)=\left(\frac{v_{0}}{R_{0}}\right)\left(\frac{v_{Z}}{R_{4}}\right) \\
& v_{0}=\frac{R_{0} R_{4}}{R_{1} R_{2}} v_{R} \frac{v_{X}}{v_{Z}}
\end{aligned}
$$

The reference input $V_{R}$ is generally fixed and the ratio of $R_{0} R_{4} / R_{1} R_{2}$ is usually chosen to make $V_{O}=10 \mathrm{~V}$ at the maximum value of $V_{X} / V_{Z}$. For example, if $V_{R}=6.2 \mathrm{~V}$ and $V_{X} / V_{Z}$ maximum is one, then choose $R_{0} R_{4} / R_{1} R_{2}$ of $10 / 6.2$ which is 1.613 . The output would then be:

$$
v_{0}=10 \frac{v_{X}}{v_{Z}}, \text { where } \frac{v_{X}}{v_{Z}} \leqslant 1
$$

As with the four-quadrant multiplier circuit, op amp offsets cross-multiply with the inputs. These offsets should be nulled to obtain best accuracy. The output voltage with offsets considered, but neglecting $\vee_{O S}{ }^{2}$ terms, is given by:


Because the offsets and signals are interactive, the recommended procedure for adjustment is the following:

1. Monitor the offsets at pins (8) and (1) directly and adjust VOS1, VOS2 to null them. This removes the VOS1 and VOS2 error terms.
2. Make $V_{X}=V_{Z}$ and sweep over their full dynamic range. The output should be constant; vary the VOS4 ADJ pot for a constant output of $R_{4} R_{0} V_{R} / R_{1} R_{2}$ plus $V_{O S 3}$.
3. Apply the minimum value of $V_{X} / V_{Z}$ and adjust $V_{O S 3}$ to obtain the proper $\mathrm{V}_{\mathrm{O}}$.
4. Apply the maximum value of $V_{X} / V_{Z}$ and adjust $R_{0}$ for proper $\mathrm{V}_{\mathrm{O}}$.

The accuracy will be limited only by the nonlinearity, which for the RC4200 is very small.

## SQUARE-ROOTING

The circuit for implementing the square-rooting function is shown in Figure 5. An input voltage $V_{X}$ multiplied by a reference voltage $V_{R}$ is made equal to the square of the output voltage. The relationship $I_{1} I_{2}=I_{3} I_{4}$ becomes:

$$
\frac{v_{X} V_{R}}{R_{1} R_{2}}=\frac{v_{0}^{2}}{R_{0} R_{4}}
$$

The input voltage must be positive. Scaling is determined by the external resistor network and reference voltage $\mathrm{V}_{\mathrm{R}}$. The output voltage is given by:

$$
v_{0}=\sqrt{\frac{R_{0} R_{4}}{R_{1} R_{2}} V_{R} V_{X}}
$$



Figure 4. One-Quadrant Divider

In most applications, the resistors should be comparable in value and $V_{R}$ should be in the range of 5 V to 15 V . A scale factor of 10 is very convenient and provides an output range of 0.3 V to 10 V for an input range of 10 mV to 10 V . In equation form:

$$
v_{0}=\sqrt{10 v_{X}}, 10 m V<v_{X}<10 V
$$

The offsets can be externally trimmed as needed. The nonlinear nature of the square-rooting function makes the error due to offsets very small for large inputs and very large at low input levels. With offsets included, the output voltage is:
$v_{0}=\left[\frac{R_{0} R_{4}}{R_{1} R_{2}} v_{R}\left(1-\frac{v_{O S 2}}{v_{R}}\right) v_{X}-\frac{R_{0} R_{4}}{R_{1} R_{2}} v_{R} v_{O S 1}+v_{0}\left(v_{0 S 3}+v_{O S 4^{\prime}}\right]^{1 / 2}\right.$

The term $\mathrm{V}_{\mathrm{OS} 2} / \mathrm{V}_{\mathrm{R}}$ affects gain only and is constant, therefore varying $R_{0}$ can compensate for the $V_{O S 2}$ error term. The effect of VOS3 and VOS4 is additive and only one of these offsets need be adjusted. The VOS1 term should be trimmed to zero. The recommended trimming sequence is as follows:

1. Adjust $\mathrm{V}_{\mathrm{OS} 3}$ to zero directly by monitoring pin (4).
2. Apply minimum value of $V_{X}$ and adjust $V_{O S 1}$ for correct $\mathrm{V}_{\mathrm{O}}$.
3. Apply maximum value of $\mathrm{V}_{\mathrm{X}}$ and adjust $\mathrm{R}_{\mathrm{O}}$ for correct $\mathrm{V}_{\mathrm{O}}$.

The square-rooting circuit can easily be designed for overall accuracy of $\pm 0.2 \%$ when using the RC4200A IC multiplier.


Figure 5. Square-Rooting Circuit

## RMS-TO-DC CONVERTER

The root-mean-square value of a complex waveform can be computed directly by squaring, integrating, and then square rooting. The RC4200 is ideally suited to this computation and the entire RMS-to-DC conversion can be implemented with a single device.

A functional diagram is shown in Figure 6. An absolute-value circuit, or precision rectifier, first converts the $A C$ input into a rectified positive voltage. Input currents $I_{1}$ and $I_{2}$ are made equal and will be $\left|V_{I N}\right| / R_{1}$. The remaining input current, $l_{4}$, is made equal to $V_{O} / R_{0}$ plus a derivative term, $\mathrm{C}_{\mathrm{O}} \mathrm{dV}_{\mathrm{O}} / \mathrm{dt}$. Combining these relationships according to $I_{1} I_{2}=I_{3} I_{4}$,

$$
\frac{v_{1 N^{2}}}{R_{1}^{2}}=\frac{v_{0}}{R_{1}}+c_{1} \frac{d V_{0}}{d t} \frac{v_{0}}{R_{1}}
$$

This equation is equivalent to

$$
v_{0}^{2}+\frac{R_{0} C_{0}}{2} \frac{d}{d t}\left(v_{0}^{2}\right)=v_{I N}^{2}
$$

The output voltage squared is the exponentially-weighted average of the input-voltage squared. Square-rooting both sides of the equation, and considering the polarity constraints inherent in this implementation, gives the desired results:

$$
v_{0} \equiv \sqrt{\left[v_{I N}(t)\right]^{2}}
$$



Figure 6. RMS-to-DC Converter

This is the true RMS value of $V_{I N}$ within the frequency range where the averaging time constant $\dot{R}_{1} \mathrm{C}_{1} / 2$ is of sufficient magnitude for low-pass filtering. Capacitor $\mathrm{C}_{1}$ must be large enough in value to adequately average the signal at its minimum frequency.

Various practical considerations limit performance for very small input signals, so this circuit is usually designed for a specific input voltage range. As with the divide and squareroot modes of operation, the RC4200 may require a stabilizing RSCS at the input summing junctions (pins 8, 1, and 5).

The specific component values and external adjustments needed depends on the particular application.

## DESIGN CONSIDERATIONS

## FREQUENCY RESPONSE AND STABILITY

The op amps within the RC4200 multiplier are stabilized for optimum performance in the four-quadrant multiplier configuration. At extremes of input current, the stability becomes marginal and external phase compensation may be required. The possibility of undesired oscillations should be considered for input currents of less than $50 \mu \mathrm{~A}$ or greater than $500 \mu \mathrm{~A}$. Dividing and square-rooting operations often require a wide dynamic range on the input currents.

Two techniques are very helpful for assuring frequency stability and minimizing noise under a wide range of conditions:

1. Connect a series $R_{S} C_{S}$ from input summing junction to ground as shown in Figure 7. This network has the effect of attenuating the feedback at high frequencies and thereby stabilizing the op amp. Loop gain at high frequencies is sacrificed, but this is seldom of concern in dividing or square-rooting applications. Recommended values are $10 \mathrm{k} \Omega$ for $R_{S}$ and $0.005 \mu \mathrm{f}$ for $\mathrm{C}_{S}$.
2. The resistor on the noninverting input can be bypassed as shown in Figure 7. This helps to reduce noise.

The need for these frequency compensating techniques will depend on the application, particularly the input current range and input signal characteristics.

## GAIN STABILITY

This type of multiplier is very sensitive to temperature gradients across the transistor quad ( Q 1 to Q 4 and Q 2 to Q3). The ambient temperature tends to affect offsets, but temperature gradients will cause a gain error. Several steps can be taken to minimize this effect:

1. Keep the multiplier physically remote from power dissipating components.
2. When using printed-circuit boards, make pad sizes and layout pattern as symmetrical as possible.
3. Heat sinking or epoxy potting can be used if necessary. This will tend to prevent rapid changes in temperature gradient.

Power drain within the multiplier chip itself is relatively low, therefore the gain stability can be very good if the IC is not exposed to temperature gradients.

## OFFSET STABILITY

Input offset voltage of the op amps can be easily trimmed if desired. The effects of input bias current drift can be minimized by making the impedance approximately equal on the inverting and noninverting inputs. The equivalent input offset will then depend only on the difference in bias currents rather than the absolute values.


Figure 7. Optional Frequency Stability Components $R_{S}, C_{S}$, and $C_{B}$.


AVAILABLE TYPES

| Part Type | Package | Operating Temperature |
| :--- | :--- | :---: |
| RM4200DE | Ceramic | -55 to $+125^{\circ} \mathrm{C}$ |
| RV4200NB | Plastic | -40 to $+85^{\circ} \mathrm{C}$ |
| RV4200DE | Ceramic | -40 to $+85^{\circ} \mathrm{C}$ |
| RC4200DE | Ceramic | 0 to $+70^{\circ} \mathrm{C}$ |
| RC4200NB | Plastic | 0 to +70 C |
| RM4200ADE | Ceramic | -55 to $+125^{\circ} \mathrm{C}$ |
| RV4200ANB | Plastic | -40 to $+85^{\circ} \mathrm{C}$ |
| RV4200ADE | Ceramic | -40 to $+85^{\circ} \mathrm{C}$ |
| RC4200ADE | Ceramic | 0 to $+70^{\circ} \mathrm{C}$ |
| RC4200ANB | Plastic | 0 to $+70^{\circ} \mathrm{C}$ |

Figure 8. AC Feedthrough vs. Frequency

HIGH RELIABILITY OPTIONS

| Part Type | Added Screening | Order Part No. |
| :---: | :---: | :---: |
| RM4200DE RM4200ADE | With MIL-STD-883 Class B processing | RM4200DE3 RM4200ADE3 |
| RV4200DE RC4200DE RV4200ADE RC4200ADE | With $A+3$ processing* including burn-in and tightened AQL | RV4200DE3 <br> RC4200DE3 <br> RV4200ADE3 <br> RC4200ADE3 |
| RV420GNB RC4200NB RV4200ANB RC4200ANB | With $A+2$ processing* including "Hot Rail" testing, burn-in, temp cycle and tightened AQL | RV4200NB2 RC4200NB2 RV4200ANB2 RC4200ANB2 |
| RV4200NB RC4200NB RV4200ANB RC4200ANB | With $\mathrm{A}+1$ processing* including "Hot Rail" testing, temp cycle and tightened AQL | RV4200NB1 RC4200NB1 RV4200ANB1 RC4200ANB1 |

[^8]
## GENERAL DESCRIPTION

The RC4444 is a monolithic dielectrically isolated crosspoint array arranged into a $4 \times 4 \times 2$ matrix. The primary applications are for balanced switching of 600 ohm transmission lines. The ring and tip are selected by selective biasing of the $\mathrm{P}+$ and P - gate.
Designed to replace reed-relays in telephone switchboards, it does not require a constant gate drive to keep the SCR in the "on" condition. It is several orders faster, with no bouncing, and has a much longer operating life than its mechanical counterpart.
The 16 SCR pairs with the gating system are packaged in a 24 pin dual-in-line package.

The RC4444 is a monolithic pin-for-pin replacement for the MC3416 and MCBH7601.

## DESIGN FEATURES

- Low Bi-Directional $\mathrm{R}_{\text {on }}$
- High Roff
- Excellent Matching of Gates
- Low Capacitance
- High Rate Firing
- Predictable Holding Current


## SCHEMATIC DIAGRAM




## CONNECTION INFORMATION



## ABSOLUTE MAXIMUM RATINGS

| Operating Voltage (Note 1) | 25V | Storage Temperature Range . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| Internal Power Dissipation (Note 2) | 900 mW | Operating Temperautre Range . . . . . . $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Operating Current per Crosspoint (Note 2) | 100 mA | Lead Temperature (Soldering, 60s) . . . . . . . . $300^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS $10^{\circ} \mathrm{C} \leqslant T_{A} \leqslant 70^{\circ} \mathrm{C}$ unless otherwise noted)

| CHARACTERISTIC | SYMBOL | MIN | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
| Anode-Cathode Breakdown Voltage ( I AK $=25 \mu \mathrm{~A}$ ) | BVAK | 25 | - | Vdc |
| Cathode-Anode Breakdown Voltage (IKA $=25 \mu \mathrm{~A}$ ) | BVKA | 25 | - | Vdc |
| Base-Cathode Breakdown Voltage ( $\mathrm{IBK}_{\text {B }}=25 \mu \mathrm{~A}$ ) | $B V_{B K}$ | 25 | - | Vdc |
| Cathode-Base Breakdown Voltage ( $\mathrm{I}_{\mathrm{KB}}=25 \mu \mathrm{~A}$ ) | BVKB | 25 | - | Vdc |
| Base-Emitter Breakdown Voltage ( $\mathrm{I}_{\mathrm{BE}}=25 \mu \mathrm{~A}$ ) | $B V_{B E}$ | 25 | - | Vdc |
| Emitter-Cathode Breakdown Voltage ( $\mathrm{IEK}=25 \mu \mathrm{~A}$ ) | BVEK | 25 | - | Vdc |
| OFF State Resistance (VAK $=10 \mathrm{~V}$ ) | roff | 100 | - | $\mathrm{M} \Omega$ |
| Dynamic ON Resistance <br> (Center Current $=10 \mathrm{~mA}$ ) <br> (Center Current $=20 \mathrm{~mA}$ ) | ron | $\begin{aligned} & 4.0 \\ & 2.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 12 \\ & 10 \\ & \hline \end{aligned}$ | $\Omega$ |
| Holding Current (See Figure 10) | IH | 0.9 | 3.8 | mA |
| Enable Current ( $\mathrm{V}_{\mathrm{BE}}=1.5 \mathrm{~V}$ ) | IEn | 4.0 | - | mA |
| Anode-Cathode ON Voltage $\begin{aligned} & \left(I_{A K}=10 \mathrm{~mA}\right) \\ & \left(\mathrm{I}_{\mathrm{AK}}=20 \mathrm{~mA}\right) \end{aligned}$ | VAK | - | $\begin{aligned} & 1.0 \\ & 1.1 \\ & \hline \end{aligned}$ | V |
| Gate Sharing Current Ratio @ Cathodes (Under Select Conditions with Anodes Open) | $\mathrm{G}_{\text {Sh }}$ | 0.8 | 1.25 | $\mathrm{mA} / \mathrm{mA}$ |
| Inhibit Voltage ( $\mathrm{V}_{\mathrm{B}}=3.0 \mathrm{~V}$ ) | $V_{\text {inh }}$ | - | 0.3 | V |
| Inhibit Current ( $\mathrm{V}_{\mathrm{B}}=3.0 \mathrm{~V}$ ) | Iinh | - | 0.1 | mA |
| OFF State Capacitance (VAK $=0 \mathrm{~V}$ ) | Coff | - | 2.0 | pF |
| Turn-ON Time | $\mathrm{t}_{\text {on }}$ | - | 1.0 | $\mu \mathrm{s}$ |
| Minimum Voltage Ramp (Which Could Fire the SCR Under Transient Conditions) | $\mathrm{dv} / \mathrm{dt}$ | 800 | - | $\mathrm{V} / \mu \mathrm{s}$ |

## NOTES:

1. Maximum voltage from anode to cathode.
2. Package thermal resistance $\theta$ JA typically $.055^{\circ} \mathrm{C} / \mathrm{mW}$. Package power dissipation limited to 900 mW .

## TYPICAL APPLICATIONS



## TYPICAL APPLICATIONS

FEEDTHROUGH VERSUS SIGNAL FREQUENCY


CROSSTALK VERSUS SIGNAL FREQUENCY


TEST CIRCUIT FOR FEEDTHROUGH VERSUS FREQUENCY

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{i}}=12 \mathrm{dBm}$, Crosspoints Off Feedthrough $=20 \log 10\left(v_{0} / v_{i}\right)$



## SECTION 8

## Packaging Information and Beam Lead Products

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1. 24-pin package.
2. Large cavity.

| 3-LEAD TO-5 PACKAGE | 10-LEAD TO-66 PACKAGE |
| :---: | :---: |
|  | TK |
| 8-LEAD <br> TO-99 PACKAGE TE <br> between pt a And PT b LEAD DIA IS $\frac{.019}{.016}$ <br> BETWEEN B \& C $\frac{.021}{.016}$ |  |
| 2-LEAD <br> TO-46 PACKAGE <br> TR | 4-LEAD <br> TO-46 PACKAGE |

## Packaging Information




| 14-LEAD CERAMIC FLAT PACKAGE CJ | 16-LEAD CERAMIC FLAT PACKAGE CL |
| :---: | :---: |
| $\begin{array}{ll} .015 & .050 \\ \hline \text { TYP } .008 \\ & \text { MIN } \end{array}$ | .005 .050 <br> MIN  <br> TYP  |
|  |  |

## 10-LEAD CERAMIC <br> FLAT PACKAGE CQ




16-LEAD PLASTIC DIP BM/MB


14-PIN PLASTIC DIP DB/BD



Typical Beam Lead Cross Section with Interconnections


## Ordering Information






[^0]:    ***Plastic mini-dip

[^1]:    *Denotes commercial temperature range device
    *Applies over temperature
    t149/349 ( $\mathrm{A}_{\mathrm{v}_{\text {min }}}=5$ ) parameter
    $\ddagger$ Denotes industrial temperature range device
    ${ }^{(1)}$ Gain-bandwidth product ( $A_{v_{\min }}=5$ )

[^2]:    3. High Temperature Functional Test (Hot Rail)
    (epoxy packages only)
    $+100^{\circ} \mathrm{C}$. This screening serves to further prove bond integrity.
[^3]:    Notes: 1. Rating applies for case temperature of $+25^{\circ} \mathrm{C}$ maximum; derate linearity at $6.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for temperatures above $+25^{\circ} \mathrm{C}$.
    2. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.
    3. Short circuit to ground on one amplifier only.

[^4]:    (1) See note 1 of 4194 data sheet.

[^5]:    Notes on following page.

[^6]:    * Each decoder section.

[^7]:    ${ }^{(1)}$ Temperature coefficient of output current mirror (pin 1 output) exclusive of reference voltage drift.

[^8]:    *Full descriptions contained in the quality section of this catalog.

